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PLAN DE ELECTRIFICACION DE LA PROVINCIA DE LA RIOJA

ANTEPROYECTO DEFINITIVO LINEA DE ALTA TENSION 132 KV CHAMICAL - CHEPES - LUJAN

INFORME PARCIAL Nº 5 TOMO 1 FLUJO DE CARGAS

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ANTEPROYECTO DEFINITIVO
LINEA DE ALTA TENSION 132 KV
CHAMICAL - CHEPES - LUJAN
PROVINCIA DE LA RIOJA

- 1994 -

TOMO 1

FLUJO DE CARGAS

T O M O I

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LINEA DE 132 KV CHAMICAL-CHEPES-LUJAN

INFORME PARCIAL 5

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CONTENIDO

INTRODUCCION

El C.F.I. se ha encargado del estudio del Anteproyecto Definitivo de Ingeniería de la LAT 132 que une las localidades de Chamical, Chepes y Luján en San Luis y las estaciones transformadoras de Chamical y Chepes en 132/33/13,3 kV. En Luján (San Luis) se realizará una estación transformadora en 500/132 kV cuyo proyecto original realizó Agua y Energía Eléctrica y del cual se tomaron las referencias para la ubicación del poste terminal.

La alimentación se realiza desde la LAT 500 kV que viene de Rio Tercero, (E.T. Almafuerte) y va a Gran Mendoza. Donde esta línea cruza la ruta 6 que va de Luján (S.L.) a San Juan, se ubica la ET 500 kV y el poste terminal de la LAT 132 kV.

La traza de la línea se detalla en el plano LAR-P-1001 LAR-P-1002. En el plano LAR-P-ET-1015 se detalla la ubicación del poste terminal.

Está previsto que la Estación Transformadora de Luján alimente con dos líneas de 132 kV a la ciudad de San Luis y otra de la misma tensión a la zona de Dolores y traslasierra (Córdoba).

Los Anteproyectos de las Estaciones Transformadoras de Chamical y Chepes ya fueron terminados y entregados a la Provincia de La Rioja.

Se realizó un estudio de mercado para verificar la viabilidad del proyecto. Se analizaron alternativas y se determinó elegir la traza más económica.

Su análisis eléctrico se realizó con estudio de flujo de cargas.

Esta línea tiene dos ventajas fundamentales:

* Permite la conexión sur con la red de 500 kV. Actualmente la Provincia está conectada a ese sistema por una línea de doble terna en 132 kV por su parte norte. Esta línea está, por otro lado, al borde de su prestación y además significa un vínculo débil en cuanto a su confiabilidad.

* Alimenta una zona muy necesitada, la del sur provincial, no solo de energía sino de un aporte mayor a la confiabilidad del servicio. Actualmente la zona está alimentada por una línea de 33 kV que requiere mucho mantenimiento.

Entre las alternativas estudiadas para el aprovisionamiento de energía se contempló la posibilidad de una conexión en 500 kV. a

la población de Patquía directamente de la ET 500 kV Recreo, ya que Patquía es el baricentro eléctrico de la provincia.

El costo de una línea de 500 kV es comparativa y proporcionalmente más económico que una de 132 kV.

Otro estudio es la conexión en 132 kV entre La Rioja y Nonogasta. Esta línea pasa por el Cerro del Velazco que significa una cierta dificultad pero seguramente es una alternativa muy conveniente para el futuro. Otra posibilidad es una conexión con San Juan en 132 kV por el aprovechamiento hidroeléctrico de Los Caracoles cuyo licitación fué anunciada en marzo de 1994.

Cabe señalar que esta incorporación de energía se puede realizar por la línea de 132 kV entre Nonogasta y Villa Unión cuya construcción está en un grado de avance del 85 %

En este contexto no hay soluciones únicas sino complementarias y en función de los recursos disponibles se irán escalando las mismas. Cabe destacar que a lo largo de este estudio se han producido modificaciones en el ordenamiento del suministro de energía nacional en una forma profunda como nunca en la historia del país con privatizaciones de la generación, transporte y distribución.

Las tarifas han cambiado, y el concepto de costo por nodo eléctrico produce un ordenamiento del consumo según pautas distintas de las vigentes hacia atras.

Por otro parte el país se está alineando en su actividad económica como socio participante del mercado sur con normativas sobre aranceles concertadas por el Gatt, ronda Uruguay y con sus socios del mercosur que afectan a toda la población creando nichos de oportunidad de negocios para los cuales la provincia debe estar preparada para aprovechar.

Cada decisión debe analizarse cuidadosamente para elegir la mejor en cada caso.

Como particularidades del proyecto surge que seria mas conveniente una tensión mayor como por ejemplo 220 kV, debido a la distancia que debe cubrir para un mejor comportamiento eléctrico.

Por otro lado debe haber acuerdos provinciales con Córdoba y San Luis la construcción de la ET Luján.

Por último cabe destacar que la línea puede realizarse hasta la ET Chepes mientras se avanza con la ET Luján lo que tendría un costo casi mitad.

De esta forma se potencia la confiabilidad hacia el sur y se puede hacer una inversión pautada al avance del proyecto de la ET Luján.

Este estudio se realiza en forma completa pero con nivel de detalle en la ingeniería menor al ideal debido a razones presupuestarias. El alcance es Anteproyecto Definitivo apto para licitar con Proyecto a cargo del Contratista.

El contenido de esta parte del trabajo es el siguiente:

TOMO I Flujo de Cargas.

TOMO II Traza de la línea.

TOMO III Cálculos técnicos. Memorias de Cálculo

TOMO IV Documentación Licitatoria

FLUJO DE CARGAS

El Flujo de cargas es un capítulo del cálculo de las líneas de alta tensión que permite conocer el comportamiento de línea eléctrica para una configuración definida por la topología de la red, las características físicas de la línea, generación y consumos determinados en los puntos que denominamos nodos. Se plantea de esta forma un sistema de ecuaciones simultáneas, no lineales, que se resuelven por métodos iterativos.

Se cargan datos a los nodos según la información disponible. Uno de ellos se deja sin datos (llamado swing) y el juego de iteraciones le asigna los resultados que satisfacen las leyes de Kirchoff y Norton, equilibrando el sistema.

Propósito

Es verificar el comportamiento de la línea en los aspectos eléctricos: caídas de tensión, pérdidas de potencia, etc. durante su vida útil, insertada en la zona cuyo mercado de demanda eléctrica se conoce y permite verificar su diseño para atender esa demanda.

Mercado

Los consumos históricos, más una serie de hipótesis y planteos sobre el crecimiento, consultas sobre las políticas provinciales acerca del planeamiento futuro, políticas de inversión, conforman un capítulo que fija en alternativas los rangos de crecimiento del mismo. La situación actual del mercado en conformidad con las pautas de acuerdos internacionales con nuestros socios del Mercosur, definen un contexto en el que se elaboran alternativas de crecimiento para un período suficientemente válido para la vida útil de la línea.

Las conclusiones del mercado han sido oportunamente estudiadas, consultadas con las autoridades provinciales, publicadas y enviadas a la Provincia de La Rioja (Informe Parcial IV de este trabajo). De allí se toman los datos que interesan a la continuación de los estudios.

Programas utilizados

El estudio de flujo de cargas es en definitiva la resolución de una matriz de tantas filas y columnas como incógnitas deben resolverse.

Las incógnitas pueden ser determinadas en función de los datos que se incorporan. Por ejemplo si se introducen potencia activa, tensión en un extremo y consumos en distintos nodos surgen como resultados las corrientes, las caídas de tensión, ángulos de potencia, potencia reactiva en el resto de la red.

Hay distintos programas según la forma de resolución. Se utiliza un método iterativo que, saliendo de valores estimados asignados

a las variables que va corrigiendo en función de que los resultados converjan a valores coincidentes.

Se utilizaron los siguientes programas: EMTF(ATP), FLUPROG (Fludern, desacople rápido).

Ambos programas tienen un comportamiento distinto: El EMTF (Electromagnetic Transient Program) es un programa muy grande para estudios eléctricos y una de sus aplicaciones se destina al flujo de cargas.

La carga de datos no siempre converge a una solución, si ello ocurre después de un número determinado de iteraciones envía una solución con los parámetros tal como quedaron en la última iteración, con las advertencias del caso.

El FLUPROG tiene un método más expeditivo por desacople rápido y siempre presenta su solución. Este programa fué gentilmente cedido por la Universidad de La Plata con autorización para su uso.

El flujo de cargas es una herramienta necesaria para tomar decisiones en cuanto a priorizar inversiones para llegar a optimizar satisfacciones del mercado con cuotas crecientes de inversión. Así por ejemplo no hay, a la fecha, confirmación sobre la construcción de la Estación Transformadora Luján, y necesita el acuerdo y aporte proporcional de los tres estados provinciales afectados.

Está más avanzado a la fecha el Proyecto de la Central Hidráulica de Los Caracoles en San Juan. Siendo probable una alimentación alternativa por esa Provincia a traves de Villa Unión. Por lo tanto es probable que la línea objeto de este estudio se justifique hacerla en dos etapas: Una hasta Chepes o Ulapes y la otra hasta Luján. Esto queda facultativo para las autoridades provinciales para administrar los préstamos que mayor tasa de retorno signifique priorizando la inversión.

ESTUDIO DE LOS CASOS

La denominación de los casos es puramente arbitraria, la asignación válida es la que figura no como título de cada caso sino la asignada en caracteres manuscritos, esto se debe a la conveniencia de relacionar los casos que en el estudio resulten interesantes. Muchos de los casos con numeración correlativa ha tenido que descartarse porque se han tomado como escalones para detectar tendencias, porque no son significativos, por divergencia o porque no aportan novedades.

Se incluyen corridas de elaboración, resolución, y transformación de los datos eléctricos. Los datos que alimentan cada programa tienen que tener un formato especial.

También se incluyen algunos de los cálculos de las bases de fundación de hormigón de los soportes, por método de Sulzberger.

Caso 100

Encabeza un gráfico 100 que es una representación topológica de la red; en ese gráfico, entre corchetes se vuelca el valor de

consumo en MW para cada nodo. Se adjunta la corrida en EMTP. Para este primer caso, se hará una descripción más detallada para conocer su mecánica, e interpretar sus resultados.

En la hoja 1 se ingresan los datos: RECRE, LARIO, 0.11, 0.22 son respectivamente nodo origen (Recreo), nodo destino (La Rioja) impedancia resistiva e inductiva. Así el resto.

En pag. 2 se vuelcan los nodos que generan tensión Luján y Recreo con valor de tensión en valores por unidad. Los valores de consumo en escala 100 MW = 1, y consumo reactivo de la misma forma, la tensión mínima, la máxima (.65 y 1.25). Para los nodos generadores el ángulo eléctrico THMIN Y THMAX.

Se inicia la iteración y se realizan 1048. Los primeros resultados arrojan el número del nodo, la magnitud de la tensión, la potencia real y reactiva.

Después se vuelcan los valores por cada rama progresiva multiplicados por un factor 1.41 que los transforma en valores pico, en coordenadas rectangulares, polares. Del mismo modo la corriente, la potencia activa y reactiva y las pérdidas.

Como último punto se vuelcan los valores eléctricos de los nodos con tensión conocida y aquí, igual que antes, los valores de tensión pico, rectangular, polar; corriente rectangular y polar y valores de potencia activa, reactiva, aparente y factor de potencia.

Se advierte por ejemplo la caída importante de la tensión en los nodos Nonogasta y Chilecito $1.06 \cdot 1 / 1.41 = 0.75$ que es inaceptable. Esto significa que deben corregirse valores de potencia activa y reactiva, compensando adecuadamente para evitar caídas tan importantes. Otros recurso son: cambiar la topología de la red, aumentar secciones, compensaciones capacitivas etc.

CASO 110

En este caso se supone una desconexión entre Patquía y Nonogasta y se admite una conexión entre La Rioja y Nonogasta.

Este resulta ser un caso interesante de estudio ya que evidencia la gran ventaja de la conexión "transVelazco".

Obsérvese que para VU.(Villa Unión) en el caso 100, con la conexión actual, la tensión es de $1.04 / 1.41 = 0.73$. En el caso de estar conectados por la "transVelazco", la tensión es $1.16 / 1.41 = 0.82$.

Este caso es de laboratorio, no tiene implementadas correcciones de ningún tipo pero sirve de evidencia como justificante de construcción futura de la línea de interconexión.

El terreno es dificultoso pero tiene un antecedente de una línea telegráfica tendida por ese camino que actuó durante mucho tiempo (30 a 40 años).

CASO 130 y 200

Ilustra la preparación de datos para incluirlos en el programa de EMTP como datos elaborados según los requisitos de aceptación, en forma y sintaxis.

Son los que surgen de las configuración física y geográfica de la línea más los requisitos de energía y potencia de la zona que abastece. Es resultado del uso de una planilla electrónica u hoja de cálculo.

CASO 160

Se estudia en este caso mediante el uso del programa FLUPROG. Es una hipótesis de funcionamiento de alimentación de la línea sólo para las poblaciones del sur, centro y oeste.

CASO 250

Ilustra otro caso en EMTP de alimentación simplificada para verificar el funcionamiento del programa y asegurar convergencia, estudiar el juego de compensaciones. Que pueden ser correcciones de coseno ϕ mediante capacitores, o regulación de los pasos del transformador.

CASO 260

Esta es otra forma más completa, ilustra además un caso de rechazo de datos preliminares y advertencia de error, del que despues se recupera.

CASO 270

Este caso sirve para controlar la diferencia en caídas de tensión con el caso 260 porque es la línea con conexión actual y con cargas similares al anterior. Resultando una tensión 0.71 contra 0.82 la caída de tensión para V.Unión en valores en tanto por unidad. Con este caso se verifica la ventaja de funcionamiento de la conexión La Rioja- Nonogasta. Ver también caso 110.

CASO 300

Este caso ilustra una configuración en la que se supone generación en V.Unión y en Luján. Esta es una posibilidad que se da en la alternativa de alimentación de energía de la Central de Los Caracoles en San Juan.

CASO 310

Se vuelca aquí la salida de un programa que da los datos del cuadripolo Π , las constantes A,B,C,D. El estudio es para líneas con parámetros distribuidos, o sea los valores reales de líneas de gran longitud. Se analiza el caso particular de la línea con sección 240 AlAc mm² que fué la primer alternativa analizada.

CASO 320

Lo mismo que el caso anterior pero la sección AlAc en este caso de 150 mm².

CASO 325

Lo mismo que el caso anterior pero con otras condiciones de transporte de energía.

CASO 330

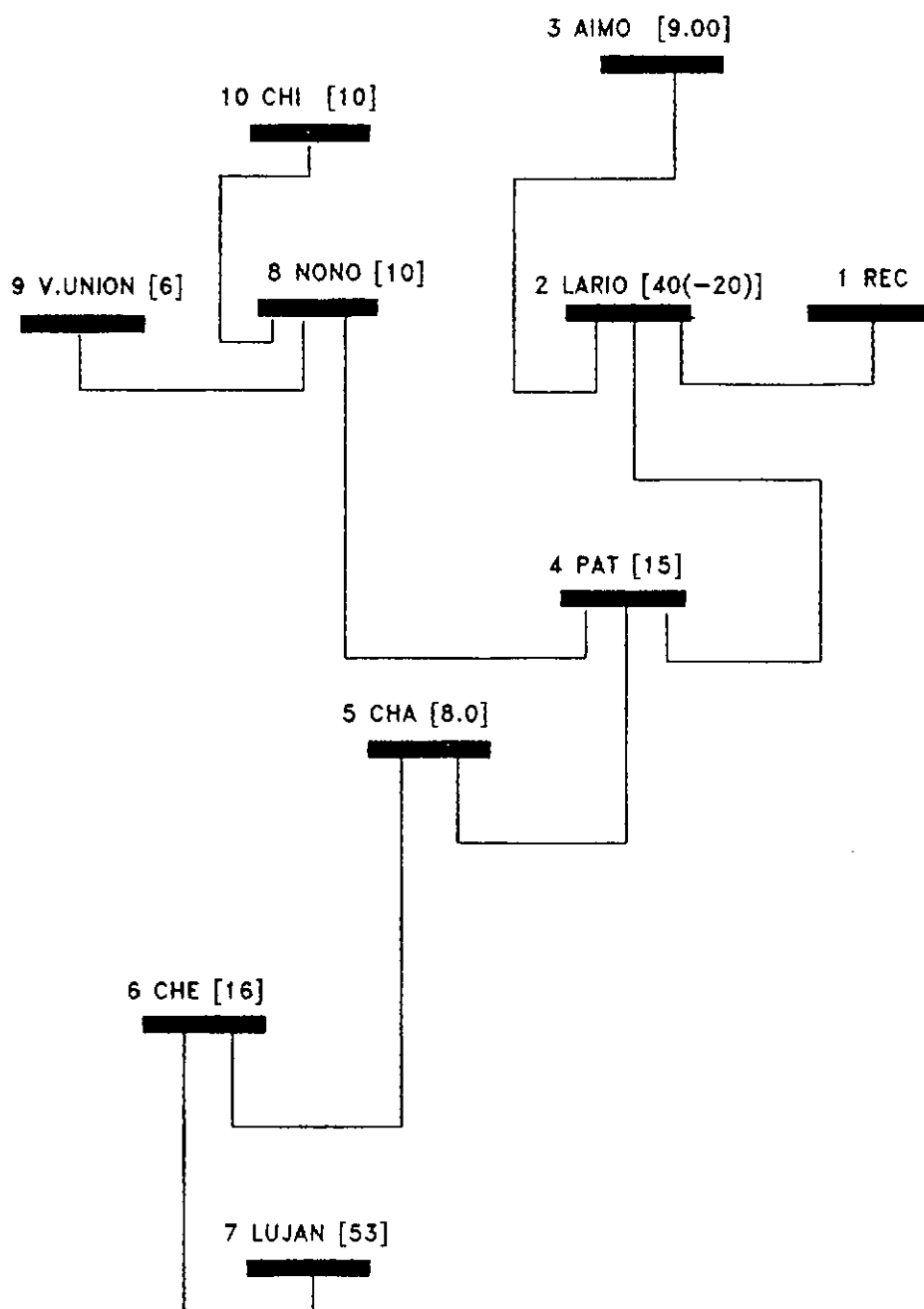
Esta es la salida de una corrida EMTP con línea de AlAc 150 mm² con alimentación por Luján y Recreo.

CASO 340

Esta es la salida de una corrida EMTP con línea de AlAc 150 mm² con alimentación por Luján, Recreo y por V.Unión. Esta es una alternativa viable para el futuro por lo tanto se incorpora para conocer su comportamiento.

Estos no son, como se dijo arriba, todos los casos estudiados. Esto haría muy voluminoso el estudio sin agregar más elementos de juicio.

CIRCUITO PARA FLUJO
DE CARGAS 132 kV – LA RIOJA
CASO 100
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
 Date (dd-mth-yy) and time of day (hh.mm.ss) = 05-Apr-94 15.12.49 Name of disk plot file, if any, is C:\44051512.pl4
 For information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
 Total length of "LABCOM" tables = 444863 INTEGER words. "VARDIM" List Sizes follow: 752 900 1500 150 7500
 120 2100 5250 225 480 150 15000 60 64800 120 12 15 4800 1780 300 450 12000 9 1200 252 4

Descriptive interpretation of input data cards.

Input data card images are shown below, all 80 columns, character by character
 0 1 2 3 4 5 6 7 8
 01234567890123456789012345678901234567890123456789012345678901234567890

Blank card. KOMPAT = 1. :C DATA:C:\RIV\EMIN\PROBE2.DAT
 Blank card. KOMPAT = 1. :C DATA:C:\RIV\EMIN\PROBE2.DAT{-05-04-94 15:55:REIDNO Y AGREGO DATOS DE ARCH
 Blank card. KOMPAT = 1. :C RED 132 KV LA RIOJA; DATOS DE RED FLUJ32E.WG1 12-12-97}
 Blank card. KOMPAT = 1. :C (SE AGREGAN LOS DATOS DE RESTRICCIONES Y RAMAS COMPLETAS *XC)
 Blank card. KOMPAT = 1. :ERASE
 Blank card. KOMPAT = 1. :BEGIN NEW DATA CASE
 Blank card. KOMPAT = 1. :PRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
 Blank card. KOMPAT = 1. :FIX SOURCE (An EMTP load flow will satisfy requested phasor power injections.
 Blank card. KOMPAT = 1. :POWER FREQUENCY, 50.0,
 Blank card. KOMPAT = 1. :C MISCELANEA CARD SIGUE II B-1, II B-2
 Blank card. KOMPAT = 1. :C 34567890123456789012345678901234567890123456789012345678901234567890
 Blank card. KOMPAT = 1. :C DELTAT TMAX XOPT COPT EPSILN TOLMAT
 Blank card. KOMPAT = 1. :C 1.000200 .000 50.50.(T-max = 0 means that no transient solution follows
 Blank card. KOMPAT = 1. :C IOUT IFLUT IDOUEL KSSOUT MAXOUT IFUN MEMSAV ICAT MERERS IPRSUP
 Blank card. KOMPAT = 1. :C 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
 Blank card. KOMPAT = 1. :C 1 1 0 1 0 1 0 0 0 0 :C 1 1 1 0 1
 Blank card. KOMPAT = 1. :C
 Blank card. KOMPAT = 1. :C CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.
 Blank card. KOMPAT = 1. :C BASE 100 MVA =1; UB=132 KV
 Blank card. KOMPAT = 1. :C SIGUE FORMATO RULE BOOK 4A-2
 Blank card. KOMPAT = 1. :C 34567890123456789012345678901234567890123456789012345678901234567890
 Blank card. KOMPAT = 1. :C BUS1 BUS2 BUS3 BUS4 RES13 XL XC OUTPUT OPTION
 Blank card. KOMPAT = 1. :C A6 A6 A6 A6 E6.2 E6.2 E6.2 11
 Blank card. KOMPAT = 1. :C 3-8 9-14 15-20 21-26 27-32 33-38 39-44 50
 Blank card. KOMPAT = 1. :C LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUAL11)
 Blank card. KOMPAT = 1. :C EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;3=I y V DE RAMA; 4=CONSUMO POT Y ENEAS
 Blank card. KOMPAT = 1. :C RECRE LARIO 0.11 0.22
 Blank card. KOMPAT = 1. :C LARIO AINGOS .16 .30
 Blank card. KOMPAT = 1. :C LARIO PATQU .08 .16
 Blank card. KOMPAT = 1. :C PATQU CHAMI .08 .16
 Blank card. KOMPAT = 1. :C PATQU NONDS .14 .26
 Blank card. KOMPAT = 1. :C CHAMI CHEPE .09 .28
 Blank card. KOMPAT = 1. :C CHEPE LUJAN .09 .27
 Blank card. KOMPAT = 1. :C NONDS VUNIO .11 .21
 Blank card. KOMPAT = 1. :C NONDS CHILE .01 .02
 Blank card. KOMPAT = 1. :C LARIO NONDS .08 .16
 Blank card. KOMPAT = 1. :C
 Blank card. KOMPAT = 1. :C
 Blank card ending branches. IBR, NTOT = 9 11 :BLANK card ending branch cards.
 Blank card ending switches. KSWTCH = 0. :BLANK card ending switch cards.
 Blank card. KOMPAT = 1. :C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
 Blank card. KOMPAT = 1. :C 34567890123456789012345678901234567890123456789012345678901234567890

```

ment card.  KOMPAT = 1.      IC NAME IV AMPLITUDE FREQUENCY PHASE  A1  TIME-1  TSTART  TSTOP
ment card.  KOMPAT = 1.      IC 12 A6 12  E10.6  E10.6  E10.6  E10.6  E10.6  E10.6
ment card.  KOMPAT = 1.      IC 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
ment card.  KOMPAT = 1.      IC
source. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114LUJAN 1.10 50. 15.0 -1.
source. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114RECRE 1.10 50. 15.0 -1.
ment card.  KOMPAT = 1.      IC
ment card.  KOMPAT = 1.      IC
Blank card ends electric network sources.  BLANK card terminating all EMTP source cards.
ment card.  KOMPAT = 1.      IC Next come power constraints of the load flow. There will be one
ment card.  KOMPAT = 1.      IC for each non-slack generator. So, 3 of them will apply to nodes
ment card.  KOMPAT = 1.      IC that have no Type-14 source as required by the algorithm. The
ment card.  KOMPAT = 1.      IC program will define these internally. Yet, this is only possible
ment card.  KOMPAT = 1.      IC for TMAX non-positive (no transient continuation). If data is
ment card.  KOMPAT = 1.      IC modified to make TMAX > 0, a KILL = 40 error termination will
ment card.  KOMPAT = 1.      IC will result. Yet, the transient simulation is possible as a
ment card.  KOMPAT = 1.      IC 2nd simulation that replaces the power constraints at load nodes
ment card.  KOMPAT = 1.      IC by constant-impedance loads. Branch cards for these will be
ment card.  KOMPAT = 1.      IC punched by the present subcase, and the transient continuation
ment card.  KOMPAT = 1.      IC will be illustrated by the following (4th of 4) subcase.
ment card.  KOMPAT = 1.      IC The following 4 cards would be used if peak rather than RMS input data.
ment card.  KOMPAT = 1.      IC Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.828428 ) = 1.414212
ment card.  KOMPAT = 1.      IC (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 + 1.02
ment card.  KOMPAT = 1.      IC
ment card.  KOMPAT = 1.      IC VALORES DE POTENCIA EN PU 1=100 MVA
ment card.  KOMPAT = 1.      IC PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4:10-6
ment card.  KOMPAT = 1.      IC 34567890123456789012345678901234567890123456789012345678901234567890
ment card.  KOMPAT = 1.      IC NKBUS1 BUS2 BUS3 PK or GK GK or VK VMIN VMAX TMIN TMAX
ment card.  KOMPAT = 1.      IC 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-69 69-74 75-80
X. -4.000E-01 -2.000E-01 6.500E-01 1.250E+00 LARIO -0.4000 -0.200 .65 1.25
X. -8.000E-02 -3.400E-02 6.500E-01 1.250E+00 CHAMI -0.080 -0.034 .65 1.25
X. -1.500E-01 -8.000E-02 6.500E-01 1.250E+00 PATOU -0.150 -0.080 .65 1.25
X. -1.000E-01 -6.100E-02 6.500E-01 1.250E+00 NONOS -0.10 -0.061 .65 1.25
X. -6.000E-02 -2.000E-02 6.500E-01 1.250E+00 VUNIO -0.0600 -0.02 .65 1.25
ment card.  KOMPAT = 1.      IC LUJAN 1.0 1.20 -20. 40.
X. 8.000E-01 1.100E+00 0.000E+00 1.000E+19 IRECRE 0.8 1.10 -20. 15.
X. -1.600E-01 -9.000E-02 0.000E+00 1.500E+00 CHEPE -.16 -.09 1.5
X. -9.000E-02 -4.000E-02 6.500E-01 1.150E+00 AINOS -0.090 -0.04 .65 1.15
X. -1.000E-01 -4.000E-02 0.000E+00 1.150E+00 CHILE -.1000 -.04 1.15
ment card.  KOMPAT = 1.      IC The following load-flow miscellaneous data card has two peculiarities. The
ment card.  KOMPAT = 1.      IC use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
ment card.  KOMPAT = 1.      IC voltages. The use of KTAPEK = 0 ensures constant acceleration factors
ment card.  KOMPAT = 1.      IC (this works well for this problem whether RMS or peak values are used).
ment card.  KOMPAT = 1.      IC NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITER VSCALE KTAPEK
ment card.  KOMPAT = 1.      IC 10-16 17-24 25-32 33-40 41-48 50-56 57-64
= LASTOV, NTOT, NEXT, IOFKOL, IOFKOR, NCURR = 9 11 19 0 0 0
Load flow iter. 1 2500 20 1 1.00E-02 1 2500 20 1 .01 0.2 2.5 1.414 2
ax del-V: .0232 .0227 .0223 .0218 .0213 .0209 .0204 .0187 .0152 .0155 .0158 .0149 .0136 .0135 .0133 .0131 .0129 .0127 .0125
ource No. 1 -4 -4 -4 -4 -4 -4 -4 -4 -9 -9 -9 -9 -5 -5 -5 -5 -5 -5
ax del-V: .0122 .013 .0132 .0133 .0112 .0111 .0109 .0106 .0113 .0094 .0103 .0113 .0103 .0114 .0117 .0102 .0115 .0115 .0114
ource No. 7 7 7 7 -5 4 -5 -5 -9 -4 -4 -4 -4 -4 -4 -4 -4 -4 -4
ax del-V: .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0115 .0116 .0115 .0115 .0115 .0115 .0115 .0115 .0115 .0115 .0115 .0115

```

[illegible]

Source No.	-4	-7	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0104	.0105	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0105	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0102	.0103	.0102
Source No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9
Max del-V:	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102
Source No.	-4	4	-4	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0103	.0102	.0103	.0103
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103	.0102	.0103
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0102	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0101	.0104	.0101	.0104	.0101	.0104	.0101	.0104	.01	.0105	.01	.0105	.01	.0105	.01	.0105	.0077	.0105	.0077	.0105
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0077	.0105	.0077	.0105	.0077	.0105	.0077	.0105	.0077	.0105	.0077	.0105	.0077	.0105	.0077	.0105	.01	.0105	.01	.0105
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4
Max del-V:	.01	.0105	.01	.0105	.01	.0105	.01	.0105	.01	.0106	.01	.0105	.0077	.0104	.0078	.0103	.0078	.0101	.0074	.0078
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4
Max del-V:	.0091	.0074	.0088	.0091	.0084	.0086	.0079	.0082	.0075	.0077	.007	.0072	.0065	.0067	.0059	.0062	.0054	.0056	.0049	.0051
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4
Max del-V:	.0045	.0046	.004	.0042	.0036	.0037	.0032	.0033	.0028	.0029	.0025	.0025	.0022	.0022	.0019	.0019	.0016	.0016	.0014	.0014
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
Max del-V:	.0012	.0012	.001	1.E-3	.9E-3	.8E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3	.7E-3
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4

Exit the load flow iteration loop with counter NEKITE = 1048. If no warning on the preceding line, convergence was attained.

Row	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	3	LARIO	9.03095820E-01	2.81941	-4.03220938E-01	-2.01118971E-01

4	6	CHAM1	8.92146054E-01	3.81992	-8.11722435E-02	-3.54636234E-02
5	5	PATQU	8.52596333E-01	1.47386	-1.51310701E-01	-8.11924027E-02
6	7	NONOG	7.55086210E-01	-2.92695	-1.08753601E-01	-7.63559025E-02
7	10	VUNIO	7.38849166E-01	-3.96111	-6.40176872E-02	-2.38321913E-02
2	2	RECRE	1.10000000E+00	9.02719	7.95027448E-01	6.13694372E-01
8	8	CHEPE	9.72179851E-01	9.05299	-1.60217557E-01	-9.06666367E-02
9	4	AIMOG	8.71505735E-01	1.26612	-9.30610913E-02	-4.11698788E-02
10	11	CHILE	7.52241020E-01	-3.08951	-9.30108620E-02	-3.32825663E-02

Buscoidal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage		Phasor branch current		Power flow	Power loss
		Rectangular	Polar	Rectangular	Polar	P and Q	F and Q
RECRE		1.5363782760361	1.5556349186104	1.1332327372933	1.2912223859794	.79502744830178	.09167903875299
		.244011870458	9.0244988	-.6189012951844	-28.6406245	.61369437241158	0.1833981
LARIO		1.2755643899932	1.2771083813261	-1.1332327372933	1.2912223859794	-.7033284095488	
		.06277981072376	2.8176688	.6189012951844	151.3593755	-.4302962949056	
ARIO		1.2755643899932	1.2771083813261	.15245771331815	.16513862425238	.09524275247453	.0021816512176
		.06277981072376	2.8176688	-.0634618851735	-22.5999565	.0452604936173	0.0040706
AIMOG		1.2321325903103	1.2324327016873	-.1524577133181	.16513862425238	-.0930610912569	
		.02719639835607	1.2644628	.06346188517347	157.4000435	-.0411698788343	
ARIO		1.2755643899932	1.2771083813261	.33459648140368	.43114403872619	.20486471882004	.00743540728517
		.06277981072376	2.8176688	-.2719014100026	-39.0781669	.18391682997982	0.0142708
PATQU		1.2052924458805	1.2056909480758	-.3345964814037	.43114403872619	-.1974293115349	
		.03099648649938	1.4731499	.27190141000261	140.9018331	-.1690460154095	
ATQU		1.2052924458805	1.2056909480758	-.3989777803711	.4211890624396	-.2383506512603	.00705500905275
		.03099648649938	1.4731499	.15457020615318	161.3098340	-.0875227400444	0.0141920
CHAM1		1.2589059016147	1.2616077964478	.39897778037108	.4211890624396	.24544665031205	
		.0840353147065	3.8192824	-.1349702081532	-18.6901660	.10171475894988	
ATQU		1.2052924458805	1.2056909480758	.47920024641766	.55434578515984	.28446906158253	.02151094746671
		.03099648649938	1.4731499	-.2786868733144	-30.1808340	.17537633557022	0.0397487
NONOG		1.0657458243203	1.0671424909421	-.4792002464177	.55434578515984	-.2627581141158	
		-.0545794153052	-2.9316939	.27868687331435	149.8191460	-.135427451132	
CHAM1		1.2589059016147	1.2616077964478	-.5311174043656	.56159562650557	-.3266189037828	.01419253414696
		.0840353147065	3.8192824	.18245369986434	161.0371089	-.1071783823093	0.0441546
CHEPE		1.3577047039696	1.3748301822891	.53111740436556	.56159562650557	.34081143792976	
		.21632375494106	9.0528704	-.1824536998643	-18.9628711	.18133293298877	
CHEPE		1.3577047039696	1.3748301822891	-.7820397865097	.82937854700719	-.5010289746863	.03095110914984
		.21632375494106	9.0528704	.27607281261993	160.3561364	-.2719956977316	0.0928533

LUJAN	1.5026277441629	1.5556349186104	.78203978650968	.82933854700719	.5319801038361	
	.40262774416288	15.0000000	-.2760728126199	-19.4438636	.36495289718116	
WONOG	1.0657458243203	1.0671424809421	.11177527823698	.12390774389819	.06102129445152	.84442209489E-3
	-.0545794153052	-2.9316939	-.0534735090768	-25.5665426	.02544426983929	0.0016121
VUNIO	1.0422211068081	1.0447168823453	-.111775278237	.12390774389819	-.0601768727566	
	-.0721701377365	-3.9612074	.05347350907678	154.4334574	-.0238321912945	
WONOG	1.0657458243203	1.0671424809421	.17118872721111	.18566435569345	.07318321822373	.17235626488E-3
	-.0545794153052	-2.9316939	-.0718726140536	-22.7748228	.03362727882632	0.0003447
CHILE	1.0625964847671	1.0641394641784	-.1711887272111	.18566435569345	-.0730108619589	
	-.0572844637089	-3.9853223	.07187261405365	157.2251772	-.0732825663066	
Total network loss P-loss by summing injections =			1.760834854316E-01			

Injection at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed result applying to the composite group. The entry "MVA" is $\text{SQRT}(P^2 + Q^2)$ in units of power, while "P.F." is the associated power factor.

Node name	Source node voltage		Injected source current		Injected source power	
	Rectangular	Polar	Rectangular	Polar	P and Q	MVA and P.F.
RECRE	1.5363782760361	1.5556349186104	1.1332327372933	1.2912223859794	.79502744830178	1.0043333156605
	.244011870458	9.0244988	-.6189012951844	-28.6406245	.61369437241158	0.7915956
LARIO	1.2755643899932	1.2771083813261	-.8461785425715	.70564899654756	-.4032209382542	.45039512388262
	.06277981072376	2.8176688	.28353800000835	156.3085165	-.2011189713085	-0.8948631
AIMOG	1.2321325903103	1.2324327016873	-.1524577133181	.16513862425278	-.0730610912569	.10176112042014
	.02719639835607	1.2644628	.06346198517347	157.4000435	-.041169788343	-0.7145054
PATOU	1.2052924458805	1.2056909480758	-.2543740133571	.284846394569	-.1513109012127	.17171835976194
	.03099648649938	1.4731499	.12818474484143	153.2554450	-.0811924026837	-0.8811574
CHAMI	1.2588059016147	1.2616077964478	-.1321396239945	.14042564756419	-.0311722434697	.02855104589411
	.0840353147065	3.8192824	.04752349171116	160.2190796	-.0354636233595	-0.9163613
WONOG	1.0657458243203	1.0671424809421	-.1962362409496	.24904226134701	-.1087536014406	.13288178831664
	-.0545794153052	-2.9316939	.15334075018392	141.9756135	-.0763559024564	-0.5184237
CHEPE	1.3577047037696	1.3748301822851	-.2509223821441	.26780420498007	-.1602175567565	.18409265197527
	.21632375494106	9.0528704	.09357911275559	159.5474766	-.0706666367429	-0.8703094
LUJAN	1.5026277441629	1.5556349186104	.78203978650968	.82933854700719	.5319801038361	.645074001537
	.40262774416288	15.0000000	-.2760728126199	-19.4438636	.36485289718116	0.6246897
VUNIO	1.0422211068081	1.0447168823453	-.111775278237	.12390774389819	-.0601768727566	.06472425595188
	-.0721701377365	-3.9612074	.05347350907678	154.4334574	-.0238321912945	-0.6237422
CHILE	1.0625964847671	1.0641394641784	-.1711887272111	.18566435569345	-.0730108619589	.07879678359233
	-.0572844637089	-3.9853223	.07187261405365	157.2251772	-.0732825663066	-0.9415352

ment card. KOMPAT = 1. IC
ment card. KOMPAT = 1. IC
ment card. KOMPAT = 1. IC
uest for flushing of punch buffer. \$PUNCH { Flush punched cards: R-L branches for equivalent impedance loads

isting of 80-column card images now being flushed from punch buffer follows.

=====

456789012345678901234567890123456789012345678901234567890123456789

=====< End of LUNIT7 punched cards as flushed by \$PUNCH request >=====

nk card ending node names for voltage output. {BLANK card ending requests for output variables

ective branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be
mented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

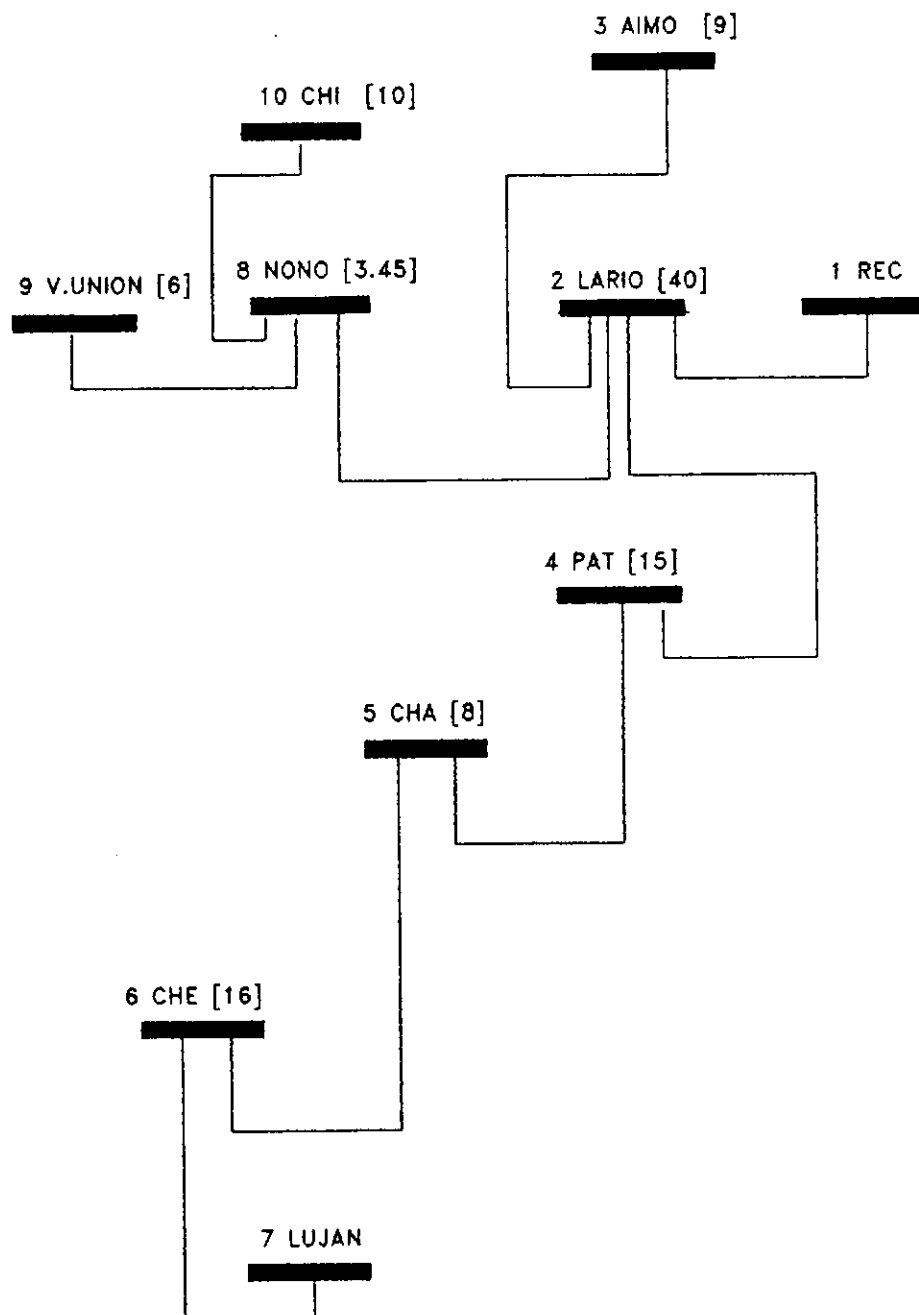
From	To	Branch voltage Vkm = V _k - V _m				Branch current Ikm from K to M			
From K	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
CRE	LARIQ	3.1759871E-01	34.794324	2.6081387E-01	1.8123206E-01	1.2912224E+00	-28.640624	1.1332327E+00	-6.1890130E-01
RIO	AIMOG	5.6147132E-02	39.327557	4.3431800E-02	3.5583412E-02	1.6513863E-01	-22.599957	1.5245771E-01	-6.3461885E-02
RIO	PATQU	7.7125390E-02	24.336782	7.0271944E-02	3.1783324E-02	4.3114404E-01	-39.098167	3.3459648E-01	-2.7190141E-01
QU	CHANI	7.5344590E-02	-135.255217	-5.3513456E-02	-5.3038828E-02	4.2118906E-01	161.309834	-3.7897778E-01	1.3497021E-01
QU	NONGG	1.6369635E-01	31.518390	1.3954662E-01	8.5575902E-02	5.5434572E-01	-30.180354	4.7920025E-01	-2.7868667E-01
ANI	CHEPE	1.6517023E-01	-126.781780	-9.8898802E-02	-1.3228844E-01	5.6159563E-01	161.037109	-5.3111740E-01	1.8249370E-01
PE	LUJAN	2.3603389E-01	-127.878812	-1.4492324E-01	-1.8630419E-01	6.2933855E-01	160.556136	-7.8203979E-01	2.7607231E-01
NGG	VUNIO	2.9374238E-02	36.787482	2.3524718E-02	1.7590722E-02	1.2390774E-01	-25.566543	1.1177528E-01	-5.3477509E-02
NGG	CHILE	4.1515812E-03	40.660126	3.1493396E-03	2.7050484E-03	1.8566435E-01	-22.774823	1.7118873E-01	-7.1972614E-02

tual List Sizes for the preceding solution follow. 05-Apr-94 15.13.23

Size 1-10:	11	9	9	2	-9999	0	-9999	-9999	0	0
Size 11-20:	-9999	-9999	-9999	-9999	-9999	0	0	9	23	0
Size 21-29:	0	-9999	9	-9999	-9999	-9999	-9999	-9999	-9999	-9999
conds for overlays 1-5 :	23.680	0.000	23.680	---	(CP: 1/0; tot)					
conds for overlays 6-11 :	10.387	0.000	10.387							
conds for overlays 12-15 :	0.000	0.000	0.000							
conds for time-step loop :	0.000	0.000	0.000							
conds after DELTAT-loop :	0.383	0.000	0.383							

Totals : 34.449 0.000 34.449

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 110
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

DATA:C:\RIV\EMIN\PROBE3.DAT(06-04-94 11:20:RETONO Y AGREGO DATOS DE ARCH
RED 132 KV LA RIGJA; DATOS DE RED FLU132E.WQ1 12-12-93)
CASO 110; LINEA=CHAMI[5], CHEP[6] Y CHEP[60, LUJ[7] EN 240 MM2
BASE

GIN NEW DATA CASE

INTED NUMBER WIDTH, 13, 2, { Request maximum precision for 8 output columns
X SOURCE { An EMTP load flow will satisfy requested phasor power injections.
WER FREQUENCY, 50.0,

MISCELANEA CARD SIGUE II B-1, II B-2

34567890123456789012345678901234567890123456789012345678901234567890
DELTAT TMAX XOPT COPT EPSILN TOLMAT
000200 .000 50.50.(T-max = 0 means that no transient solution follows
IOUT IFLOT IDOUBL KSGOUT MAXOUT IPUN MENSAY ICAT NERERG IPRSUP
1-8 2-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
1 1 1 0 1

CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.

BASE 100 MVA =1; UR=132 KV

SIGUE FORMATO RULE BOOK 4A-2

34567890123456789012345678901234567890123456789012345678901234567890
BUS1 BUS2 BUS3 BUS4 REGIS XL XC OUTPUT OPTION
A6 A6 A6 A6 E6.2 E6.2 E6.2 II
3-8 9-14 15-20 21-26 27-32 33-38 39-44 80

LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)

EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;3=I y V DE RAMA; 4=CONSUMO POT Y ENERE

RECRE LARIO	0.11	0.22	4
LARIO AINOS	.16	.30	4
LARIO PATQU	.08	.16	4
PATQU CHAMI	.08	.16	4
PATQU NONOS	.14	.26	4
CHAMI CHEPE	.11	.35	4
CHEPE LUJAN	.105	.34	4
NONOS VUNIO	.11	.21	4
NONOS CHILE	.01	.02	4
LARIO NONOS	.08	.16	4

ANK card ending branch cards.

ANK card ending switch cards.

SOURCE CARD SIGUE FORMATO RULE BOOK VII-4

34567890123456789012345678901234567890123456789012345678901234567890
NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP
12 A6 12 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6
1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

LUJAN	1.10	50.	15.0	-1.
RECRE	1.10	50.	15.0	-1.

ANK card terminating all EMTP source cards.

Next come power constraints of the load flow. There will be one
for each non-slack generator. So, 3 of them will apply to nodes

that have no Type-14 source as required by the algorithm. The program will define these internally. Yet, this is only possible for THAX non-positive (no transient continuation). If data is modified to make THAX > 0, a KILL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data. Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4703 = 1.414 + 1.02

VALORES DE POTENCIA EN FU 1=100 MVA

PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4;10-6

34567890123456789012345678901234567890123456789012345678901234567890

NKBUS1	BUS2	BUS3	PK or BK	BK or VK	VMIN	VMAX	THMIN	THMAX
1-2	3-8	9-14	15-20	21-36	37-52	53-60	61-68	69-74 75-80

LARIO			-0.4000		-0.200	.65	1.25	
CHAMI			-0.080		-.034	.65	1.25	
PATBU			-0.150		-.080	.65	1.25	
NONOG			-0.10		-.061	.65	1.25	
VUNIO			-.0600		-.02	.65	1.25	
LUGAN		1.0			1.20			-20. 40.
RECKE		0.8			1.10			-20. 15.
CHEFE		-.16			-.09		1.3	
AINOG		-0.090			-0.04	.65	1.15	
CHILE		-.1000			-.04		1.15	

The following load-flow miscellaneous data card has two peculiarities. The use of VSCALE = 1.414 is the special flag requesting RMS rather than peak voltages. The use of KTAPER = 0 ensures constant acceleration factors (this works well for this problem whether RMS or peak values are used).

NNOUT	NITERA	NFOUT	NPRINT	RALCHK	CFITEV	CFITEA	VSCALE	KTAPER
10-16	17-24	25-32	33-40	41-48	50-56	57-64		
1	2500	20	1	.01	0.2	2.5	1.414	2

PUNCH (Flush punched cards: R-L branches for equivalent impedance loads

ANK card ending requests for output variables

ANK card ending plot cards

EGIN NEW DATA CASE

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
Date (dd-mth-yy) and time of day (hh.mm.ss) = 06-Apr-94 11.24.05 Name of disk plot file, if any, is C:\44061124.pl4
For information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
Total length of "LARGO" tables = 444863 INTEGER words. "VAROIN" List Sizes follow: 752 900 1500 150 7500
120 2100 5250 225 480 150 150 15000 60 64800 120 12 15 4800 1980 300 450 12000 9 1200 252 4

Descriptive interpretation of input data cards. Input data card images are shown below, all 80 columns, character by character
0 1 2 3 4 5 6 7 8
012345678901234567890123456789012345678901234567890123456789012345678901234567890

Comment card. KOMPAT = 1. IC DATA: C:\RIV\EMIN\PROBE4.DAT
Comment card. KOMPAT = 1. IC DATA: C:\RIV\EMIN\PROBE3.DAT (-06-04-94 11:20; RETOMO Y ABREGO DATOS DE ARCH
Comment card. KOMPAT = 1. IC RED 132 KV LA RIOJA; DATOS DE RED FLU132E.W01 12-12-93}
Comment card. KOMPAT = 1. IC CASO 110; LINEA CHAMI(3), CHEPE(6) Y CHEPE(50, LUJ(7) EN 240 MW2
Case all of 0 cards in the punch buffer. ;ERASE
Marker card preceding new EMTP data case. ;BEGIN NEW DATA CASE
Width of time-step loop numbers. W=13 S=2 ;PRINTED NUMBER WIDTH, 13, 2, { Request maximum precision for 8 output columns
Declaration of desired EMTP load flow usage. ;FIX SOURCE { An EMTP load flow will satisfy requested phasor power injections.
Power frequency STATFR = 5.00000000E+01 Hz. ;POWER FREQUENCY, 50.0,
Comment card. KOMPAT = 1. IC MISCELANEA CARD SIGUE II B-1, II B-2
Comment card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
Comment card. KOMPAT = 1. IC DELTAT THAX XDPT COPT EPSILN TOLMAT
sc. data. 2.000E-04 0.000E+00 5.000E+01 ; .000200 .000 50.50. { T-max = 0 means that no transient solution follows
Comment card. KOMPAT = 1. IC IOUT IPLOT IDOUBL KSSOUT MAXOUT IPUN MENSAR ICAT NERERG IPRSUP
Comment card. KOMPAT = 1. IC 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
sc. data. 1 1 0 1 0 1 0 0 0 0 ; 1 1 1 0 1
Comment card. KOMPAT = 1. IC
Comment card. KOMPAT = 1. IC CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.
Comment card. KOMPAT = 1. IC BASE 100 MVA =1; UR=132 KV
Comment card. KOMPAT = 1. IC SIGUE FORMATO RULE BOOK 4A-2
Comment card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
Comment card. KOMPAT = 1. IC BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
Comment card. KOMPAT = 1. IC A6 A6 A6 A6 E6.2 E6.2 E6.2 11
Comment card. KOMPAT = 1. IC 3-8 9-14 15-20 21-26 27-32 33-38 39-44 50
Comment card. KOMPAT = 1. IC LAS OPCIONES DE SALIDA SON: {IV-A.2 RULE BOOK ACTUALIZ}
Comment card. KOMPAT = 1. IC EN 80 1=CORRIENTE RAMA; 2=VOLT RAMA; 3=I y V DE RAMA; 4=CONSUMO POT Y ENERG
ries R-L-C. 1.100E-01 7.003E-04 0.000E+00 ; RECRE LARIO 0.11 0.22 4
ries R-L-C. 1.600E-01 9.549E-04 0.000E+00 ; LARIO AINOG .16 .30 4
ries R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; LARIO PATQU .08 .16 4
ries R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; PATQU CHAMI .08 .16 4
Comment card. KOMPAT = 1. IC PATQU NONOG .14 .26 4
ries R-L-C. 1.100E-01 1.114E-03 0.000E+00 ; CHAMI CHEPE .11 .35 4
ries R-L-C. 1.050E-01 1.082E-03 0.000E+00 ; CHEPE LUJAN .105 .34 4
ries R-L-C. 1.100E-01 6.685E-04 0.000E+00 ; NONOG VUNIO .11 .21 4
ries R-L-C. 1.000E-02 6.366E-05 0.000E+00 ; NONOG CHILE .01 .02 4
ries R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; LARIO NONOG .08 .16 4
Comment card. KOMPAT = 1. IC
Comment card. KOMPAT = 1. IC
Blank card ending branches. IRR, NTOT = 9 11 ;BLANK card ending branch cards.
Blank card ending switches. KSWTCH = 0. ;BLANK card ending switch cards.
Comment card. KOMPAT = 1. IC SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
Comment card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890

```
oment card. KOMPAR = 1.          IC NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP
oment card. KOMPAR = 1.          IC 12 A6 12 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6
oment card. KOMPAR = 1.          IC 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
oment card. KOMPAR = 1.          IC
ource. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114LUJAN 1.10 50. 15.0 -1.
ource. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114RECRE 1.10 50. 15.0 -1.
oment card. KOMPAR = 1.          IC
oment card. KOMPAR = 1.          IC
ank card ends electric network sources. BLANK card terminating all EMTP source cards.
oment card. KOMPAR = 1.          IC Next come power constraints of the load flow. There will be one
oment card. KOMPAR = 1.          IC for each non-slack generator. So, 3 of them will apply to nodes
oment card. KOMPAR = 1.          IC that have no Type-14 source as required by the algorithm. The
oment card. KOMPAR = 1.          IC program will define these internally. Yet, this is only possible
oment card. KOMPAR = 1.          IC for TMAX non-positive (no transient continuation). If data is
oment card. KOMPAR = 1.          IC modified to make TMAX > 0, a KILL = 40 error termination will
oment card. KOMPAR = 1.          IC will result. Yet, the transient simulation is possible as a
oment card. KOMPAR = 1.          IC 2nd simulation that replaces the power constraints at load nodes
oment card. KOMPAR = 1.          IC by constant-impedance loads. Branch cards for these will be
oment card. KOMPAR = 1.          IC punched by the present subcase, and the transient continuation
oment card. KOMPAR = 1.          IC will be illustrated by the following (4th of 4) subcase.
oment card. KOMPAR = 1.          IC The following 4 cards would be used if peak rather than RMS input data.
oment card. KOMPAR = 1.          IC Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.826428 ) = 1.414212
oment card. KOMPAR = 1.          IC (power constraints RED, BLUE, and YELLOW), and 1.4706 = 1.414 + 1.02
oment card. KOMPAR = 1.          IC
oment card. KOMPAR = 1.          IC VALORES DE POTENCIA EN PU 1=100 MVA
oment card. KOMPAR = 1.          IC PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4:10-4
oment card. KOMPAR = 1.          IC 34567890123456789012345678901234567890123456789012345678901234567890
oment card. KOMPAR = 1.          IC NKBUS1 BUS2 BUS3 PK or BK BK or VK VMIN VMAX THMIN THMAX
oment card. KOMPAR = 1.          IC 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
X. -4.000E-01 -2.000E-01 6.500E-01 1.250E+00 LARIO -0.4000 -0.200 .65 1.25
X. -8.000E-02 -3.400E-02 6.500E-01 1.250E+00 CHAMI -0.080 -0.034 .65 1.25
X. -1.500E-01 -8.000E-02 6.500E-01 1.250E+00 PATOU -0.150 -0.080 .65 1.25
X. -1.000E-01 -6.100E-02 6.500E-01 1.250E+00 NONOG -0.10 -0.061 .65 1.25
X. -6.000E-02 -2.000E-02 6.500E-01 1.250E+00 VUNIO -0.0600 -0.02 .65 1.25
oment card. KOMPAR = 1.          IC LUJAN 1.0 1.20 -20. 40.
X. 8.000E-01 1.100E+00 0.000E+00 1.000E+19 IRECRE 0.8 1.10 -20. 15.
X. -1.600E-01 -9.000E-02 0.000E+00 1.500E+00 CHEPE -.16 -.09 1.5
X. -9.000E-02 -4.000E-02 6.500E-01 1.150E+00 AIMOG -0.090 -0.04 .65 1.15
X. -1.000E-01 -4.000E-02 0.000E+00 1.150E+00 CHILE -.1000 -.04 1.15
oment card. KOMPAR = 1.          IC The following load-flow miscellaneous data card has two peculiarities. The
oment card. KOMPAR = 1.          IC use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
oment card. KOMPAR = 1.          IC voltages. The use of XTAPER = 0 ensures constant acceleration factors
oment card. KOMPAR = 1.          IC (this works well for this problem whether RMS or peak values are used).
oment card. KOMPAR = 1.          IC NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE XTAPER
oment card. KOMPAR = 1.          IC 10-16 17-24 25-32 33-40 41-48 50-56 57-64
= LASTOV, NTOT, NEXT, IOFKOL, IOFKOR, NCURR = 9 11 19 0 0 0
ad flow iter. 1 2500 20 1 1.00E-02 1 2500 20 1 .01 0.2 2.5 1.414 2
x del-V: .0232 .0227 .0223 .0218 .0213 .0209 .0204 .0149 .0152 .0149 .0137 .0136 .0134 .0133 .0131 .0129 .0127 .0125 .0124 .0126
ource No. 1 -4 -4 -4 -4 -4 -4 -9 -9 -9 -5 -5 -5 -5 -5 -5 -5 -5 -5 -5
x del-V: .0128 .013 .0131 .0112 .0111 .0109 .0106 .0105 .0108 .0106 .0108 .0115 .0116 .0105 .0115 .0117 .0113 .0102 .0113 .0107
ource No. 7 7 7 -5 -5 4 -5 5 4 4 9 -9 -4 -4 -9 -4 -4 -4 5 -5 -4
x del-V: .0114 .0108 .0113 .0105 .0114 .0107 .0113 .0102 .0113 .0103 .011 .0117 .0117 .0124 .0102 .0111 .0118 .012 .0135 .0105
```


[illegible]

[illegible]

Source No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4
x del-V:	.0114	.0117	.0114	.0117	.0114	.0117	.0113	.0117	.0113	.0117	.0113	.0117	.0112	.0117	.0112	.0117	.0112	.0117	.0112	.0117
Source No.	9	4	9	4	9	4	9	4	9	4	9	4	-4	4	-4	4	-4	4	-4	4
x del-V:	.0112	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4
x del-V:	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118	.0113	.0118
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4
x del-V:	.0112	.0116	.0111	.0114	.0108	.0111	.0104	.0107	.01	.0102	.0095	.0096	.0089	.009	.0083	.0084	.0077	.0077	.007	.0071
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4
x del-V:	.0063	.0064	.0057	.0057	.005	.0051	.0044	.0045	.0038	.0039	.0033	.0034	.0028	.0029	.0024	.0024	.002	.002	.0017	.0017
Source No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	9	4	9	4	9	4
x del-V:	.0014	.0014	.0012	.0012	.9E-3	.9E-3	.8E-3	.8E-3	.6E-3											
Source No.	9	4	9	4	9	4	9	4	9											

At the load flow iteration loop with counter NEKITE = 1209. If no warning on the preceding line, convergence was attained.

Row	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	3	LARIO	8.89848959E-01	-3.80873	-4.04020805E-01	-2.03048523E-01
4	6	CHAMI	9.05428077E-01	0.16103	-8.18270015E-02	-3.56048400E-02
5	5	FATOU	8.82701331E-01	-2.45285	-1.52497678E-01	-8.17911190E-02
6	9	NONOG	8.33623352E-01	-6.21261	-7.08492787E-02	-5.03486506E-02
7	10	VUNIO	8.24732153E-01	-7.03372	-6.01987321E-02	-2.43593172E-02
2	2	RECRE	1.10000000E+00	2.04657	7.92761431E-01	6.78039071E-01
8	7	CHEPE	9.70934254E-01	7.05285	-1.60428259E-01	-9.08059684E-02
9	4	AIMOG	8.57252277E-01	-5.40203	-9.32589514E-02	-4.23486528E-02
10	11	CHILE	8.36738430E-01	-6.33785	-1.09194030E-01	-5.54031841E-02

sinusoidal steady-state phasor solution, branch by branch. All flows are away from a bus. and the real part, magnitude, or "P"
 printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus X	Bus M	Phasor node voltage		Phasor branch current		Power flow P and Q	Power loss P and Q
		Rectangular	Polar	Rectangular	Polar		
RECRE	7	1.5546456346272	1.5556349186104	1.0496480231542	1.3411526246414	.77276143126438	.09892796994204
		.05547026866898	2.0434654	-.8348229693001	-38.4964972	.67803907148634	0.1978959
LARIO	LARIO	1.2555232988362	1.2583049528123	-1.049648023154	1.3411526246414	-.6838334613223	
		-.0836217696019	-3.8104500	.83482296930006	141.5035028	-.4891831316923	
LARIO	LARIO	1.2555232988362	1.2583049528123	.14659910010062	.16898272912901	.09554336445337	.00228441301951
		-.0836217696019	-3.8104500	-.084046811918	-29.8261026	.04663192719174	0.0042633
AIMOG	AIMOG	1.2068533992447	1.2122401846189	-.1465991001006	.16898272912901	-.0932589514339	
		-.1141540097252	-5.4034244	.08404681191799	130.1738974	-.0423486527802	
LARIO	LARIO	1.2555232988362	1.2583049528123	-.1296428897114	.17513153600272	-.0765966062631	.00122664219611
		-.0836217696019	-3.8104500	-.1175239502998	-137.8509909	.07920587499028	0.0024537
FATOU	FATOU	1.2471068979652	1.2482515700127	.12984288971139	.17513153600272	.0778234484592	
		-.0534449912241	-2.4539194	.11752395029979	42.1490091	-.0767521905581	
FATOU	FATOU	1.2471068979652	1.2482515700127	-.3683458960794	.36911828709613	-.2303211265575	.00544993239475
		-.0534449912241	-2.4539194	.02386651860333	176.2927727	-.0050389283586	0.01089799
CHAMI	CHAMI	1.280393212628	1.2803982203692	.36834589607941	.36911828709613	.2357710592523	

Path: C:\ATP

File: AP61125 .SAL 40.173 .a.. 06-04-94 11:24:40

Page 6

	.00358103066031	0.1602456	-.0238665186033	-3.7972273	.001593873316811	
CHAMI	1.280393212628	1.2803982203692	-.4963158669284	.50258338703058	-.3175980607765	.01389245333055
	.00358103066031	0.1602456	.07912408706717	170.9419692	-.0515436331864	0.0442033
CHEPE	1.3626813884637	1.3730704490764	.49631586692843	.50258338703058	.33145051412705	
	.16858793450787	7.0526702	-.0791240870672	-7.0530308	.09574689384728	
CHEPE	1.3626813884637	1.3730704490764	-.7444658766525	.76631843595364	-.4919187729672	.03083030712733
	.16858793450787	7.0526702	.18169893720791	166.2841848	-.1865328622466	0.0998315
LUJAN	1.5026279441629	1.5556349186104	.74446587665248	.76631843595364	.52274908009457	
	.40262794416288	15.0000000	-.1816989372079	-13.7158152	.28638433274465	
NDNOG	1.1794668861286	1.1864257688768	.09734877138892	.11137362356051	.06088095671741	.68222462137E-3
	-.1283120009229	-6.2086848	-.0541045352449	-23.0644457	.02566174603322	0.0013024
VUNIO	1.1573965628744	1.166173111915	-.0973487713889	.11137362356051	-.060198732096	
	-.1428037440376	-7.0338096	.0541045352449	150.9355543	-.0243593172106	
NDNOG	1.1794668861286	1.1864257688768	.1731727383279	.20706021017633	.10940839983566	.21436965319E-3
	-.1283120009229	-6.2086848	-.113512317528	-33.2442449	.05533192343033	0.0004287
CHILE	1.1754649098797	1.1827022669092	-.1731727383279	.20706021017633	-.1091940301825	
	-.1306403375443	-6.3417867	.11351231752795	146.7557551	-.0554031841339	
LARIO	1.2555232988362	1.2583049528123	.41359218817384	.49313354128363	.27086589862674	.00372724336184
	-.0836217696019	-3.8104500	-.2685564852355	-32.9967432	.15129680679071	0.0134585
NDNOG	1.1794668861286	1.1864257688768	-.4135921881738	.49313354128363	-.2611386552649	
	-.1283120009229	-6.2086848	.26855648523554	147.0032568	-.131842320067	
Total network loss P-loss by summing injections = 1.632357556667E-01						

solution at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed result applying to the composite group. The entry "MVA" is $\text{SQR}(\text{P}^2 + \text{Q}^2)$ in units of power, while "P.F." is the associated power factor.

Node name	Source node voltage Rectangular	Source node voltage Polar	Injected source current Rectangular	Injected source current Polar	Injected source power P and Q	MVA and P.F.
RECRE	1.5546456346292	1.5556349186104	1.0496480231542	1.3411526246414	.77276143126438	1.0431719270391
	.05547026886898	2.0434654	-.8348229673001	-38.4964972	.67803907148634	0.7599528
LARIO	1.2555232988362	1.2583049528123	-.6192996243711	.71870369019806	-.4040208045053	.43217420649034
	-.0836217696019	-3.8104500	.36469572184674	149.5068440	-.2030485226295	-0.8935070
AINOG	1.2068533992447	1.2122401846189	-.1465991001006	.16898272912901	-.0932589514335	.10242381737938
	-.1141540097252	-5.4034244	.08404681191799	150.1738974	-.0423486527802	-0.9105201
PATBU	1.2471068979652	1.2482515700127	-.236503006368	.27726332022687	-.1524976783983	.17304718739007
	-.0534449912241	-2.4539194	.14133046399312	149.3354914	-.0317911189967	-0.8812491
CHAMI	1.280393212628	1.2803982203692	-.127669770849	.13934050274634	-.0818270015242	.09923767575443

```
seconds after DELTAT-loop :    0.328    0.000    0.328
```

Path: C:\ATP

File: AP61125 .SAL 40.173 .a.. 06-04-94 11:24:40

Page 8

Totals : 35.164 0.000 35.164

CASO 130

C:\RIV\FLULSA\

flul32e.wq1(2-12-93)

ENERGIA [GWH]

BARRA ANO1991 ANO1991#
CIRCUITO

Arauco	3	1.623E+01	1.8E+01
Capital	2	1.443E+02	1.6E+02
Castro Barros	3	1.830E+00	2.0E+00
Chilecito	10	4.439E+01	4.9E+01
Famatina	10	2.341E+00	2.6E+00
Gen.Penalzoa	5	9.300E-01	1.0E+00
G.Belgrano	5	2.450E+00	2.7E+00
G.F.Guiroga	5	6.700E-01	7.4E-01
G.Lamadrid	9	4.880E-01	5.4E-01
G.Lavalle	9	3.400E+00	3.7E+00
G.Ocampo	5	1.925E+00	2.1E+00
G.S.Martin	6	1.010E+00	1.1E+00
G.Sarmiento	9	8.380E-01	9.2E-01
Bob.Gordillo	5	5.975E+00	6.6E+00
Independencia	4	6.010E-01	6.6E-01
R.V.Penalzoa	6	3.751E+00	4.1E+00
Sanagasta	2	7.170E-01	7.9E-01
S.B.de los Sauces	3	1.177E+00	1.3E+00
Total La Rioja		2.331E+02	2.6E+02

*[INCLUYE PERDIDAS] FUENTE :EPELAR 1993

DATOS ACTIVOS

VALORES DE CRECIMIENTO EN NODOS [TAS. AN.AC.= 5%]

	1991	1993	1995	2000	2005	2010	2013
LOCALIDAD	BARRA	ENERGIA					
RECREO	1	0.000E+00					
LA RIOJA	2	1.596E+02	1.759E+02	1.9E+02	2.48E+02	3.159E+02	4.03E+02
AIMOGASTA	3	2.116E+01	2.333E+01	2.6E+01	3.28E+01	4.190E+01	5.35E+01
PATOUJA	4	6.611E-01	7.289E-01	8.0E-01	1.03E+00	1.309E+00	1.67E+00
CHAMICAL	5	1.315E+01	1.449E+01	1.6E+01	2.04E+01	2.603E+01	3.32E+01
CHEPES	6	5.237E+00	5.774E+00	6.4E+00	8.12E+00	1.037E+01	1.32E+01
LUJAN	7	0.000E+00	0.000E+00	0.0E+00	0.00E+00	0.00E+00	0.00E+00
NONOGASTA	8	1.000E+01	1.103E+01	1.2E+01	1.55E+01	1.980E+01	2.53E+01
V.UNION	9	5.199E+00	5.731E+00	6.3E+00	8.06E+00	1.029E+01	1.31E+01
CHILECITO	10	4.140E+01	4.565E+01	5.0E+01	6.42E+01	8.198E+01	1.05E+02
TOTAL		2.564E+02	2.826E+02	3.1E+02	3.98E+02	5.076E+02	6.48E+02

R[OHM]= RO[OHM*mm^2/m] Ro(Al)=1/37= 2.70E-02

d12[m]= 5.200E+00 Ro(Cu)=1/52= 1.92E-02

d13[m]= 3.310E+00 Seccion [mm^2]= 1.50E+02

d23[m]= 6.160E+00 React.induc.[ohm/k4.23E-01

Cap.a t.[mf/km]= 1.04E-03

VALORES ELECTRICOS Suc.[2*pi*50*47] 3.28E-01 umho/km/f

ojo revisar suceptancia L[mHy/km]X1[ohm/km]

1.35E-03 4.231E-01

DE	A	DIST[KM]	R [OHM]	XL [J O]	Sucep	XC[-j OHM]	R (1/1)	XI(1/1)	XC (1/1)
					umho/km/f				
1	2	185.00	16.67	39.14	9.6E+02	1.93E-01	0.10	0.22	1.11E-03
2	3	130.00	23.42	55.00	7.4E+00	1.36E-01	0.13	0.32	7.79E-04
2	4	69.00	12.43	29.19	1.4E+01	7.20E-02	0.07	0.17	4.13E-04

Red Patricio Naves

4	5	68.00	12.25	28.77	1.4E+01	7.10E-02	0.07	0.17	4.07E-04
5	6	158.00	28.47	66.85	6.1E+00	1.65E-01	0.16	0.38	9.47E-04
6	7	114	20.54	48.23	8.4E+00	1.19E-01	0.12	0.28	6.83E-04
7	8	151.00	27.21	63.89	6.3E+00	1.58E-01	0.16	0.37	9.05E-04
8	9	92.00	16.58	38.93	1.0E+01	9.60E-02	0.10	0.22	5.51E-04
9	10	13.00	2.34	5.50	7.4E+01	1.36E-02	0.01	0.03	7.79E-05

LA LINEA ENTRE RECREO Y LA RIOJA ES DOBLE TERNA

TENSION BASE: 132 [KV]; POTENCIA BASE: 100 [MVA]

IMPEDANCIA BASE=((TENSION BASE[kv])^2)/POTENCIA BASE [MVA]

ZB[OHM]= 1.742E+02

ANO 1991

VALORES VOLCADOS A BASE ELEGIDA [MVA] 1.0E+02

LOCALIDAD	BARRA	ACAR	REACAR	CAREST	ACTGEN	REMAX	REMIN	T
RECREO	1	0.000E+00	0.000E+00		1.40E+02			
LA RIOJA	2	1.596E+02	4.787E+01		1.15E+02			
AINOGASTA	3	2.116E+01	6.348E+00			0.000E+00	1.800E+00	†
PATQUIA	4	6.611E-01	1.983E-01					
CHAMICAL	5	1.315E+01	3.944E+00		3.40E-01			
CHEPES	6	5.237E+00	1.571E+00					
LUJAN	7	0.000E+00	0.000E+00					
NONOGASTA	8	1.000E+01	3.000E+00					
V.UNION	9	5.199E+00	1.560E+00		5.35E+00			
CHILECITO	10	4.140E+01	1.242E+01		2.95E+00	8.850E-01	8.000E-01	

LOCALIDAD	BARRA	ENERGIA GWH	FAC.UTIL. [HORAS]	C.MAX MW
RECREO	1	0.000E+00		
LA RIOJA	2	1.596E+02	3000	53.19
AINOGASTA	3	2.116E+01	4200	5.04
PATQUIA	4	6.611E-01	3200	0.21
CHAMICAL	5	1.315E+01	3200	4.11
CHEPES	6	5.237E+00	3200	1.64
LUJAN	7	0.000E+00		
NONOGASTA	8	1.000E+01	3200	3.13
V.UNION	9	5.199E+00	3400	1.53
CHILECITO	10	4.140E+01	3600	11.50
TOTAL		2.564E+02		

VALORES DE CRECIMIENTO EN NODOS [TAS. AN.AC.= 5%]

DATOS ACTIVOS

1993 1995 2000 2005 2010 2013

1.76E+02 1.939E+02 2.475E+02 3.159E+02 4.0E+02 5.15E+02
2.33E+01 2.572E+01 3.283E+01 4.190E+01 5.3E+01 6.82E+01
7.29E-01 8.036E-01 1.026E+00 1.309E+00 1.7E+00 2.13E+00

1.45E+01 1.598E+01 2.039E+01 2.603E+01 3.3E+01 4.24E+01
5.77E+00 6.366E+00 8.124E+00 1.037E+01 1.3E+01 1.69E+01
0.00E+00 0.000E+00 0.000E+00 0.000E+00 0.0E+00 0.00E+00
1.10E+01 1.216E+01 1.551E+01 1.980E+01 2.5E+01 3.23E+01
5.73E+00 6.319E+00 8.065E+00 1.029E+01 1.3E+01 1.68E+01
4.56E+01 5.033E+01 6.423E+01 8.198E+01 1.0E+02 1.34E+02
2.83E+02 3.116E+02 3.977E+02 5.076E+02 6.5E+02 8.27E+02

ASIGNACION DE FACTOR DE UTILIZACION A CADA NODO

BARRA	ENERGIA GWH	FAC.UTIL. [HORAS]	C.MAX MW
1	0.000E+00		
2	1.596E+02	3000	53.19
3	2.116E+01	4200	5.04
4	6.611E-01	3200	0.21
5	1.315E+01	3200	4.11
6	5.237E+00	3200	1.64
7	0.000E+00		0.00
8	1.000E+01	3200	3.13
9	5.199E+00	3400	1.53
10	4.140E+01	3600	11.50
	2.564E+02		

1991

BARRA	ACAR	REACAR	CAREST	ACTGEN	REMAX
1		0.00		139.57	
2	53.19	15.96		114.57	
3	5.04	1.51			0.00
4	0.21	0.06			
5	4.11	1.23		0.34	
6	1.64	0.49			
7	0.00	0.00			
8	3.13	0.94			
9	1.53	0.46		5.35	
10	11.50	3.45		2.95	0.89

TOTAL

VALOR DE LA SUCEPTANCIA EXPRESADA EN MVAR

Cap.a t.[mf/km]= 1.04E-03
Suc.[2*pi*50*f*47] 3.28E-01 umho/km/f
Suc[mvar]=U^2*2*pi*50*C[uF]*(f166)

DE	A	DIST[KM]	R [OHM]	XL [J O]	CAP uF	Suc MVar
1	2	185.00	16.67	39.14	1.9E-01	5.29E+05
2	3	130.00	23.42	55.00	1.4E-01	3.71E+05
2	4	69.00	12.43	29.19	7.2E-02	1.97E+05
4	5	68.00	12.25	28.77	7.1E-02	1.94E+05

5	6	158.00	28.47	66.85	1.6E-01	4.51E+05
5	8	114	20.54	48.23	1.2E-01	3.26E+05
6	7	151.00	27.21	63.89	1.6E-01	4.31E+05
8	9	92.00	16.58	38.93	9.6E-02	2.63E+05
8	10	13.00	2.34	5.50	1.4E-02	3.71E+04

DATOS ELABORADOS PARA EMTP
LOS DATOS DE RAMA DEBEN PRESENTARSE EN TANTO POR UNO COMO
RESISTENCIA INDUCTANCIA Y CAPACIDAD

VALOR DE LA SUCEPTANCIA EXPRESADA EN MVAR

Cap.a t.[mf/km]= 1.04E-03
Suc.[2*pi*50*f47] 3.28E-01 umho/km/f

DE	A	DIST[KM]	R [OHM] 1/1	XL [J O] Xl 1/1	CAP QC*Km1/1
1	2	185.00	0.10	0.22	3.5E-01
2	3	130.00	0.13	0.32	2.4E-01
2	4	69.00	0.07	0.17	1.3E-01
4	5	68.00	0.07	0.17	1.3E-01
5	6	158.00	0.16	0.38	3.0E-01
5	8	114	0.12	0.28	2.1E-01
6	7	151.00	0.16	0.37	2.8E-01
8	9	92.00	0.10	0.22	1.7E-01
8	10	13.00	0.01	0.03	2.4E-02

Cap.a t. [mf/km]= 1,04E-03
Suc. [2*pi*50*f47] 3,28E-01 µmho/km/f
Suc [mvaR]=U^2*2*pi*50*C [µF] (f 166)

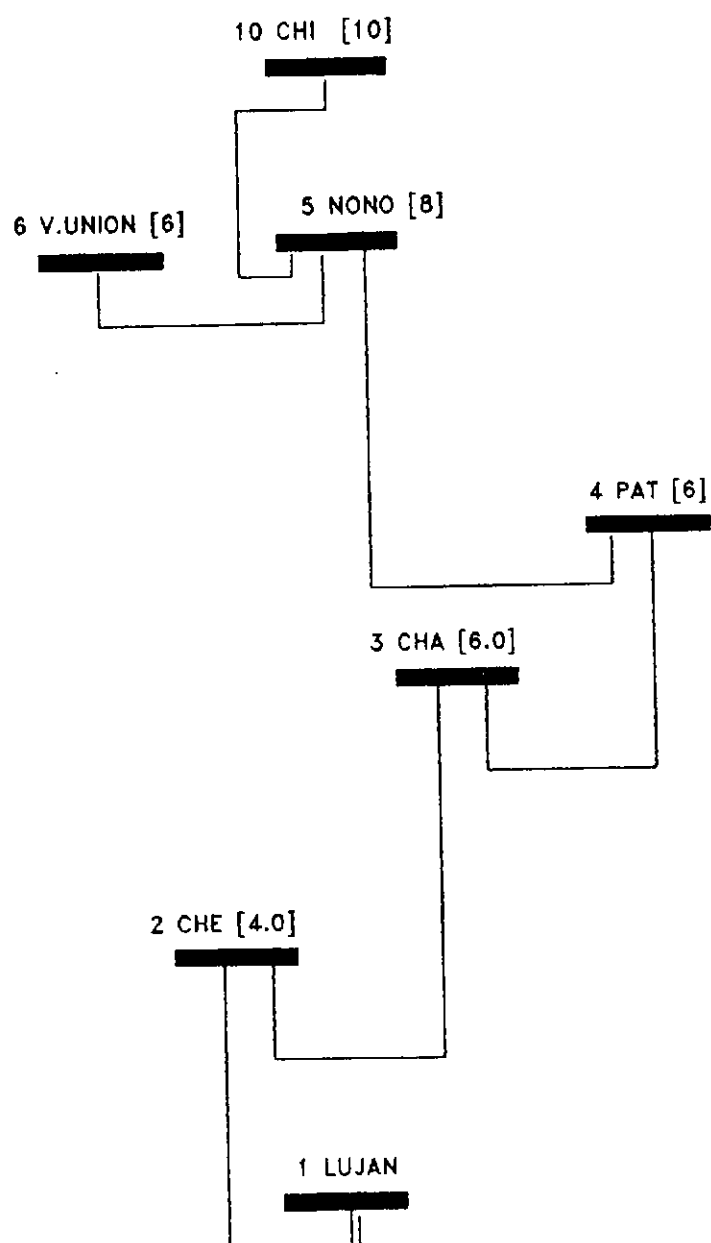
DE	A	DIST [KM]	R [OHM]	XL [J 0	CAP µF	Suc MVAr
1	2	185,00	19,43	38,67	1,93E-01	5,286E+05
2	3	130,00	23,42	55,00	1,36E-01	3,715E+05
2	4	69,00	12,43	29,19	7,20E-02	1,972E+05
4	5	68,00	12,25	28,77	7,10E-02	1,943E+05
5	6	158,00	28,47	66,85	1,65E-01	4,515E+05
4	8	114	20,54	48,23	1,19E-01	3,257E+05
6	7	151,00	27,21	63,89	1,58E-01	4,315E+05
8	9	92,00	16,58	38,93	9,60E-02	2,629E+05
8	10	13,00	2,34	5,50	1,36E-02	3,715E+04

LA IMPEDANCIA RECREO-LA RIOJA ES DOBLE TERNA SU VALOR ES:
z [OHM/KM]= 0.105 + j 0.209
DATOS ELABORADOS PARA EMTF
LOS DATOS DE RAMA DEBEN PRESENTARSE EN TANTO POR UNO COMO
RESISTENCIA INDUCTANCIA Y CAPACIDAD

VALOR DE LA SUCEPTANCIA EXPRESADA EN MVAR
Cap.a t. [mf/km]= 1,04E-03
Suc. [2*pi*50*f47] 3,28E-01 µmho/km/f

DE	A	DIST [KM]	R [OHM] 1/1	XL [J 0 X1 1/1	CAP RC*Km1/1
1	2	185,00	0,10	0,22	3,48E-01
2	3	130,00	0,13	0,32	2,45E-01
2	4	69,00	0,07	0,17	1,30E-01
4	5	68,00	0,07	0,17	1,28E-01
5	6	158,00	0,16	0,38	2,97E-01
4	8	114	0,12	0,28	2,15E-01
6	7	151,00	0,16	0,37	2,84E-01
8	9	92,00	0,10	0,22	1,73E-01
8	10	13,00	0,01	0,03	2,45E-02

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 160
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

CASO 160

TARJETA CODIGO 2. TITULO)

EMA LA RIOJA - CASO: FLUJO132-V.UNION LUJAN 5/04/93-11:07

TARJETA CODIGO 1. TITULO)

SEGURACION 1 - POTENCIA GENERADA 35 MW - X TRANSFORMADORES

(LOTE MISCELANEO)

0. 20 .00001 1 0 0 0

NODOS

002 LUJAN	1.1	35.0	10.0	7.0	20.0		
0 CHEPES						4.0	3.0
0 CHAMICAL						6.0	0.1 10.0
0 PATQUIA						6.0	2.9
0 NONOGASTA						8.0	6.0
1 V.UNION	1.1	20.0	15.0	4.0	18.0	6.0	4.0

(DATOS DE RAMAS EN %)

00	002	0	0	11.71	24.21	00.000	1.02	.700	1.20
00	003	0	0	11.47823.73	0.0		1.1		
00	004	0	0	6.82514.11					
00	005	0	0	11.19	23.13				
00	006	0	0	9.82420.31					

(ORDENA EJECUCION DE LOS CALCULOS)

POTENCIA BASE MVA . 100.0
NUMERO MAXIMO DE ITERACIONES 20
TOLERANCIA DE LA CONVERGENCIA .00001000

ONFIGURACION 1 - POTENCIA GENERADA 35 MW - X TRANSFORMADORES

PAGINA 2

DATOS DE LAS BARRAS

NUMERO	NOMBRE	TIPO	TENSION	POTENCIA GENERADA		POTENCIA CONSUMIDA		SHUNT
			PU	MW	MVAR	MW	MVAR	MVAR
1	LUJAN	2	1.1000	35.00	10.00	.00	.00	.00
2	CHEPES	0	1.0000	.00	.00	4.00	3.00	.00
3	CHAMICAL	0	1.0000	.00	.00	6.00	.10	10.00
4	PATQUIA	0	1.0000	.00	.00	6.00	2.90	.00
5	NONOGASTA	0	1.0000	.00	.00	8.00	6.00	.00
6	V.UNION	1	1.1000	20.00	15.00	6.00	4.00	.00

ONFIGURACION 1 - POTENCIA GENERADA 35 MW - X TRANSFORMADORES

PAGINA 3

DATOS DE LAS RAMAS

DE BARRA		A BARRA	NUMERO	CIRC. NUM.	RESISTENCIA	REACTANCIA	SUCEPTANCIA	TAP EN FASE
NUMERO	NOMBRE	NUMERO			PU	PU	PU	PU
1	LUJAN	2	CHEPES	0	.1171	.2421	.0000	1.0200
2	CHEPES	3	CHAMICAL	0	.1148	.2373	.0000	1.1000
3	CHAMICAL	4	PATQUIA	0	.0683	.1411	.0000	
4	PATQUIA	5	NONOGASTA	0	.1119	.2313	.0000	
5	NONOGASTA	6	V.UNION	0	.0982	.2031	.0000	

ONFIGURACION 1 - POTENCIA GENERADA 35 MW - X TRANSFORMADORES

PAGINA 4

INFORMACIONES CON RESPECTO AL SISTEMA

TOTAL DE BARRAS 6
TOTAL DE RAMAS ENTRE BARRAS 5
NUMERO DE RAMAS COMO LT 3
NUMERO DE TRAFOS.CON TAP 2
NUMERO DE TRAFOS.SIN TAP 0
NUMERO DE REACTORES DE BARRA 0
NUMERO DE CAPACITORES DE BARRA 1
NUMERO DE GENERADORES 2
NUMERO DE BARRAS (PQ) 4
BARRAS CON RESIDUOS ARRIBA DE LA TOLERANCIA

ITERACION BARRAS CON RESIDUOS DE POTENCIA ACTIVA Y REACTIVA ARRIBA DE LA TOLERANCIA DE .000010 - MAXIMO DE 22 BARRAS

1	2	3	4	5	6
	2	3	4	5	
2	2	3	4	5	6
	2	3	4	5	
3	2	3	4	5	6
	2	3	4	5	
4	2	3	4	5	6
	2	3	4	5	

IDENTIFICACION DE LA LINEA Y TRAFIO		REACTIVO	REACTIVO	PERDIDAS	PERDIDAS
BARRA	EMISORA	GEN.	CONSUMIDO	REACTIVAS	ACTIVAS
NUMERO	NOMBRE	NVAR	NVAR	NVAR	MW
1	LUJAN	.00	.56	.56	.24
2	CHEPES	.00	.70	.70	.91
3	CHEPES	.00	.05	.05	.02
4	PATQUIA	.00	.24	.24	.11
5	PATQUIA	.00	.75	.75	.36
		=====	=====	=====	=====
VALORES TOTALES		.00	2.29	2.29	1.65

200-1

CASO 200

flu132e.wq1[2-12-93]

		ENERGIA [GWH]	
	BARRA	ANO1991	ANO1991*
	CIRCUITO		
Arauco	3	1.623E+01	1.8E+01
Capital	2	1.443E+02	1.6E+02
Castro Barros	3	1.830E+00	2.0E+00
Chilecito	10	4.439E+01	4.9E+01
Famatina	10	2.341E+00	2.6E+00

en.Penalzoa 5 9.300E-01 1.0E+00
.Belgrano 5 2.450E+00 2.7E+00
.F.Quiroga 5 6.700E-01 7.4E-01
.Lamadrid 9 4.880E-01 5.4E-01
.Lavalle 9 3.400E+00 3.7E+00
.Ocampo 5 1.925E+00 2.1E+00
.S.Martin 6 1.010E+00 1.1E+00
.Sarmiento 9 8.380E-01 9.2E-01
.Gob.Gordillo 5 5.975E+00 6.6E+00
.Independencia 4 6.010E-01 6.6E-01
.R.V.Penalzoa 6 3.751E+00 4.1E+00
.Sanagasta 2 7.170E-01 7.9E-01
.S.B.de los Sauces 3 1.177E+00 1.3E+00
Total La Rioja 2.331E+02 2.6E+02
* [INCLUYE PERDIDAS] FUENTE :EPELAR 1993

DATOS ACTIVOS

VALORES DE CRECIMIENTO EN NODOS [TAS. AN.AC.= 5%]

	1991	1993	1995	2000	2005	2010	2013
GNH							
LOCALIDAD BARRA	ENERGIA						
RECRO 1	0.000E+00						
LA RIOJA 2	1.596E+02	1.759E+02	1.9E+02	2.48E+02	3.159E+02	4.03E+02	5.15E+02
AINOGASTA 3	2.116E+01	2.333E+01	2.6E+01	3.28E+01	4.190E+01	5.35E+01	6.82E+01
PATQUIA 4	6.611E-01	7.289E-01	8.0E-01	1.03E+00	1.309E+00	1.67E+00	2.13E+00
CHAMICAL 5	1.315E+01	1.449E+01	1.6E+01	2.04E+01	2.603E+01	3.32E+01	4.24E+01
CHEPES 6	5.237E+00	5.774E+00	6.4E+00	8.12E+00	1.037E+01	1.32E+01	1.69E+01
LUJAN 7	0.000E+00	0.000E+00	0.0E+00	0.00E+00	0.000E+00	0.00E+00	0.00E+00
NONOGASTA 8	1.000E+01	1.103E+01	1.2E+01	1.55E+01	1.980E+01	2.53E+01	3.23E+01
V.UNION 9	5.199E+00	5.731E+00	6.3E+00	8.06E+00	1.029E+01	1.31E+01	1.68E+01
CHILECITO 10	4.140E+01	4.565E+01	5.0E+01	6.42E+01	8.198E+01	1.05E+02	1.34E+02
TOTAL	2.564E+02	2.826E+02	3.1E+02	3.98E+02	5.076E+02	6.48E+02	8.27E+02

R[OHM]= RO[OHM*mm^2/m] Ro[Al]=1/37= 2.70E-02
d12[m]= 5.200E+00 Ro[Cu]=1/52= 1.92E-02
d13[m]= 3.310E+00 Seccion [mm^2]= 1.50E+02
d23[m]= 6.160E+00 React.induc.[ohm/k4.23E-01
Cap.a t.[mf/km]= 1.04E-03
VALORES ELECTRICOS Suc.[2*pi*50*147] 3.28E-01 umho/km/f
ojo revisar suceptancia L[mHy/km]Xl[ohm/km]
1.35E-03 4.231E-01

DE	A	DIST[KM]	R [OHM]	XL [J O]	Sucep [umho/km/f]	XC [-j OHM/R (1/1)]	Xl (1/1)	Xc (1/1)
1	2	185.00	16.67	39.14	9.6E+02	1.93E-01	0.10	0.22
2	3	130.00	23.42	55.00	7.4E+00	1.36E-01	0.13	0.32
2	4	69.00	12.43	29.19	1.4E+01	7.20E-02	0.07	0.17
4	5	68.00	12.25	28.77	1.4E+01	7.10E-02	0.07	0.17
5	6	158.00	28.47	66.85	6.1E+00	1.65E-01	0.16	0.38
5	8	114	20.54	48.23	8.4E+00	1.19E-01	0.12	0.28
6	7	151.00	27.21	63.89	6.3E+00	1.58E-01	0.16	0.37
8	9	92.00	16.58	38.93	1.0E+01	9.60E-02	0.10	0.22
8	10	13.00	2.34	5.50	7.4E+01	1.36E-02	0.01	0.03

LA LINEA ENTRE RECRO Y LA RIOJA ES DOBLE TERNA

TENSION BASE: 132 [KV]; POTENCIA BASE: 100 [MVA]

IMPEDANCIA BASE=((TENSION BASE[kv])^2)/POTENCIA BASE [MVA]

ZR[OHM]= 1.742E+02

AÑO 1991

VALORES VOLCADOS A BASE ELEGIDA [MVA] 1.0E+02

LOCALIDAD	BARRA	ACAR	REACAR	CAREST	ACTGEN	REMAX	REMIN	T
RECREO	1	0.000E+00	0.000E+00		1.40E+02			
LA RIOJA	2	1.596E+02	4.787E+01		1.15E+02			
AIMOGASTA	3	2.116E+01	6.348E+00			0.000E+00	1.800E+00	*
PATQUIA	4	6.611E-01	1.983E-01					
CHAMICAL	5	1.315E+01	3.944E+00		3.40E-01			
CHEPES	6	5.237E+00	1.571E+00					
LUJAN	7	0.000E+00	0.000E+00					
NONOGASTA	8	1.000E+01	3.000E+00					
V.UNION	9	5.199E+00	1.560E+00		5.35E+00			
CHILECITO	10	4.140E+01	1.242E+01		2.95E+00	8.850E-01	8.000E-01	

LOCALIDAD	BARRA	ENERGIA GWH	FAC.UTIL. [HORAS]	C.MAX MW
RECREO	1	0.000E+00		
LA RIOJA	2	1.596E+02	3000	53.19
AIMOGASTA	3	2.116E+01	4200	5.04
PATQUIA	4	6.611E-01	3200	0.21
CHAMICAL	5	1.315E+01	3200	4.11
CHEPES	6	5.237E+00	3200	1.64
LUJAN	7	0.000E+00		
NONOGASTA	8	1.000E+01	3200	3.13
V.UNION	9	5.199E+00	3400	1.53
CHILECITO	10	4.140E+01	3600	11.50
TOTAL		2.564E+02		

VALORES DE CRECIMIENTO EN NODOS [TAS. AN.AC.= 5%]

DATOS ACTIVOS

1993	1995	2000	2005	2010	2013
------	------	------	------	------	------

1.76E+02	1.939E+02	2.475E+02	3.159E+02	4.0E+02	5.15E+02
2.33E+01	2.572E+01	3.283E+01	4.190E+01	5.3E+01	6.82E+01
7.29E-01	8.036E-01	1.026E+00	1.309E+00	1.7E+00	2.13E+00
1.45E+01	1.598E+01	2.039E+01	2.603E+01	3.3E+01	4.24E+01
5.77E+00	6.366E+00	8.124E+00	1.037E+01	1.3E+01	1.69E+01
0.00E+00	0.000E+00	0.000E+00	0.000E+00	0.0E+00	0.00E+00
1.10E+01	1.216E+01	1.551E+01	1.980E+01	2.5E+01	3.23E+01
5.73E+00	6.319E+00	8.065E+00	1.029E+01	1.3E+01	1.68E+01
4.56E+01	5.033E+01	6.423E+01	8.198E+01	1.0E+02	1.34E+02
2.83E+02	3.116E+02	3.977E+02	5.076E+02	6.5E+02	8.27E+02

ASIGNACION DE FACTOR DE UTILIZACION A CADA NODO

BARRA	ENERGIA GWH	FAC.UTIL. [HORAS]	C.MAX MW
1	0.000E+00		
2	1.596E+02	3000	53.19
3	2.116E+01	4200	5.04
4	6.611E-01	3200	0.21
5	1.315E+01	3200	4.11
6	5.237E+00	3200	1.64
7	0.000E+00		0.00
8	1.000E+01	3200	3.13
9	5.199E+00	3400	1.53
10	4.140E+01	3600	11.50
	2.564E+02		

1991

BARRA	ACAR	REACAR	CAREST	ACTGEN	REMAX
1		0.00		139.57	
2	53.19	15.96		114.57	
3	5.04	1.51			0.00
4	0.21	0.06			
5	4.11	1.23		0.34	
6	1.64	0.49			
7	0.00	0.00			
8	3.13	0.94			
9	1.53	0.46		5.35	
10	11.50	3.45		2.95	0.89

TOTAL

VALOR DE LA SUCEPTANCIA EXPRESADA EN MVAR

Cap.a t.[mf/km]= 1.04E-03
 Suc.[2*pi*50*147] 3.28E-01 umho/km/f
 Suc[mvar]=U^2*2*pi*50*C[μF](f166)

DE	A	DIST[KM]	R [OHM]	XL [J O]	CAP μF	Suc MVar
1	2	185.00	16.67	39.14	1.9E-01	5.29E+05
2	3	130.00	23.42	55.00	1.4E-01	3.71E+05
2	4	69.00	12.43	29.19	7.2E-02	1.97E+05
4	5	68.00	12.25	28.77	7.1E-02	1.94E+05
5	6	158.00	28.47	66.85	1.6E-01	4.51E+05
5	8	114	20.54	48.23	1.2E-01	3.26E+05
6	7	151.00	27.21	63.89	1.6E-01	4.31E+05
8	9	92.00	16.58	38.93	9.6E-02	2.63E+05
8	10	13.00	2.34	5.50	1.4E-02	3.71E+04

LOS DATOS DE RAMA DEBEN PRESENTARSE EN TANTO POR UNO COMO
RESISTENCIA INDUCTANCIA Y CAPACIDAD

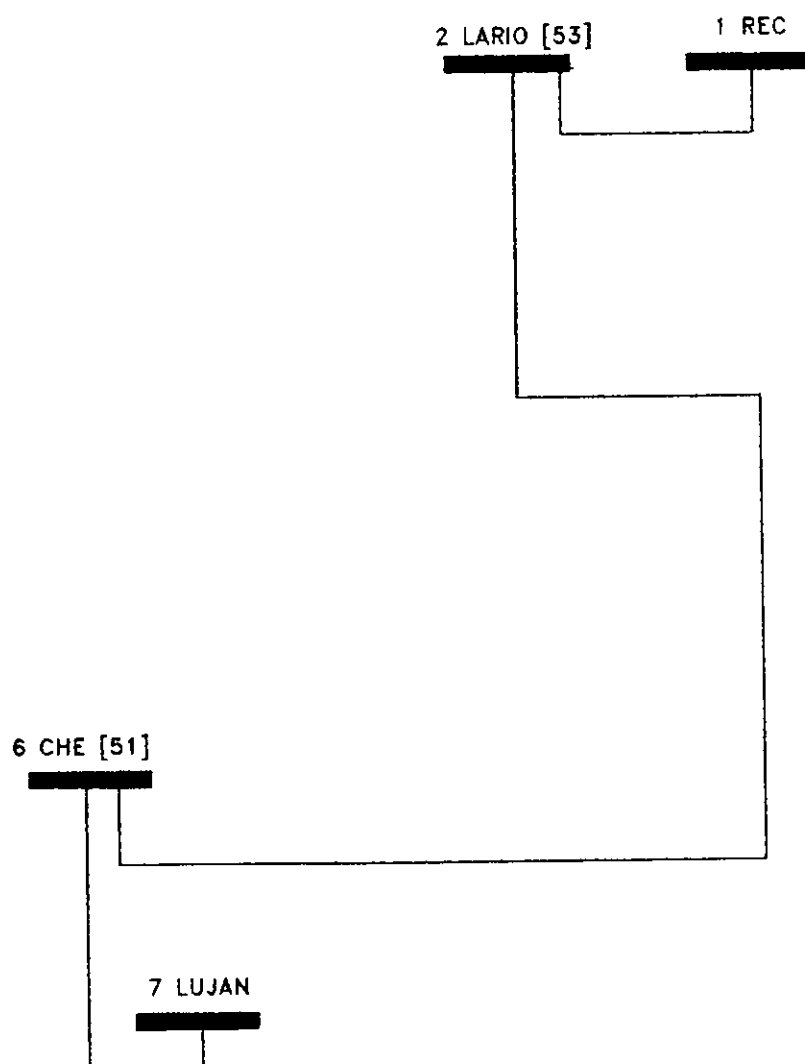
VALOR DE LA SUCEPTANCIA EXPRESADA EN MVAR

Cap.a t.(mf/km)= 1.04E-03

Suc.[2*pi*50*f47] 3.28E-01 umho/km/f

DE	A	DIST(KM)	R [OHM] 1/1	XL [J O] X1 1/1	CAP QC*Km1/1
1	2	185.00	0.10	0.22	3.5E-01
2	3	130.00	0.13	0.32	2.4E-01
2	4	69.00	0.07	0.17	1.3E-01
4	5	68.00	0.07	0.17	1.3E-01
5	6	158.00	0.16	0.38	3.0E-01
5	8	114	0.12	0.28	2.1E-01
6	7	151.00	0.16	0.37	2.8E-01
8	9	92.00	0.10	0.22	1.7E-01
8	10	13.00	0.01	0.03	2.4E-02

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 250
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

```

descriptive interpretation of input data cards.      ! Input data card images are shown below, all 80 columns, character by character
0           1           2           3           4           5           6           7           8
0123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890

```

```

Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Erase all of 0 cards in the punch buffer.
Marker card preceding new ENTP data case.
Width of time-step loop numbers. W=13 S=2
Declaration of desired ENTP load flow usage.
New power frequency STATFR = 5.00000000E+01 Hz.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Disc. data.  2.000E-04 0.000E+00 5.000E+01
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Disc. data.  1 1 0 1 0 1 0 0 0 0
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Series R-L-C.  1.000E-01 7.003E-04 0.000E+00
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Series R-L-C.  8.000E-02 1.210E-03 0.000E+00
Series R-L-C.  8.000E-02 1.178E-03 0.000E+00
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Blank card ending branches.  IRR, NTOT = 3 5
Blank card ending switches.  KSWTCH = 0.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.
Comment card.  KOMPAT = 1.

```

7-057

[illegible]

```

ax del-V: .0033 .0033 .0033 .0034 .0034 .0034 .0033 .0033 .0032 .0032 .0032 .0031 .0031 .0031 .003 .003 .003 .0029 .0029 .0029
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .0029 .0028 .0028 .0028 .0027 .0027 .0027 .0027 .0026 .0026 .0026 .0025 .0025 .0025 .0025 .0024 .0024 .0024 .0024 .0023
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .0023 .0023 .0023 .0023 .0022 .0022 .0022 .0022 .0022 .0021 .0021 .0021 .0021 .0021 .002 .002 .002 .002 .002 .0019
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .0019 .0019 .0019 .0019 .0019 .0018 .0018 .0018 .0018 .0018 .0018 .0017 .0017 .0017 .0017 .0017 .0017 .0016 .0016 .0016
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .0016 .0016 .0016 .0016 .0015 .0015 .0015 .0015 .0015 .0015 .0015 .0015 .0014 .0014 .0014 .0014 .0014 .0014 .0014 .0014
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .0013 .0013 .0013 .0013 .0013 .0013 .0013 .0013 .0013 .0012 .0012 .0012 .0012 .0012 .0012 .0012 .0012 .0012 .0012 .0012
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .0011 .0011 .0011 .0011 .0011 .0011 .0011 .0011 .0011 .0011 .0011 .001 .001 .001 .001 .001 .001 .001 1.E-3 1.E-3 1.E-3
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: 1.E-3 1.E-3 1.E-3 1.E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3 .9E-3
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3 .8E-3
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3 .7E-3
ource No. -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2 -2
ax del-V: .6E-3 .6E-3 .6E-3 .6E-3
ource No. -2 -2 -2 -2

```

Exit the load flow iteration loop with counter NEKITE = 264. If no warning on the preceding line, convergence was attained.

Row	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	4	CHEPE	8.51020729E-01	-7.28808	-5.09141849E-01	-3.13251897E-01
2	2	RECRE	1.02000000E+00	-13.01490	1.01529871E+00	-8.80866837E-02
4	3	LARIO	9.66585905E-01	-26.63249	-1.51801594E+00	8.50444661E-01

Sinusoidal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" is printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage		Phasor branch current		Power flow P and Q	Power loss P and Q
		Rectangular	Polar	Rectangular	Polar		
RECRE		1.4055836948592	1.4424978336206	1.399124311889	1.4129833635385	1.015298711256	.09982609928187
		-.3242444706482	-12.9899339	-.1974161733945	-8.0314041	-.0880866837274	0.2196174
LARIO		1.2222397055235	1.3670382881027	-1.399124311889	1.4129833635385	-.9154726119742	
		-.6123102019243	-26.6096744	.1974161733946	171.7685959	.30770410214737	
LARIO		1.2222397055235	1.3670382881027	-1.143816027338	1.1864209370084	-.6025433270133	.05630378559088
		-.6123102019243	-26.6096744	-.3150865521984	-164.5987370	.54274075871858	0.2674430
CHEPE		1.1940120978752	1.2037054723679	1.1438160273382	1.1864209370084	.6588471126042	
		-.1524531873599	-7.2762378	.31508655219844	15.4012630	-.2752977771619	
CHEPE		1.1940120978752	1.2037054723679	-1.916914449274	1.941712704843	-1.167988961525	.15080372912595
		-.1524531873599	-7.2762378	.3093335130755	170.8331736	-.0385541196011	0.6974959
LUJAN		1.4618186536551	1.5556349186104	1.9169144492744	1.941712704843	1.3187988906514	
		.53205847782555	20.0000000	-.3093335130755	-9.1668264	.73605004120861	
Total network loss P-loss by summing injections =				3.069398139987E-01			

Path: C:\ATP

File: PROBE10.SAL 21.567 a.. 29-03-94 16:19:20

Page 4

Solution at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed result applying to the composite group. The entry "MVA" is $\sqrt{P^2 + Q^2}$ in units of power, while "P.F." is the associated power factor.

Node name	Source node voltage		Injected source current		Injected source power	
	Rectangular	Polar	Rectangular	Polar	P and Q	MVA and P.F.
RECRE	1.4055836948592 -.3242444706482	1.4424978336206 -12.9899339	1.399124311889 -.1974161733945	1.4129833635385 -8.0314041	1.015298711256 -.0880866837274	1.0191127204231 0.9962575
LARIO	1.2222397055235 -.6123102019243	1.3670382881027 -25.6096744	-2.542940333227 -.117670378804	2.5456613849679 -177.3506220	-1.518015938987 .85044466086595	1.7400082908977 -0.8724188
CHEPE	1.1940120978752 -.1524531873599	1.2037054723679 -7.2762378	-.7730984219362 .62442006527398	.99377139620592 141.0727068	-.5091418487213 -.313851896763	.55810403394739 -0.8512597
LUJAN	1.4618186536551 .53205847782555	1.5556349186104 20.0000000	1.9169144492744 -.3093335130755	1.941712704643 -2.1668264	1.3187988906514 .73605004180861	1.5102780427816 0.8732044

Comment card. KOMPAN = 1.

IC

Comment card. KOMPAN = 1.

IC

Comment card. KOMPAN = 1.

IC

Request for flushing of punch buffer.

!\$PUNCH

(Flush punched cards: R-L branches for equivalent impedance loads

A listing of 80-column card images now being flushed from punch buffer follows.

```

=====
123456789012345678901234567890123456789012345678901234567890123456789
=====

```

```

=====
< End of LUNIT7 punched cards as flushed by $PUNCH request >=====

```

Blank card ending node names for voltage output. !BLANK card ending requests for output variables

Selective branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be augmented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

From	To	Branch voltage $V_{km} = V_k - V_m$				Branch current I_{km} from K to M			
bus K	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
RECRE	LARIO	3.4146286E-01	57.524641	1.8334399E-01	2.8806573E-01	1.4129834E+00	-8.031404	1.3991243E+00	-1.9741617E-01
LARIO	CHEPE	4.6072255E-01	-86.487395	2.8227608E-02	-4.5985701E-01	1.1864209E+00	-164.598737	-1.1438160E+00	-3.1508655E-01
CHEPE	LUJAN	7.3503508E-01	-111.367295	-2.6780656E-01	-6.8451167E-01	1.9417127E+00	170.833174	-1.9169144E+00	3.0933351E-01

Actual List Sizes for the preceding solution follow. 29-Mar-94 16:19:20

Size 1-10: 5 3 3 2 -9999 0 -9999 -9999 0 0

Size 11-20: -9999 -9999 -9999 -9999 -9999 0 0 3 23 0

Size 21-29: 0 -9999 3 -9999 -9999 -9999 -9999 -9999 -9999

Seconds for overlays 1-5 : 18.133 0.000 18.133 --- (CP: 1/0; tot)

Seconds for overlays 6-11 : 5.824 0.000 5.824

Seconds for overlays 12-15 : 0.000 0.000 0.000

Seconds for time-step loop : 0.000 0.000 0.000

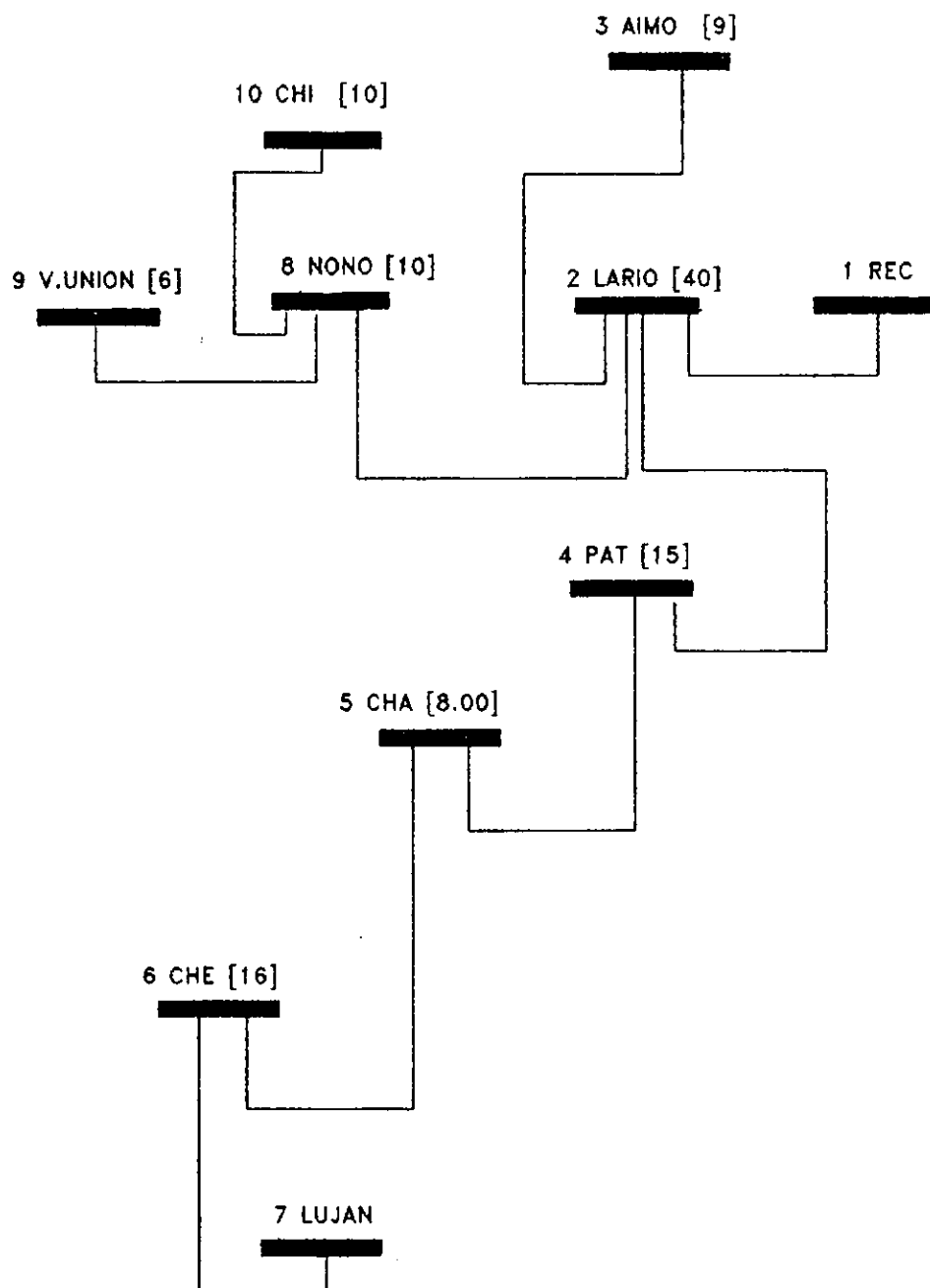
Seconds after DELTAT-loop : 0.328 0.000 0.328

```

-----
Totals : 24.285 0.000 24.285

```

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 260
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

DATA:C:\RIVVENIN\PROBE3.DAT(-06-04-94 10:05;RETOMO Y AGREGO DATOS DE ARCH
RED 132 KV LA RIOJA; DATOS DE RED FLU132E.WQ1 12-12-93)
(SE AGREGAN LOS DATOS DE RESTRICCIONES Y RAMAS COMPLETAS +XC)
CASO 110: LINEA CHAMICAL(5) CHEPES(6) Y CHEPES(6) LUJAN(7) EN 240 MM2
SE ELIMINA CONEXION PATQUIA NONOGASTA Y SE AGREGA LA RIOJA NONOGASTA
ERASE

EGIN NEW DATA CASE

PRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
IX SOURCE (An EMTP load flow will satisfy requested phasor power injections.
OWER FREQUENCY, 50.0,

MISCELANEA CARD SIGUE II B-1,II B-2

34567890123456789012345678901234567890123456789012345678901234567890

DELTAT THAX XOFT CGPT EPSILN TOLMAT

.000200 .000 50.50.(T-max = 0 means that no transient solution follows

IOUT IPLOT IOUUBL KSSOUT MAXOUT IPUN MEMSAY ICAT NERERG IPRSUP

1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72

1 1 1 0 1

CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.

BASE 100 MVA =1; UB=132 KV

SIGUE FORMATO RULE BOOK 4A-2

34567890123456789012345678901234567890123456789012345678901234567890

BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION

A6 A6 A6 A6 E6.2 E6.2 E6.2 11

3-8 9-14 15-20 21-26 27-32 33-38 39-44 80

LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)

EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG

RECRE LARIO 0.11 0.22 4

LARIO AINOG .16 .30 4

LARIO PATQU .08 .16 4

PATQU CHAMI .08 .16 4

PATQU NONOG .14 .26 4

CHAMI CHEPE .11 .35 4

CHEPE LUJAN .195 .34 4

NONOG VUNIO .11 .21 4

NONOG CHILE .01 .02 4

LARIO NONOG .08 .16 4

BLANK card ending branch cards.

BLANK card ending switch cards.

C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4

34567890123456789012345678901234567890123456789012345678901234567890

C NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP

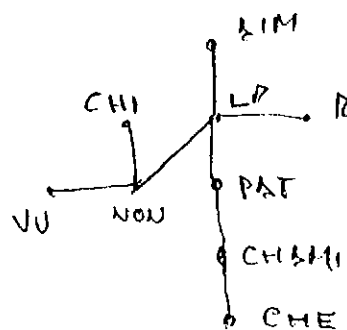
C I2 A6 I2 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6

C 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

14LUJAN 1.10 50. 15.0 -1.

14RECRE 1.10 50. 15.0 -1.

BLANK card terminating all EMTP source cards.



Next come power constraints of the load flow. There will be one for each non-slack generator. So, 3 of them will apply to nodes that have no Type-14 source as required by the algorithm. The program will define these internally. Yet, this is only possible for TMAX non-positive (no transient continuation). If data is modified to make TMAX > 0, a KILL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data. Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02

VALORES DE POTENCIA EN PU 1=100 MVA
 PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4;10-8
 3456789012345678901234567890123456789012345678901234567890
 NKBUS1 BUS2 BUS3 PK or QK QK or VK VMIN VMAX TMIN TMAX
 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
 LARIO -0.4000 -0.200 .65 1.25
 CHAMI -0.080 -.034 .65 1.25
 FATOU -0.150 -.080 .65 1.25
 NONOG -0.10 -.061 .65 1.25
 VUNIO -.0600 -.02 .65 1.25
 LUJAN 1.0 1.20 -20. 40.
 IRECRE 0.8 1.10 -20. 15.
 CHEPE -.16 -.09 1.5
 AIMOG -0.090 -0.04 .65 1.15
 CHILE -.1000 -.04 1.15

The following load-flow miscellaneous data card has two peculiarities. The use of VSCALE = 1.414 is the special flag requesting RMS rather than peak voltages. The use of KTAPER = 0 ensures constant acceleration factors (this works well for this problem whether RMS or peak values are used).

NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE KTAPER
 10-16 17-24 25-32 33-40 41-48 50-56 57-64
 1 2500 20 1 .01 0.2 2.5 1.414 2

MPUNCH (Flush punched cards: R-L branches for equivalent impedance loads
 BLANK card ending requests for output variables
 BLANK card ending plot cards
 BEGIN NEW DATA CASE

```

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
Date (dd-mth-yy) and time of day (hh.mm.ss) = 06-Apr-94 10.32.55 Name of disk plot file, if any, is C:\44061032.plt
For information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct. 1990
Total length of "LABCOM" tables = 444863 INTEGER words. "VARDIM" List Sizes follow : 752 900 1500 150 7500
120 2100 5250 225 480 150 150 15000 60 64800 120 12 15 4800 1980 300 450 12000 9 1200 252 4

```

```

descriptive interpretation of input data cards.      ; Input data card images are shown below, all 80 columns, character by character
0             1             2             3             4             5             6             7             8
0123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890

```

```

oment card.  KOMPAR = 1.          IC data:C:\RIV\EMIN\FROBE4.DAT
oment card.  KOMPAR = 1.          IC DATA:C:\RIV\EMIN\FROBE3.DAT{-06-04-94 10:05:RETONO Y AGREGO DATOS DE ARCH
oment card.  KOMPAR = 1.          IC RED 132 KV LA RIOJA; DATOS DE RED FLU132E.W01 12-12-93}
oment card.  KOMPAR = 1.          IC (SE AGREGAN LOS DATOS DE RESTRICCIONES Y RAMAS COMPLETAS +XC)
oment card.  KOMPAR = 1.          IC CASO 110; LINEA CHAMICAL(5) CHEPES(6) Y CHEPES(6) LUJAN(7) EN 240 MM2
oment card.  KOMPAR = 1.          IC SE ELIMINA CONEXION PATQUIA NONOGASTA Y SE AGREGA LA RIOJA NONOGASTA
rase all of 0 cards in the punch buffer.  IERASE

```

[illegible]

ou lose, fella. The EMTP logic has detected an error condition, and is now going to terminate program execution. The following message summarizes the circumstances leading to this situation. Where an otherwise-unidentified data card is referred to, or where the "last" card is mentioned, it is the most recently read card of the input data that is meant. The 80-column image of this card is generally the last one printed out prior to this termination message. But possibly this last-read card has not yet been displayed, so a copy follows:

```

$ERASE
      KILL code number      Overlay number      Nearby statement number
            22              1              2843
KILL = 22.  The last-read data card is not recognized as either a comment card or a special-request card that can precede
miscellaneous data cards.  Hence, it is taken to be the floating-point miscellaneous data card.  But the presence of an alphabetical
letter other than "E" on the card makes it illegal as a miscellaneous data card, too.  Try again.

```

[illegible]

Actual List Sizes for the preceding solution follow. 06-Apr-94 10.33.21

Size 1-10: -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999

Size 11-20: -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999

Size 21-29: -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999 -9999

```
total case timing (CP, I/O, tot), sec: 26.266 0.000 26.266
```

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
 Date (dd-mth-yy) and time of day (hh.mm.ss) = 06-Apr-94 10.33.22 Name of disk plot file, if any, is C:\44061033.plt
 For information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct. 1990
 Total length of "LARDOM" tables = 444863 INTEGER words. "VARDIM" List Sizes follow: 752 900 1500 150 7500
 120 2100 5250 225 480 150 150 15000 60 64800 120 12 15 4800 1980 300 450 12000 9 1200 252 4

descriptive interpretation of input data cards. | Input data card images are shown below, all 80 columns, character by character

01234567890123456789012345678901234567890123456789012345678901234567890

```
ker card preceding new EMTF data case.
th of time-step loop numbers. W=13 S=2
laration of desired EMTF load flow usage.
power frequency STATFR = 5.00000000E+01 Hz.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
sc. data. 2.000E-04 0.000E+00 5.000E+01
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
sc. data. 1 1 0 1 0 1 0 0 0 0
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ries R-L-C. 1.100E-01 7.003E-04 0.000E+00
ries R-L-C. 1.600E-01 9.549E-04 0.000E+00
ries R-L-C. 8.000E-02 5.073E-04 0.000E+00
ries R-L-C. 8.000E-02 5.073E-04 0.000E+00
ment card. KOMPAS = 1.
ries R-L-C. 1.100E-01 1.114E-03 0.000E+00
ries R-L-C. 1.050E-01 1.082E-03 0.000E+00
ries R-L-C. 1.100E-01 6.685E-04 0.000E+00
ries R-L-C. 1.000E-02 6.366E-05 0.000E+00
ries R-L-C. 8.000E-02 5.073E-04 0.000E+00
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ank card ending branches. IRR, NTOT = 9 11
ank card ending switches. KSWTCH = 0.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
source. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00
source. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ank card ends electric network sources.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.
ment card. KOMPAS = 1.

BEGIN NEW DATA CASE
PRINTED NUMBER WIDTH, 13, 2, ( Request maximum precision for 8 output columns
FIX SOURCE ( An EMTF load flow will satisfy requested phasor power injections.
POWER FREQUENCY, 50.0,
MISCELANEA CARD SIGUE II B-1,II B-2
34567890123456789012345678901234567890123456789012345678901234567890
DELTA T TMAX XOPT COPT EPSILN TOLMAT
.000200 .000 50.50.( T-max = 0 means that no transient solution follows
IOUT IPLOT IDOURL KSSOUT MAXOUT IPUN NEMSAV ICAT NERERG IPRSUP
1-B 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
1 1 1 0 1
C
C CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.
C BASE 100 MVA =1; UB=132 KV
C SIGUE FORMATO RULE BOOK 4A-2
34567890123456789012345678901234567890123456789012345678901234567890
BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
A6 A6 A6 A6 E6.2 E6.2 E6.2 11
3-8 9-14 15-20 21-26 27-32 33-38 39-44 80
LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)
EN BO 1=CORRIENTE RAMA;2=VOLT RAMA;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG
RECRE LARIO 0.11 0.22
LARIO AINOG .16 .30
LARIO PATOU .08 .16
PATOU CHANI .08 .16
PATOU NONOG .14 .26
CHANI CHEFE .11 .35
CHEFE LUJAN .105 .34
NONOG VUNIO .11 .21
NONOG CHILE .01 .02
LARIO NONOG .08 .16
C
C
BLANK card ending branch cards.
BLANK card ending switch cards.
C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
34567890123456789012345678901234567890123456789012345678901234567890
NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP
12 A6 12 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6
1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
C
14LUJAN 1.10 50. 15.0 -1.
14RECRE 1.10 50. 15.0 -1.
C
C
BLANK card terminating all EMTF source cards.
C Next come power constraints of the load flow. There will be one
C for each non-slack generator. So, 3 of them will apply to nodes
C that have no Type-14 source as required by the algorithm. The
C program will define these internally. Yet, this is only possible
```

```
ment card. KOMPAS = 1.          IC          for TMAX non-positive (no transient continuation). If data is
ment card. KOMPAS = 1.          IC          modified to make TMAX > 0, a KILL = 40 error termination will
ment card. KOMPAS = 1.          IC          will result. Yet, the transient simulation is possible as a
ment card. KOMPAS = 1.          IC          2nd simulation that replaces the power constraints at load nodes
ment card. KOMPAS = 1.          IC          by constant-impedance loads. Branch cards for these will be
ment card. KOMPAS = 1.          IC          punched by the present subcase, and the transient continuation
ment card. KOMPAS = 1.          IC          will be illustrated by the following (4th of 4) subcase.
ment card. KOMPAS = 1.          IC          The following 4 cards would be used if peak rather than RMS input data.
ment card. KOMPAS = 1.          IC          Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.828428 ) = 1.414212
ment card. KOMPAS = 1.          IC          (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02
ment card. KOMPAS = 1.          IC
ment card. KOMPAS = 1.          IC VALORES DE POTENCIA EN PU 1=100 MVA
ment card. KOMPAS = 1.          IC PARA RESTRICCIÓN DE POTENCIASIGUE RULE BOOK 10-4:10-6
ment card. KOMPAS = 1.          IC 34567890123456789012345678901234567890123456789012345678901234567890
ment card. KOMPAS = 1.          IC NKBUS1 BUS2 BUS3 PK or QK      QK or VK      VMIN      VMAX      THMIN THMAX
ment card. KOMPAS = 1.          IC 1-2 3-6 7-14 15-20 21-36      37-52      53-60      61-68 69-74 75-80
X. -4.000E-01 -2.000E-01 6.500E-01 1.250E+00 : LARIO          -0.4000          -0.200          .65      1.25
X. -8.000E-02 -3.400E-02 6.500E-01 1.250E+00 : CHANI          -0.080          -.034          .65      1.25
X. -1.500E-01 -8.000E-02 6.500E-01 1.250E+00 : PATQU          -0.150          -.080          .65      1.25
X. -1.000E-01 -6.100E-02 6.500E-01 1.250E+00 : NONOS          -0.10          -.061          .65      1.25
X. -6.000E-02 -2.000E-02 6.500E-01 1.250E+00 : VUNIO          -.0600          -.02          .65      1.25
ment card. KOMPAS = 1.          IC LUJAN          1.0          1.20          -20.      40.
X. 8.000E-01 1.100E+00 0.000E+00 1.000E+19 : IRECRE          0.8          1.10          -20.      15.
X. -1.600E-01 -9.000E-02 0.000E+00 1.500E+00 : CHEPE          -.16          -.09          1.5
X. -9.000E-02 -4.000E-02 6.500E-01 1.150E+00 : AIMOG          -0.070          -0.04          .65      1.15
X. -1.000E-01 -4.000E-02 0.000E+00 1.150E+00 : CHILE          -.1000          -.04          1.15
ment card. KOMPAS = 1.          IC          The following load-flow miscellaneous data card has two peculiarities. The
ment card. KOMPAS = 1.          IC          use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
ment card. KOMPAS = 1.          IC          voltages. The use of KTAPER = 0 ensures constant acceleration factors
ment card. KOMPAS = 1.          IC          (this works well for this problem whether RMS or peak values are used).
ment card. KOMPAS = 1.          IC          MINOUT NITERA NFLOUT NFRINT BALCHK CFITEV CFITEA VSCALE KTAPER
ment card. KOMPAS = 1.          IC          10-16 17-24 25-32 33-40 41-48 50-56 57-64
= LASTOV, NTOT, NEXT, IOFKOL, IOFKOR, NCURR = 9 11 19 0 0 0
ad flow iter. 1 2500 20 1 1.00E-02 : 1 2500 20 1 .01 0.2 2.5 1.414 2
ax del-V: .0232 .0227 .0223 .0219 .0213 .0209 .0204 .0149 .0152 .0149 .0137 .0136 .0134 .0133 .0131 .0129 .0127 .0125 .0124 .0126
ource No. 1 -4 -4 -4 -4 -4 -4 -9 -9 -9 -5 -5 -5 -5 -5 -5 -5 -5 -5 7 7
ax del-V: .0129 .013 .0131 .0112 .0111 .0109 .0106 .0105 .0109 .0105 .0108 .0115 .0116 .0105 .0115 .0117 .0113 .0102 .0113 .0107
ource No. 7 7 7 -5 -5 4 -5 9 4 4 9 -9 -4 -4 -4 -9 -4 -4 9 -9 -4
ax del-V: .0114 .0108 .0113 .0105 .0114 .0107 .0113 .0102 .0113 .0103 .011 .0117 .0117 .0124 .0102 .0111 .0118 .012 .0135 .0105
ource No. -4 4 -9 -4 -4 4 -9 -4 -4 9 -9 -4 4 -4 9 -9 -4 -9 -4 9
ax del-V: .0116 .0118 .0115 .0106 .0115 .0109 .0116 .0113 .0115 .011 .0116 .0112 .0115 .011 .0116 .0112 .0115 .011 .0116 .0111
ource No. -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4
ax del-V: .0115 .011 .0116 .011 .0116 .0107 .0116 .011 .0116 .0109 .0116 .0109 .0116 .0107 .0116 .0109 .0116 .0105 .0116 .0108
ource No. -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4
ax del-V: .0116 .0108 .0116 .0108 .0115 .0108 .0116 .0107 .0116 .0108 .0116 .0107 .0116 .0107 .0116 .0106 .0116 .0107 .0117 .0105
ource No. -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4
ax del-V: .0116 .0104 .0117 .0106 .0116 .0106 .0117 .0105 .0116 .0106 .0117 .0105 .0116 .0105 .0117 .0104 .0116 .0105 .0117 .0104
ource No. -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 4 -9 -4 -4 9
ax del-V: .0116 .0104 .0117 .0104 .0116 .0104 .0117 .0104 .0116 .0104 .0117 .0104 .0116 .0104 .0117 .0104 .0116 .0104 .0117 .0104
ource No. -9 -4 -4 9 -9 -4 -4 9 -9 -4 -4 9 -9 -4 9 -9 -4 9 -4 9
ax del-V: .0116 .0103 .0117 .0104 .0116 .0104 .0117 .0104 .0116 .0103 .0117 .0104 .0116 .0104 .0117 .0104 .0116 .0103 .0117 .0104
ource No. -9 4 -4 9 -9 -9 -4 9 -9 4 -4 9 -9 -9 -9 -4 9 -9 4 9
```

[illegible]

[illegible]

At the load flow iteration loop with counter NEKITE = 1209. If no warning on the preceding line, convergence was attained.

Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	LARIO	8.89848959E-01	-3.80873	-4.04020805E-01	-2.03048523E-01
4	CHAMI	9.05428079E-01	0.16103	-8.98270015E-02	-3.56048400E-02
5	PATOU	8.82701351E-01	-2.45285	-1.52497678E-01	-8.17911190E-02
6	NONOG	8.38623352E-01	-6.21261	-9.08492987E-02	-5.03486506E-02
7	VUNIO	8.24732158E-01	-7.03372	-6.01987321E-02	-2.43593172E-02
2	RECRE	1.10000000E+00	2.04657	7.92761431E-01	6.78039071E-01
8	CHEPE	9.70934254E-01	7.05285	-1.60428259E-01	-9.08059684E-02
9	AIMOG	8.57252277E-01	-5.40203	-9.32589514E-02	-4.23486528E-02
10	CHILE	8.36738430E-01	-6.33785	-1.09194030E-01	-5.54031841E-02

Harmonic steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage		Phasor branch current		Power flow P and Q	Power loss P and Q
		Rectangular	Polar	Rectangular	Polar		
RECRE		1.5546456346292	1.5556349186104	1.0496480231542	1.3411526246414	.79276143126432	.09892796794204
		.05547026886898	2.0434654	-.8348229693001	-38.4964972	.67803907148634	0.1978559
LARIO		1.2555232988362	1.2583049528123	-1.049648023154	1.3411526246414	-.6938334613223	
		-.0836217696019	-3.8104500	.83482296930006	141.5035028	-.4801831316023	
AIMOG		1.2555232988362	1.2583049528123	.14659910010062	.16898272912901	.09554336445337	.00228441391951
		-.0836217696019	-3.8104500	-.084046811918	-29.9261026	.04563192719174	0.0042833
PATOU		1.2068533992447	1.2122401846189	-.1465991001006	.16898272912901	-.0932589514339	
		-.1141540097252	-5.4034244	.08404681191799	150.1738974	-.0423485527802	
CHAMI		1.2555232988362	1.2583049528123	-.1298428897114	.17513153600272	-.0765966062631	.00122684219611
		-.0836217696019	-3.8104500	-.1175239502998	-137.8509909	.07920587499028	0.0024537
NONOG		1.2471068979652	1.2482515700127	.12984288971139	.17513153600272	.0778234484572	
		-.0534449912241	-2.4539194	.11752395029979	42.1490051	-.0767521905981	
VUNIO		1.2471068979652	1.2482515700127	-.3683458960794	.36911828709613	-.2303211268575	.00544953239475
		-.0534449912241	-2.4539194	.02386651860333	176.2527727	-.0050389283986	0.0108999
CHILE		1.280393212628	1.2803982203692	.36834589607941	.36911828709613	.2357710592523	
		.00358103066031	0.1602456	-.0238665186033	-3.7072273	.01593877318811	
CHEPE		1.280393212628	1.2803982203692	-.4963158669284	.50258338703058	-.3175980607765	.01389245335055
		.00358103066031	0.1602456	.07912408706717	170.9419692	-.0515436331864	0.0442033
LUJAN		1.3626813884637	1.3730704490764	.49631586692843	.50258338703058	.33149051412705	
		.16858793450787	7.0526702	-.0791240870672	-9.0580308	.09574689384728	
CHILE		1.3626813884637	1.3730704490764	-.7444658766525	.76631843595364	-.4919187729672	.03083030712733
		.16858793450787	7.0526702	.18169893720791	166.2041848	-.1865528622466	0.0955315
CHILE		1.5026279441629	1.5556349186104	.74446587665248	.76631843595364	.52274608009457	
		.40262794416288	15.0000000	-.1816989372079	-13.7158152	.28638433294465	

NONOG	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	.09734877138892 -.0541048352449	.11137362356051 -29.0644457	.06088095671741 .02566174603322	.68222462137E-3 0.0013024
VUNIO	1.1573965688744 -.1428037440376	1.166173111915 -7.0338096	-.0973487713889 .0541048352449	.11137362356051 150.9355543	-.060198732096 -.0243593172106	
NONOG	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	.17317298983299 -.113512317528	.20706021017633 -33.2442449	.10940839983566 .05583192343033	.21436955319E-3 0.0004287
CHILE	1.1754449098797 -.1306403375443	1.1827022659092 -6.3417867	-.173172989833 .11351231752795	.20706021017633 146.7557551	-.1091740301925 -.0554031841239	
LARIO	1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	.41359218837384 -.2685564852355	.49313394128363 -32.9767432	.27086569862674 .15127680679971	.03972724336184 0.0194543
NONOG	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	-.4135921883738 .2685564852355	.49313394128363 147.0032568	-.2611386552545 -.131842320067	
Total network loss F-loss by summing injections = 1.632357556667E-01						

solution at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed result applying to the composite group. The entry "MVA" is $\sqrt{P^2 + Q^2}$ in units of power, while "P.F." is the associated power factor.

Node name	Source Rectangular	node voltage Polar	Injected Rectangular	source current Polar	Injected source power F and Q	MVA and P.F.
RECRE	1.5546456346292 .05547026886898	1.5556349186104 2.0434654	1.0496480231542 -.8348229693001	1.3411526546414 -58.4564972	.75276143126438 .67603907148634	1.0431719270371 0.7539528
LARIO	1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	-.6192966243911 .36469572184574	.71870369019886 149.5068440	-.4040208045053 -.2030485226273	.45217420649034 -0.9975079
AIMOG	1.2068533992447 -.1141540097252	1.2122401846189 -5.4034244	-.1465991001006 .08404681191799	.16898272912901 150.1738974	-.0932589514339 -.0423486527802	.10242582737838 -0.9105201
PATQU	1.2471068979652 -.0534447712241	1.2482515700127 -2.4539194	-.238503906368 .14139046890312	.27726332022687 149.3334914	-.1524976783983 -.0817911139967	.17304718739007 -0.8812491
CHAMI	1.280393212628 .00358103066031	1.2803982203692 0.1602456	-.127569970849 .05525756846384	.13939050294634 156.6452622	-.0918270015242 -.0356048379983	.08923767595443 -0.9167558
CHEPE	1.3626813884637 .16858793450787	1.3730704490764 7.0526702	-.2481500097241 .10257485014074	.26851448230485 157.5418424	-.1604282588402 -.0908059683994	.18434465040093 -0.8702626
LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.74446587665248 -.1816989372079	.76631843595364 -13.7158152	.52274508009457 .28638433294485	.5960558588722 0.8770136
NONOG	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	-.1430704271519 .10093963246268	.17509413618719 144.7561099	-.0908492987118 -.0503486506035	.10386209757585 -0.8746603
VUNIO	1.1573965688744 -.1428037440376	1.166173111915 -7.0338096	-.0973487713889 .0541048352449	.11137362356051 150.9355543	-.060198732096 -.0243593172106	.0649404625884 -0.9269874

CHILE 1.1754649098797 1.1827022669092 -.173172989833 .20706021017632 .1091940301825 .12244528999112
 -.1306403375443 -.6.3417867 .11351231752795 146.7557551 -.0554031841239 -.0.8517781

oment card. KOMPAT = 1.

oment card. KOMPAT = 1.

oment card. KOMPAT = 1.

request for flushing of punch buffer.

IFPUNCH

(Flush punched cards: R-L branches for equivalent impedance loads

listing of 80-column card images now being flushed from punch buffer follows.

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selective branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be augmented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

From	To	Branch voltage Vkm = V _k - V _m				Branch current Ikm (from K to M)			
bus K	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
ECRE	LARIO	3.2987993E-01	24.938452	2.7912234E-01	1.3909204E-01	1.3411526E+00	-38.496497	1.0496480E+00	-8.3492257E-01
ARIO	AIMOG	5.7454128E-02	32.101411	4.8669900E-02	3.0532240E-02	1.6898273E-01	-29.826103	1.4689910E-01	-8.4046812E-02
ARIO	PATOU	3.1328482E-02	-74.416042	8.4164009E-03	-3.0176778E-02	1.7513154E-01	-137.850991	-1.2984287E-01	-1.1752395E-01
ATOU	CHANI	6.6029887E-02	-120.272278	-3.3286315E-02	-5.7026022E-02	3.6911829E-01	176.292773	-3.6834590E-01	2.3366519E-02
CHANI	CHEPE	1.8438715E-01	-116.505219	-8.2288176E-02	-1.6500690E-01	5.0258339E-01	170.941967	-4.9631587E-01	7.9124087E-02
CHEPE	LUJAN	2.7268787E-01	-120.877734	-1.3994656E-01	-2.3404001E-01	7.6631844E-01	166.284185	-7.4446588E-01	1.8169864E-01
ONOG	VUNIO	2.6402832E-02	33.289579	2.2070317E-02	1.4491743E-02	1.1137362E-01	-29.864446	9.7348771E-02	-5.4104535E-02
ONOG	CHILE	4.6300071E-03	30.190704	4.0019782E-03	2.3283366E-03	2.0706021E-01	-33.244245	1.7317299E-01	-1.1351232E-01
ARIO	NONOG	8.8214481E-02	30.438206	7.6056413E-02	4.4690231E-02	4.9313394E-01	-32.996743	4.1359219E-01	-2.6855649E-01

Actual List Sizes for the preceding solution follow. 06-Apr-94 10:33:36

Size 1-10: 11 9 9 2 -9999 0 -9999 -9999 0 0
 Size 11-20: -9999 -9999 -9999 -9999 -9999 0 0 9 23 0
 Size 21-29: 0 -9999 9 -9999 -9999 -9999 -9999 -9999 -9999

seconds for overlays 1-5 : 3.133 0.000 3.133 --- (CP: I/O; tot)

seconds for overlays 6-11 : 11.043 0.000 11.043

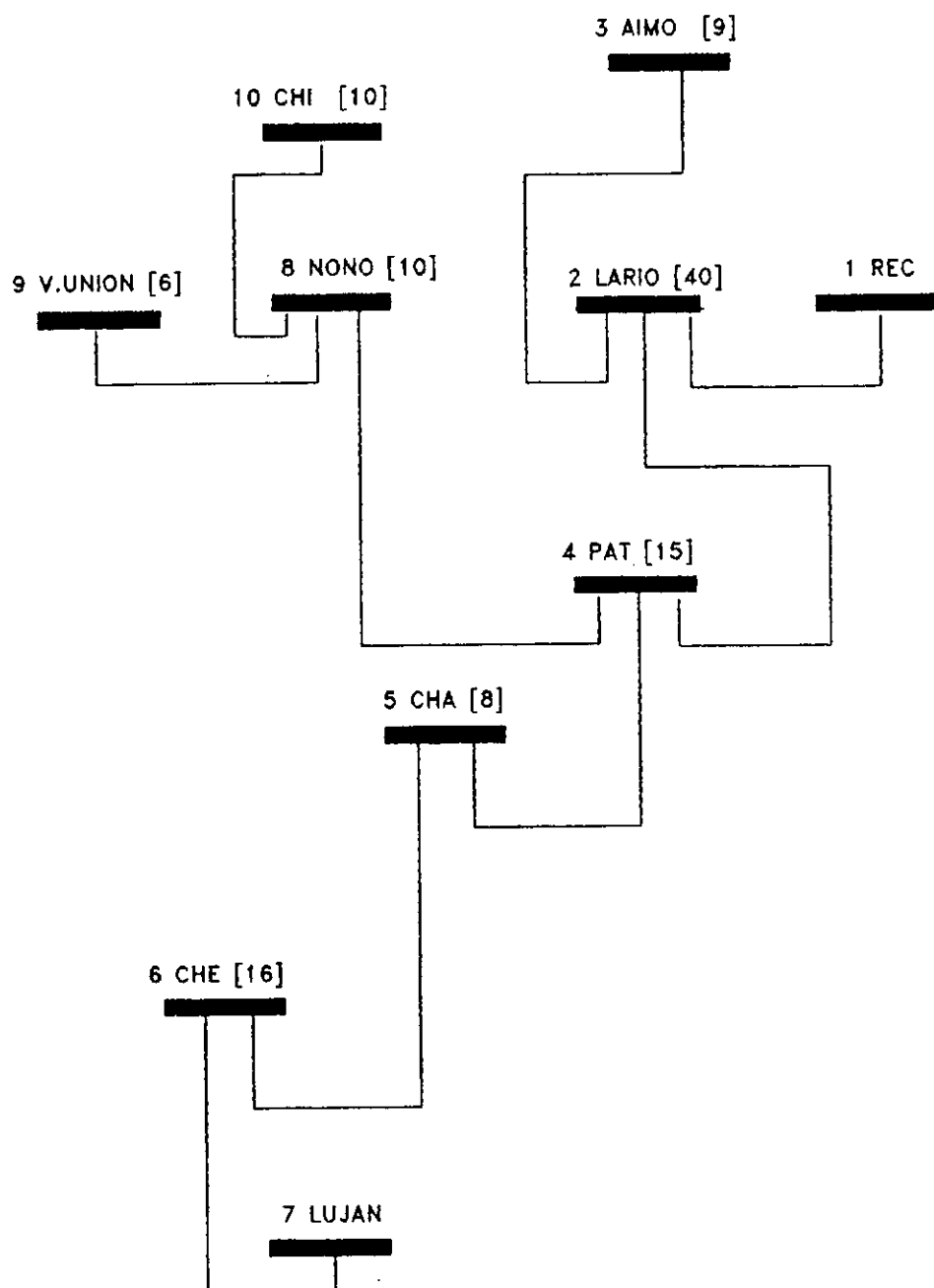
seconds for overlays 12-15 : 0.000 0.000 0.000

seconds for time-step loop : 0.000 0.000 0.000

seconds after DELTAT-loop : 0.109 0.000 0.109

Totals : 14.285 0.000 14.285

CIRCUITO PARA FLUJO
DE CARGAS 132 kV – LA RIOJA
CASO 270
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

DATA: C:\RIVEMIN\PROBE3.DAT (06-04-94 10:05; RETOMO Y AGREGO DATOS DE ARCH
RED 132 KV LA RIOJA; DATOS DE RED FLU132E.NOI 12-12-93)
-CASO-105; LINEA CHAMI[5], CHEP[6] Y CHEP[60, LUJ[7] EN 240 MM2
ERASE

EGIN NEW DATA CASE

PRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
X SOURCE (An EMTP load flow will satisfy requested phasor power injections.
POWER FREQUENCY, 50.0,

MISCELANEA CARD SIGUE II B-1, II B-2

34567890123456789012345678901234567890123456789012345678901234567890
DELTAT TMAX XOPT COPT EPSILN TOLMAT
000200 .000 50.50 (T-max = 0 means that no transient solution follows
IOUT IPLOT IDOUBL KSSOUT MAXOUT IPUN MEMSAV ICAT MERERG IPRSUP
1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
1 1 1 0 1

CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.

BASE 100 MVA =1; UB=132 KV

SIGUE FORMATO RULE BOOK 4A-2

34567890123456789012345678901234567890123456789012345678901234567890
BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
A6 A6 A6 A6 E6.2 E6.2 E6.2 11
3-8 9-14 15-20 21-26 27-32 33-38 39-44 80

LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)

EN 80 1=CORRIENTE RAMA; 2=VOLT RAMA; 3=I y V DE RAMA; 4=CONSUMO POT Y ENERG

RECRE LARIO	0.11	0.22	4
LARIO AINDG	.16	.30	4
LARIO PATQU	.08	.16	4
PATQU CHAMI	.08	.16	4
PATQU NONOG	.14	.26	4
CHAMI CHEFE	.11	.35	4
CHEPE LUJAN	.105	.34	4
NONOG VUNIO	.11	.21	4
NONOG CHILE	.01	.02	4
LARIO NONOG	.08	.16	4

BLANK card ending branch cards.

BLANK card ending switch cards.

SOURCE CARD SIGUE FORMATO RULE BOOK VII-4

34567890123456789012345678901234567890123456789012345678901234567890
NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP
I2 A6 I2 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6
1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

4LUJAN	1.10	50.	15.0	-1.
4RECRE	1.10	50.	15.0	-1.

BLANK card terminating all EMTP source cards.

Next come power constraints of the load flow. There will be one
for each non-slack generator. So, 3 of them will apply to nodes

that have no Type-14 source as required by the algorithm. The program will define these internally. Yet, this is only possible for TMAX non-positive (no transient continuation). If data is modified to make TMAX > 0, a KILL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data.

Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02

VALORES DE POTENCIA EN PU I=100 MVA

PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4;10-6

34567890123456789012345678901234567890123456789012345678901234567890

NRBUS1 BUS2 BUS3 PK or QK QK or VK VMIN VMAX THMIN THMAX

1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80

LARIO				-0.4000	-0.200	.65	1.25		
CHANI				-0.080	-0.034	.65	1.25		
PATGU				-0.150	-0.080	.65	1.25		
NONOG				-0.10	-0.061	.65	1.25		
VUNIO				-0.0600	-0.02	.65	1.25		
LUJAN			1.0		1.20			-20.	40.
IRECKE			0.8		1.10			-20.	15.
CHEPE			-.16		-.07		1.5		
AIMOG			-0.070		-0.04	.65	1.15		
CHILE			-.1000		-.04		1.15		

The following load-flow miscellaneous data card has two peculiarities. The use of VSCALE = 1.414 is the special flag requesting RMS rather than peak voltages. The use of KTAPER = 0 ensures constant acceleration factors (this works well for this problem whether RMS or peak values are used).

NNNQUT	NITERA	NFLOUT	NPRINT	RALCHK	CFITEV	CFITEA	VSCALE	KTAPER
10-16	17-24	25-32	33-40	41-48	50-56	57-64		
1	2500	20	1	.01	0.2	2.5	1.414	2

PUNCH (Flush punched cards: R-L branches for equivalent impedance loads

LANK card ending requests for output variables

LANK card ending plot cards

EGIN NEW DATA CASE

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
 Date (dd-mth-yy) and time of day (hh:mm:ss) = 06-Apr-94 11:00:16 Name of disk plot file, if any, is C:\44061100.plt
 For information, consult the copyrighted ATP EMTF Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
 Total length of "LABCON" tables = 444863 INTEGER words. "VARDIN" List Sizes follow: 752 900 1500 150 7500
 120 2100 5250 225 430 150 150 15000 60 64800 120 12 15 4800 1760 300 450 12000 9 1200 252 4

Descriptive interpretation of input data cards.

Input data card images are shown below, all 80 columns, character by character
 0 1 2 3 4 5 6 7 8
 01234567890123456789012345678901234567890123456789012345678901234567890

Comment card. KOMPAT = 1. IC DATA:C:\RIV\EMIN\PROGRES.DAT
 Comment card. KOMPAT = 1. IC DATA:C:\RIV\EMIN\PROGRES.DAT(-06-04-94 10:05:RETOÑO Y AGREGO DATOS DE ARCH
 Comment card. KOMPAT = 1. IC RED 132 KV LA RIOJA; DATOS DE RED FLU132E.W01 12-12-93}
 Comment card. KOMPAT = 1. IC CASO 105; LINEA CHANI(5), CHEP(6) Y CHEP(60, LUJ(7) EN 240 MM2
 Case all of 0 cards in the punch buffer. IERAGE
 Marker card preceding new EMTF data case. IBEGIN NEW DATA CASE
 Width of time-step loop numbers, W=13 S=2 IPRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
 Declaration of desired EMTF load flow usage. IFIX SOURCE (An EMTF load flow will satisfy requested phasor power injections.
 New power frequency STATFR = 5.00000000E+01 Hz. IPOWER FREQUENCY, 50.0,
 Comment card. KOMPAT = 1. IC MISCELANEA CARD SIGUE II R-1, II B-2
 Comment card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
 Comment card. KOMPAT = 1. IC DELTAT TMAX XOPT COPT EPSILN TOLNAT
 Disc. data. 2.000E-04 0.000E+00 5.000E+01 I.000200 .000 50.50.(T-max = 0 means that no transient solution follows
 Comment card. KOMPAT = 1. IC IOUT IPLOT IDOURL KSSOUT MAXOUT IPUN MENSAN ICAT NERERG IPRSUP
 Comment card. KOMPAT = 1. IC 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
 Disc. data. 1 1 0 1 0 1 0 0 0 0 I. 1 1 1 0 1
 Comment card. KOMPAT = 1. IC
 Comment card. KOMPAT = 1. IC CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRANOS (R-L) VALORES EN P.U.
 Comment card. KOMPAT = 1. IC BASE 100 MVA =1: UB=132 KV
 Comment card. KOMPAT = 1. IC SIGUE FORMATO RULE BOOK AA-2
 Comment card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
 Comment card. KOMPAT = 1. IC BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
 Comment card. KOMPAT = 1. IC A6 A6 A6 A6 E6.2 E6.2 E6.2 11
 Comment card. KOMPAT = 1. IC 3-8 9-14 15-20 21-26 27-32 33-38 39-44 80
 Comment card. KOMPAT = 1. IC LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)
 Comment card. KOMPAT = 1. IC EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG
 Series R-L-C. 1.100E-01 7.003E-04 0.000E+00 I. RECRE LARIO 0.11 0.22 4
 Series R-L-C. 1.600E-01 9.549E-04 0.000E+00 I. LARIO AIMOG .16 .30 4
 Series R-L-C. 8.000E-02 5.093E-04 0.000E+00 I. LARIO PATOU .08 .15 4
 Series R-L-C. 8.000E-02 5.093E-04 0.000E+00 I. PATOU CHANI .08 .16 4
 Series R-L-C. 1.400E-01 8.276E-04 0.000E+00 I. PATOU NONOG .14 .26 4
 Series R-L-C. 1.100E-01 1.114E-03 0.000E+00 I. CHANI CHEPE .11 .35 4
 Series R-L-C. 1.050E-01 1.082E-03 0.000E+00 I. CHEPE LUJAN .105 .34 4
 Series R-L-C. 1.100E-01 6.685E-04 0.000E+00 I. NONOG VUNIO .11 .21 4
 Series R-L-C. 1.000E-02 6.366E-05 0.000E+00 I. NONOG CHILE .01 .02 4
 Comment card. KOMPAT = 1. IC LARIO NONOG .08 .16 4
 Comment card. KOMPAT = 1. IC
 Comment card. KOMPAT = 1. IC
 Blank card ending branches. IRR, NTOI = 9 11 IBLANK card ending branch cards.
 Blank card ending switches. ISWTCH = 0. IBLANK card ending switch cards.
 Comment card. KOMPAT = 1. IC SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
 Comment card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890


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Comment card.  KOMPAR = 1.      IC NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP
Comment card.  KOMPAR = 1.      IC I2 A6 I2 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6
Comment card.  KOMPAR = 1.      IC 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
Comment card.  KOMPAR = 1.      IC
Source. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114LUJAN 1.10 50. 15.0 -1.
Source. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114RECRE 1.10 50. 15.0 -1.
Comment card.  KOMPAR = 1.      IC
Comment card.  KOMPAR = 1.      IC
Blank card ends electric network sources. BLANK card terminating all ENTP source cards.
Comment card.  KOMPAR = 1.      IC Next come power constraints of the load flow. There will be one
Comment card.  KOMPAR = 1.      IC for each non-slack generator. So, 3 of them will apply to nodes
Comment card.  KOMPAR = 1.      IC that have no Type-14 source as required by the algorithm. The
Comment card.  KOMPAR = 1.      IC program will define these internally. Yet, this is only possible
Comment card.  KOMPAR = 1.      IC for TMAX non-positive (no transient continuation). If data is
Comment card.  KOMPAR = 1.      IC modified to make TMAX > 0, a KILL = 40 error termination will
Comment card.  KOMPAR = 1.      IC will result. Yet, the transient simulation is possible as a
Comment card.  KOMPAR = 1.      IC 2nd simulation that replaces the power constraints at load nodes
Comment card.  KOMPAR = 1.      IC by constant-impedance loads. Branch cards for these will be
Comment card.  KOMPAR = 1.      IC punched by the present subcase, and the transient continuation
Comment card.  KOMPAR = 1.      IC will be illustrated by the following (4th of 4) subcase.
Comment card.  KOMPAR = 1.      IC The following 4 cards would be used if peak rather than RMS input data.
Comment card.  KOMPAR = 1.      IC Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.825428 ) = 1.414212
Comment card.  KOMPAR = 1.      IC (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02
Comment card.  KOMPAR = 1.      IC
Comment card.  KOMPAR = 1.      IC VALORES DE POTENCIA EN FU 1=100 MVA
Comment card.  KOMPAR = 1.      IC PARA RESTRICCIONE DE POTENCIASIQUE RULE BOOK 10-4;10-6
Comment card.  KOMPAR = 1.      IC 34567890123456789012345678901234567890123456789012345678901234567890
Comment card.  KOMPAR = 1.      IC NKBUS1 BUS2 BUS3 PK or QK QK or VK VMIN VMAX TMIN TMAX
Comment card.  KOMPAR = 1.      IC 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
IX. -4.000E-01 -2.000E-01 6.500E-01 1.250E+00 LARIO -0.4000 -0.200 .65 1.25
IX. -8.000E-02 -3.400E-02 6.500E-01 1.250E+00 CHAMI -0.080 -0.034 .65 1.25
IX. -1.500E-01 -8.000E-02 6.500E-01 1.250E+00 PATOU -0.150 -0.080 .65 1.25
IX. -1.000E-01 -6.100E-02 6.500E-01 1.250E+00 MONOG -0.10 -0.061 .65 1.25
IX. -6.000E-02 -2.000E-02 6.500E-01 1.250E+00 VUNIO -0.0600 -0.02 .65 1.25
Comment card.  KOMPAR = 1.      IC LUJAN 1.0 1.20 -20. 40.
IX. 8.000E-01 1.100E+00 0.000E+00 1.000E+19 IRECRE 0.8 1.10 -20. 15.
IX. -1.600E-01 -9.000E-02 0.000E+00 1.500E+00 CHEPE -.16 -.09 1.5
IX. -9.000E-02 -4.000E-02 6.500E-01 1.150E+00 AIMOG -0.090 -0.04 .65 1.15
IX. -1.000E-01 -4.000E-02 0.000E+00 1.150E+00 CHILE -.1000 -.04 1.15
Comment card.  KOMPAR = 1.      IC The following load-flow miscellaneous data card has two peculiarities. The
Comment card.  KOMPAR = 1.      IC use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
Comment card.  KOMPAR = 1.      IC voltages. The use of KTAPER = 0 ensures constant acceleration factors
Comment card.  KOMPAR = 1.      IC (this works well for this problem whether RMS or peak values are used).
Comment card.  KOMPAR = 1.      IC NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE KTAPER
Comment card.  KOMPAR = 1.      IC 10-16 17-24 25-32 33-40 41-48 50-56 57-64
<= LASTOV, NTOT, NEXT, IOFKOL, IOFKOR, NCURR = 9 11 19 0 0 0
Load flow iter. 1 2500 20 1 1.00E-02 1 2500 20 1 .01 0.2 2.5 1.414 2
Max del-V: .0232 .0227 .0223 .0218 .0213 .0209 .0204 .0187 .0152 .0155 .0158 .0147 .0136 .0135 .0133 .0131 .0129 .0127 .0125 .0126
Source No. 1 -4 -4 -4 -4 -4 -4 -4 -9 -9 -9 -9 -5 -5 -5 -5 -5 -5 -5 7
Max del-V: .0128 .013 .0132 .0115 .0113 .0111 .0108 .0106 .0114 .0091 .0061 .0107 .0115 .0116 .0118 .0117 .0118 .0117 .0118 .0117
Source No. 7 7 7 -5 -5 -5 -5 -4 -9 -4 -9 -5 -4 -9 -4 -9 -4 -9 -4 4
Max del-V: .0118 .0117 .0118 .0117 .0117 .0117 .0117 .0116 .0117 .0116 .0117 .0116 .0117 .0116 .0117 .0116 .0117 .0116 .0117 .0116

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[illegible]

Row	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	3	LARIO	8.91087643E-01	-1.34554	-4.00118202E-01	-2.00746833E-01
4	6	CHAMI	8.64222944E-01	0.12963	-7.94935718E-02	-3.51116205E-02
5	5	PATGU	8.31979085E-01	-2.51643	-1.49960473E-01	-8.20822973E-02
6	7	NONOS	7.32871828E-01	-7.08308	-9.05975424E-02	-5.23509333E-02
7	10	VUNIO	7.16999396E-01	-8.15415	-5.95701921E-02	-2.39812397E-02

2	2	RECRE	1.10000000E+00	4.63294	7.98768580E-01	6.69557164E-01
8	8	CHEPE	9.50362035E-01	7.15804	-1.59535586E-01	-9.05454973E-02
9	4	AINOG	8.59787951E-01	-2.87351	-8.98815151E-02	-4.08658418E-02
10	11	CHILE	7.30691633E-01	-7.24435	-1.06425229E-01	-5.36579748E-02

musoidal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage	Phasor branch current	Power flow	Power loss		
		Rectangular	Rectangular	P and Q	P and Q		
RECRE		1.5505536006569 .12563252560574	1.5556349186104 4.6322315	1.0931005410641 -1.3400000246314	1.3400000246314 -35.3387433	.79876857954054 .66955716430803	.05875800363067 0.1975160
	LARIO	1.2597974578778 -.0295920517973	1.2601449616631 -1.3456036	-1.093100541064 .77506856028199	1.3400000246314 144.6612567	-.7000103759039 -.4720411570467	
	LARIO	1.2597974578778 -.0295920517973	1.2601449616631 -1.3456036	.14429094845753 -.0745474671129	.16241057877591 -27.3229961	.09199169128486 .04482242216768	.00211017621278 0.0039566
	AINOG	1.2143466659907 -.0609517415965	1.21587538013 -2.8734375	-.1442909484575 .07454746711286	.16241057877591 152.6770039	-.0898815150721 -.0408658417707	
	LARIO	1.2597974578778 -.0295920517973	1.2601449616631 -1.3456036	.32143143161863 -.3670872778833	.48792543381625 -48.7737434	.20790068308829 .23647190196463	.0055226493928 0.0190457
	PATOU	1.1753489788861 -.0516540986253	1.1764834754783 -2.5164089	-.3214314316186 .3670872778835	.48792543381625 131.2062566	-.1983778336955 -.207426203179	
	PATOU	1.1753489788861 -.0516540986253	1.1764834754783 -2.5164089	-.3890795686029 .09784288546805	.40119339593382 165.8943687	-.2311791296593 -.0474509905562	.00643824563764 0.0128765
	CHAMI	1.2221302060493 .00277120151376	1.222133347919 0.1299190	.38907956860287 -.097842885468	.40119339593382 -14.1156313	.23761737549693 .0603274818335	
	PATOU	1.1753489788861 -.0516540986253	1.1764834754783 -2.5164089	.4619533240093 -.3143335146101	.55875435745091 -34.2331066	.27959649101614 .17279489643401	.02185445023793 0.0405868
	NONOG	1.0289487997262 -.1277552708223	1.0368495752427 -7.0776776	-.4619533240093 .3143335146101	.55875435745091 145.7668934	-.2577420407762 -.1322080602779	
	CHAMI	1.2221302060493 .00277120151376	1.222133347919 0.1299190	-.5192993741817 .19500732772467	.54194013661458 163.3799938	-.3171109473143 -.0954391102916	.01615345114206 0.0513973
	CHEPE	1.3335057019129 .16747517642763	1.3439811723955 7.1583066	.51929937418168 -.1550073277247	.54194013661458 -16.6200062	.3332643984564 .14683645483448	
	CHEPE	1.3335057019129 .16747517642763	1.3439811723955 7.1583066	-.7716468032872 .25911567030842	.8139899997068 161.4381708	-.4927999847231 -.2373819541668	.03478543526019 0.1126386
	LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.77164680328716 -.2591156703084	.8139899997068 -18.5618292	.52753542000329 .35002050650165	

NONOG	1.0289487997262 -.1277552708223	1.0368495752427 -7.0776776	.1096200358704 -.0634990186393	.12668337551698 -30.0821990	.060452869329 .02566635082125	.88267726978E-3 0.0016851
VUNIO	1.0035559018662 -.1437905863047	1.0138047051426 -8.1539065	-.1096200358704 .06349901863926	.12668337551698 149.9178010	-.0595701920592 -.0239812396698	
NONOG	1.0289487997262 -.1277552708223	1.0368495752427 -7.0776776	.19135183090538 -.1290907315903	.23082447914671 -34.0045874	.10669162905523 .05419077417296	.26639970087E-3 0.0005328
CHILE	1.0244534667853 -.1302914001245	1.0327055507524 -7.2480439	-.1913518309054 .12909073159026	.23082447914671 145.9954126	-.1064252293544 -.0536579747712	
Total network loss P-loss by summing injections = 1.907716885047E-01						

Solution at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed result applying to the composite group. The entry "MVA" is $\text{SQR}(P^2 + Q^2)$ in units of power, while "P.F." is the associated power factor.

Node name	Source Rectangular	node voltage Polar	Injected Rectangular	source current Polar	Injected P and Q	source power MVA and P.F.
RECRE	1.5505536006569 .12563252560574	1.5556349186104 4.6322315	1.0931005410641 -.7750689560282	1.3400000246314 -35.3387433	.75876237954054 .66955716430803	1.0422754146277 0.7663700
LARIO	1.2597974578778 -.0295520517973	1.2601449616631 -1.3456036	-.627378160988 .33343381528079	.71047974359396 152.0106144	-.4001182015367 -.2007468329124	.4476537346268 -0.8938118
AINOG	1.2143466659907 -.0609517415965	1.21587538013 -2.8734375	-.1442909484575 .07454746711286	.162410598977591 152.6770039	-.0898815150721 -.0408658417707	.09873552438349 -0.9103260
PATQU	1.1753489788861 -.0516540986253	1.1764834754783 -2.5164089	-.2485576762122 .15059664874629	.29062048967274 148.7890776	-.1499604725386 -.0820822973033	.17095510186769 -0.8771921
CHAMI	1.2221302060493 .00277120151376	1.222133347919 0.1299190	-.1302198055788 .05716444225662	.14221452536043 156.2992828	-.0794935718174 -.0351116284581	.08650255700073 -0.9147438
NONOG	1.0289487997262 -.1277552708223	1.0368495752427 -7.0776776	-.1609814572335 .12174376438057	.2018330343095 142.9012579	-.090597542394 -.0523509352837	.10463524754687 -0.8658415
CHEPE	1.3335057019129 .16747517642763	1.3439811723955 7.1583066	-.2523474291055 .10410834258375	.27297943507099 157.5809366	-.1595355862667 -.0905454993313	.18343951059329 -0.8696700
LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.77164680328716 -.2591156703084	.8139899997068 -18.5618292	.52758542000329 .35002050650165	.63313563347178 0.8332897
VUNIO	1.0035559018662 -.1437905863047	1.0138047051426 -8.1539065	-.1096200358704 .06349901863926	.12668337551698 149.9178010	-.0595701920592 -.0239812396698	.06421510108123 -0.9276520
CHILE	1.0244534667853 -.1302914001245	1.0327055507524 -7.2480439	-.1913518309054 .12909073159026	.23082447914671 145.9954126	-.1064252293544 -.0536579747712	.11918686043217 -0.8929275

Comment card. KOMPAS = 1. IC
 Comment card. KOMPAS = 1. IC
 Comment card. KOMPAS = 1. IC

request for flushing of punch buffer. ;\$PUNCH (Flush punched cards: R-L branches for equivalent impedance loads

listing of 80-column card images now being flushed from punch buffer follows.

=====

23456789012345678901234567890123456789012345678901234567890123456789

=====

=====< End of LUNIT7 punched cards as flushed by ;\$PUNCH request >=====

Blank card ending node names for voltage output. (BLANK card ending requests for output variables

selective branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be augmented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

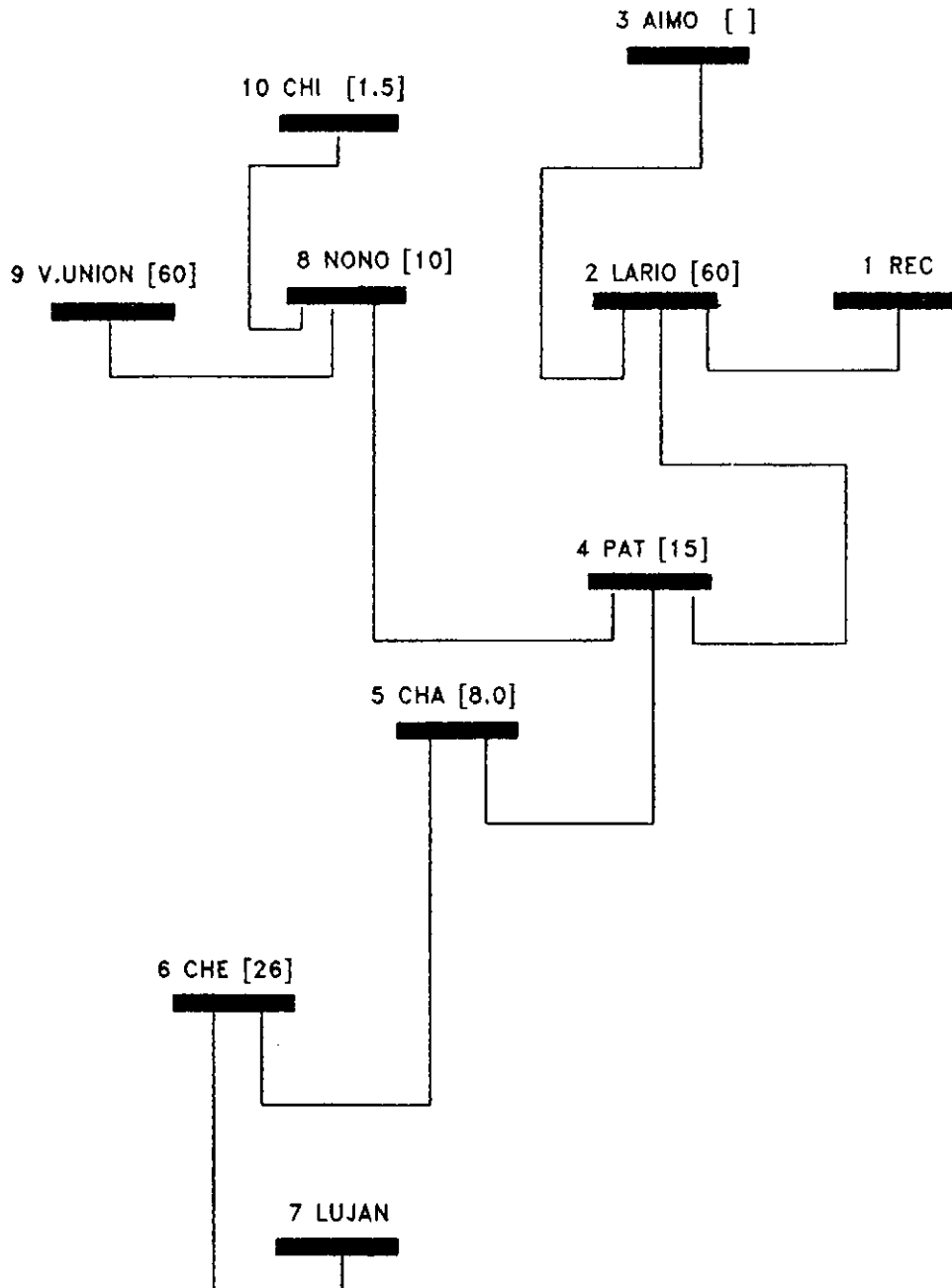
From	To	Branch voltage Vkm = V _k - V _m				Branch current Ikm from k to m			
bus K	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
ECRE	LARIO	3.2959643E-01	28.096206	2.9075614E-01	1.5522458E-01	1.3400000E+00	-35.338743	1.0931005E+00	-7.7506856E-01
LARIO	AIMOG	5.5219604E-02	34.604517	4.5450792E-02	3.1359690E-02	1.6241060E-01	-27.322996	1.4429095E-01	-7.4547467E-02
LARIO	PATQU	8.7282756E-02	14.641205	8.4448479E-02	2.2062047E-02	4.8792544E-01	-48.793743	3.2143143E-01	-3.6709728E-01
PATQU	CHAMI	7.1767656E-02	-130.680683	-4.6781227E-02	-5.4425300E-02	4.0119340E-01	165.884367	-3.3907957E-01	9.7842885E-02
PATQU	NONOG	1.6499818E-01	27.466138	1.4640018E-01	7.6101172E-02	5.5875436E-01	-34.233107	4.6195332E-01	-3.1433351E-01
CHAMI	CHEPE	1.9882631E-01	-124.067195	-1.1137550E-01	-1.6470397E-01	5.4194014E-01	163.379974	-5.1929937E-01	1.5500733E-01
CHEPE	LUJAN	2.8965351E-01	-125.723748	-1.6912224E-01	-2.3515277E-01	8.1399000E-01	161.438171	-7.7164680E-01	2.3911567E-01
NONOG	VUNIO	3.0032244E-02	32.271826	2.5392998E-02	1.6035315E-02	1.2668338E-01	-30.082197	1.0962004E-01	-6.3499019E-02
NONOG	CHILE	5.1613923E-03	29.430361	4.4933329E-03	2.5361293E-03	2.3082448E-01	-34.004587	1.9135183E-01	-1.2909073E-01

Actual List Sizes for the preceding solution follow. 06-Apr-94 11.00.56

Size 1-10:	11	9	9	2	-9999	0	-9999	-9999	0	0
Size 11-20:	-9999	-9999	-9999	-9999	-9999	0	0	9	23	0
Size 21-29:	0	-9999	9	-9999	-9999	-9999	-9999	-9999	-9999	-9999
seconds for overlays 1-5 :	30.168	0.000	30.168	--- (CP: I/O; tot)						
seconds for overlays 6-11 :	10.164	0.000	10.164							
seconds for overlays 12-15 :	0.000	0.000	0.000							
seconds for time-step loop :	0.000	0.000	0.000							
seconds after DELTAT-loop :	0.383	0.000	0.383							

Totals : 40.715 0.000 40.715

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 280
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

DATA:C:\RIVNEMIN\PROBE2.DAT(-05-04-94 15:55;RETOMO Y AGREGO DATOS DE ARCH
RED 132 KV LA RIOJA; DATOS DE RED FLU132E.W01 12-12-93)
(SE AGREGAN LOS DATOS DE RESTRICCIONES Y RAMAS COMPLETAS +XC)
ERASE

EGIN NEW DATA CASE

PRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
IX SOURCE (An EMTP load flow will satisfy requested phasor power injections.
POWER FREQUENCY, 50.0,

MISCELANEA CARD SIGUE 11 B-1,11 B-2

34567890123456789012345678901234567890123456789012345678901234567890

DELTAT THAX XOPT COPT EPSILN TOLMAT

.000200 .000 50.50.(T-max = 0 means that no transient solution follows

IOUT IPLOT IDOURL KSSOUT MAXOUT IPUN MEMSAV ICAT NERERG IFRSUP

1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72

1 1 1 0 1

CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN F.U.

BASE 100 MVA =1; UE=132 KV

SIGUE FORMATO RULE BOOK 4A-2

34567890123456789012345678901234567890123456789012345678901234567890

BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION

A6 A6 A6 A6 E6.2 E6.2 E6.2 11

3-8 9-14 15-20 21-26 27-32 33-38 39-44 80

LAS OPCIONES DE SALIDA SON: (1V-A.2 RULE BOOK ACTUALIZ)

EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG

RECRE LARIO 0.11 0.22 4

LARIO AIMOG .16 .30 4

LARIO PATQU .08 .16 4

PATQU CHAMI .08 .16 4

PATQU NONOG .14 .26 4

CHAMI CHEPE .09 .28 4

CHEPE LUJAN .09 .27 4

NONOG VUNIO .11 .21 4

NONOG CHILE .01 .02 4

LANK card ending branch cards.

LANK card ending switch cards.

SOURCE CARD SIGUE FORMATO RULE BOOK VII-4

34567890123456789012345678901234567890123456789012345678901234567890

NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP

I2 A6 I2 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6

1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

4LUJAN 1.10 50. 15.0 -1.

4RECRE 1.10 50. 15.0 -1.

LANK card terminating all EMTP source cards.

Next come power constraints of the load flow. There will be one
for each non-slack generator. So, 3 of them will apply to nodes

that have no Type-14 source as required by the algorithm. The program will define these internally. Yet, this is only possible for TMAX non-positive (no transient continuation). If data is modified to make TMAX > 0, a KTWL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data. Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 + 1.02

VALORES DE POTENCIA EN PU 1=100 MVA

PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4;10-6

34567890123456789012345678901234567890123456789012345678901234567890

NKBUS1	BUS2	BUS3	PK or QK	QK or VK	VMIN	VMAX	THMIN	THMAX
1-2	3-8	9-14	15-20	21-36	37-52	53-60	61-68	69-74 75-80

LARIO	-0.6000	-0.100	.65	1.25				
CHAMI	-0.080	-.034	.65	1.25				
PATOU	-0.150	-.089	.65	1.25				
NONOG	-0.10	-.061	.65	1.25				
VUNITO	-.0600	-.02	.65	1.25				
LUJAN	1.0	1.20					-20.	40.
RECKE	0.8	1.10					-20.	15.
CHEFE	-.26	0.09	-.09	1.5				
AIMOG	-0.050	(-0.01)	.65	1.15				
CHILE	-.0151	0.1	-.01	1.15				

The following load-flow miscellaneous data card has two peculiarities. The use of VSCALE = 1.414 is the special flag requesting RMS rather than peak voltages. The use of KTAPER = 0 ensures constant acceleration factors (this works well for this problem whether RMS or peak values are used).

NNNOUT	NITERA	NFLOUT	NPRINT	KALCHK	CFITEV	CFITEA	VSCALE	KTAPER
10-16	17-24	25-32	33-40	41-48	50-56	57-64		
1	2500	20	1	.01	0.2	2.5	1.414	2

PUNCH (Flush punched cards: R-L branches for equivalent impedance loads

LANX card ending requests for output variables

LANX card ending plot cards

EGIN NEW DATA CASE

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
 te (dd-mth-yy) and time of day (hh.mm.ss) = 04-May-94 15.55.48 Name of disk plot file, if any, is C:\45041555.pl4
 information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
 al length of "LABCOM" tables = 444863 INTEGER words. "VARDIM" List Sizes follow: 752 900 1500 150 7500
 120 2100 5250 225 480 150 150 15000 60 64800 120 12 15 4800 1980 300 450 12000 9 1200 252 4

 criptive interpretation of input data cards. ; Input data card images are shown below, all 80 columns, character by character
 0 1 2 3 4 5 6 7 8
 0123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890

 ment card. KOMPAR = 1. ;C data:C:\RIV\EMIN\PROBE2.DAT
 ment card. KOMPAR = 1. ;C DATA:C:\RIV\EMIN\PROBE2.DAT(-05-04-94 15:55:RETCMD Y AGREGO DATOS DE ARCH
 ment card. KOMPAR = 1. ;C RED 132 KV LA RIOJA; DATOS DE RED FLU132E.W01 12-12-93)
 ment card. KOMPAR = 1. ;C (SE AGREGAN LOS DATOS DE RESTRICCIONES Y RAMAS COMPLETAS +XC)
 se all of 0 cards in the punch buffer. ;ERASE
 ker card preceding new EMTP data case. ;REGIN NEW DATA CASE
 th of time-step loop numbers. W=13 S=2 ;PRINTED NUMBER WIDTH, 13, 2, { Request maximum precision for 8 output columns
 laration of desired EMTP load flow usage. ;FIX SOURCE { An EMTP load flow will satisfy requested phasor power injections.
 power frequency STATFR = 5.00000000E+01 Hz. ;POWER FREQUENCY, 50.0,
 ment card. KOMPAR = 1. ;C MISCELANEA CARD SIGUE II B-1,II B-2
 ment card. KOMPAR = 1. ;C 3456789012345678901234567890123456789012345678901234567890123456789012345678901234567890
 ment card. KOMPAR = 1. ;C DELTAT TMAX XOPT COPT EPSILN TOLHAT
 c. data. 2.000E-04 0.000E+00 5.000E+01 ;.000200 .000 50.50.{ T-max = 0 means that no transient solution follows
 ment card. KOMPAR = 1. ;C IOUT IPLOT IDOUBL KSSOUT MAXOUT IPUN NENSAV ICAT NERERG IPRSUP
 ment card. KOMPAR = 1. ;C 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
 c. data. 1 1 0 1 0 1 0 0 0 0 ; 1 1 1 0 1
 ment card. KOMPAR = 1. ;C
 ment card. KOMPAR = 1. ;C CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.
 ment card. KOMPAR = 1. ;C BASE 100 MVA =1; UB=132 KV
 ment card. KOMPAR = 1. ;C SIGUE FORMATO RULE BOOK 4A-2
 ment card. KOMPAR = 1. ;C 3456789012345678901234567890123456789012345678901234567890123456789012345678901234567890
 ment card. KOMPAR = 1. ;C BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
 ment card. KOMPAR = 1. ;C A6 A6 A6 A6 E6.2 E6.2 E6.2 11
 ment card. KOMPAR = 1. ;C 3-8 9-14 15-20 21-26 27-32 33-38 39-44 80
 ment card. KOMPAR = 1. ;C LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUAL12)
 ment card. KOMPAR = 1. ;C EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG
 ies R-L-C. 1.100E-01 7.003E-04 0.000E+00 ; RECRE LARIO 0.11 0.22 4
 ies R-L-C. 1.600E-01 9.549E-04 0.000E+00 ; LARIO AIMOG .16 .30 4
 ies R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; LARIO PATOU .08 .16 4
 ies R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; PATOU CHANI .08 .16 4
 ies R-L-C. 1.400E-01 8.276E-04 0.000E+00 ; PATOU NONOG .14 .26 4
 ies R-L-C. 9.000E-02 8.913E-04 0.000E+00 ; CHANI CHEPE .09 .28 4
 ies R-L-C. 9.000E-02 8.574E-04 0.000E+00 ; CHEPE LUJAN .09 .27 4
 ies R-L-C. 1.100E-01 6.685E-04 0.000E+00 ; NONOG VUNIO .11 .21 4
 ies R-L-C. 1.000E-02 6.366E-05 0.000E+00 ; NONOG CHILE .01 .02 4
 ment card. KOMPAR = 1. ;C
 ment card. KOMPAR = 1. ;C
 ment card. KOMPAR = 1. ;C
 nk card ending branches. IBR, NTOT = 9 11 ;BLANK card ending branch cards.
 nk card ending switches. KSWTCH = 0. ;BLANK card ending switch cards.
 ment card. KOMPAR = 1. ;C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
 ment card. KOMPAR = 1. ;C 3456789012345678901234567890123456789012345678901234567890123456789012345678901234567890

```

ment card.  KOMPAT = 1.      IC NAME IV AMPLITUDE FREQUENCY PHASE  A1  TIME-1  TSTART  TSTOP
ment card.  KOMPAT = 1.      IC 12 A6 I2  E10.6  E10.6  E10.6  E10.6  E10.6  E10.6
ment card.  KOMPAT = 1.      IC 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
ment card.  KOMPAT = 1.      IC
rce. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114LUJAN 1.10 50. 15.0 -1.
rce. 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 114RECRE 1.10 50. 15.0 -1.
ment card.  KOMPAT = 1.      IC
ment card.  KOMPAT = 1.      IC
nk card ends electric network sources.  BLANK card terminating all EMTP source cards.
ment card.  KOMPAT = 1.      IC Next come power constraints of the load flow. There will be one
ment card.  KOMPAT = 1.      IC for each non-slack generator. So, 3 of them will apply to nodes
ment card.  KOMPAT = 1.      IC that have no Type-14 source as required by the algorithm. The
ment card.  KOMPAT = 1.      IC program will define these internally. Yet, this is only possible
ment card.  KOMPAT = 1.      IC for TMAX non-positive (no transient continuation). If data is
ment card.  KOMPAT = 1.      IC modified to make TMAX > 0, a KILL = 40 error termination will
ment card.  KOMPAT = 1.      IC will result. Yet, the transient simulation is possible as a
ment card.  KOMPAT = 1.      IC 2nd simulation that replaces the power constraints at load nodes
ment card.  KOMPAT = 1.      IC by constant-impedance loads. Branch cards for these will be
ment card.  KOMPAT = 1.      IC punched by the present subcase, and the transient continuation
ment card.  KOMPAT = 1.      IC will be illustrated by the following (4th of 4) subcase.
ment card.  KOMPAT = 1.      IC The following 4 cards would be used if peak rather than RMS input data.
ment card.  KOMPAT = 1.      IC Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.826428 ) = 1.414212
ment card.  KOMPAT = 1.      IC (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02
ment card.  KOMPAT = 1.      IC
ment card.  KOMPAT = 1.      IC VALORES DE POTENCIA EN PU 1=100 MVA
ment card.  KOMPAT = 1.      IC PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4;10-6
ment card.  KOMPAT = 1.      IC 34567890123456789012345678901234567890123456789012345678901234567890
ment card.  KOMPAT = 1.      IC NKBUS1 BUS2 BUS3 PK or BK BK or VK VMIN VMAX TMIN TMAX
ment card.  KOMPAT = 1.      IC 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
X. -6.000E-01 -1.000E-01 6.500E-01 1.250E+00 1 LARIO -0.6000 -0.100 .65 1.25
X. -8.000E-02 -3.400E-02 6.500E-01 1.250E+00 1 CHAMI -0.080 -0.034 .65 1.25
X. -1.500E-01 -8.900E-02 6.500E-01 1.250E+00 1 PATOU -0.150 -0.089 .65 1.25
X. -1.000E-01 -6.100E-02 6.500E-01 1.250E+00 1 NONOG -0.10 -0.061 .65 1.25
X. -6.000E-02 -2.000E-02 6.500E-01 1.250E+00 1 VUNIO -0.0600 -0.02 .65 1.25
ment card.  KOMPAT = 1.      IC LUJAN 1.0 1.20 -20. 40.
X. 8.000E-01 1.100E+00 0.000E+00 1.000E+19 1 RECRE 0.8 1.10 -20. 15.
X. -2.600E-01 -9.000E-02 0.000E+00 1.500E+00 1 CHEPE -0.26 -0.09 1.5
X. -5.000E-02 -1.000E-02 6.500E-01 1.150E+00 1 AIMOG -0.050 -0.01 .65 1.15
X. -1.510E-02 -1.000E-02 0.000E+00 1.150E+00 1 CHILE -0.0151 -0.01 1.15
ment card.  KOMPAT = 1.      IC The following load-flow miscellaneous data card has two peculiarities. The
ment card.  KOMPAT = 1.      IC use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
ment card.  KOMPAT = 1.      IC voltages. The use of KTAPER = 0 ensures constant acceleration factors
ment card.  KOMPAT = 1.      IC (this works well for this problem whether RMS or peak values are used).
ment card.  KOMPAT = 1.      IC NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE KTAPER
ment card.  KOMPAT = 1.      IC 10-16 17-24 25-32 33-40 41-48 50-56 57-64
LASTOV, NTOT, NEXT, IOFKOL, IOFKOR, NCURR = 9 11 19 0 0 0
ad flow iter. 1 2500 20 1 1.00E-02 1 2500 20 1 .01 0.2 2.5 1.414 2
x del-V: .0232 .0227 .0223 .0218 .0213 .0209 .0204 .0168 .0151 .0155 .0158 .0137 .0136 .0134 .0133 .0131 .0129 .0127 .0126 .0127
urce No. -4 -4 -4 -4 -4 -4 -4 -4 -9 -9 -9 -5 -5 -5 -5 -5 -5 -5 -5 -5
x del-V: .0129 .0131 .0132 .0134 .0112 .0111 .0107 .0109 .0114 .0114 .0115 .0113 .0114 .0116 .0116 .0116 .0116 .0116 .0116 .0116
urce No. 7 7 7 7 -5 4 -5 -4 4 9 4 9 4 -4 4 -4 4 -4 4 -4
x del-V: .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0115 .0116 .0115 .0115 .0115 .0115 .0115 .0115 .0115 .0115 .0115 .0115

```


[illegible]

```

rce No.      4      9      4      9      4      9      4      9      4      9      4      9      4      9      4      9      4      9
del-V: .0115 .0109 .0115 .0109 .0115 .0109 .0115 .0109 .0115 .0109 .0115 .0109 .0115 .0109 .0115 .0109 .0115 .0109
rce No.      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4
del-V: .0114 .0107 .0112 .0105 .0111 .0102 .0106 .0099 .0102 .0095 .0098 .009 .0093 .0085 .0087 .0079 .0081 .0073 .0075 .0067
rce No.      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4      4      -4
del-V: .0069 .0061 .0063 .0055 .0057 .005 .0051 .0045 .0046 .004 .0041 .0035 .0036 .0031 .0031 .0027 .0027 .0023 .0023 .002
rce No.      4      -4      4      9      4      9      4      9      4      9      4      9      4      9      4      9      4      9
del-V: .002 .0017 .0017 .0014 .0014 .0012 .0012 .001 1.E-3 .9E-3 .8E-3 .7E-3 .7E-3 .6E-3
rce No.      4      9      4      9      4      9      4      9      4      9      4      9      4      9      4      9      4      9

```

t the load flow iteration loop with counter NEKITE = 1174. If no warning on the preceding line, convergence was attained.

W	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	3	LARIO	9.28771724E-01	-3.83021	-6.05297249E-01	-1.01333027E-01
4	6	CHAMI	9.14067560E-01	0.03602	-8.15944246E-02	-3.57953410E-02
5	5	PATOU	8.86450424E-01	-3.18287	-1.52856024E-01	-9.18227729E-02
6	7	NONOS	8.22849857E-01	-5.52740	-9.12444236E-02	-5.47409171E-02
7	10	VUNIO	8.08473882E-01	-6.34608	-5.88287661E-02	-2.55332895E-02
2	2	RECRE	1.10000000E+00	2.92279	7.92189169E-01	4.92476038E-01
8	8	CHEFE	9.73986618E-01	6.49866	-2.60334271E-01	-9.09189807E-02
9	4	AIMOG	9.15201725E-01	-4.82378	-5.52645254E-02	-1.15109735E-02
0	11	CRILE	8.22617728E-01	-5.53551	-2.07005901E-02	-2.41525877E-02

usoidal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P"
printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage Rectangular	Polar	Phasor branch current Rectangular	Polar	Power flow P and Q	Power loss P and Q
RECRE		1.5536161614004 .07922640365088	1.5556349186104 2.9192602	1.0494008279247 -.5804598614411	1.1992396542782 -28.9484975	.77218916938257 .49247603768196	.07907956616163 0.1581993
	LARIO	1.3104809008116 -.087791193734	1.3134182445395 -3.8326086	-1.049400827925 .5804598614413	1.1992396542782 151.0515025	-.7130895032209 -.3342767053587	
	ARIO	1.3104809008116 -.087791193734	1.3134182445395 -3.8326086	.08360269348548 -.0249103269637	.08723493974648 -16.5919947	.05587332020479 .01265246372923	.6067947798E-3 0.0011415
	AIMOG	1.2896313717649 -.1088863494655	1.2942199628116 -4.8261593	-.0336026934855 .02491032696372	.08723493974648 163.4080053	-.055264525425 -.0115109735171	
	ARIO	1.3104809008116 -.087791193734	1.3134182445395 -3.8326086	.05646056469127 -.3399814295336	.34463773413971 -80.5709683	.05191893361155 .22029121483062	.00475100671172 0.0095029
	PATOU	1.251567026911 -.0696263697219	1.2535022354234 -3.1841597	-.0564605646913 .33998142953358	.34463773413971 99.4290317	-.0471679268998 -.2107892014072	
	ATOU	1.251567026911 -.0696263697219	1.2535022354234 -3.1841597	-.4547027359239 .02912071771365	.4556342768678 176.3355869	-.2855592605933 -.0023936146427	.00330410377027 0.0166082
	CHAMI	1.2926025606191 .79641060879E-3	1.2926028059651 0.0353016	.45470273592391 -.0291207177137	.4556342768678 -3.6644131	.29386336436361 .01900182218323	
	ATOU	1.251567026911 -.0696263697219	1.2535022354234 -3.1841597	.27579124346107 -.2092753910589	.34620391711193 -37.1919118	.17987116315175 .12136004311169	.0083899558088 0.0155614

NONOG	1.1585445991511 -.1120335102736	1.1639489231261 -5.5234387	-.2757912434611 .20927559105894	.34620381711193 142.8080882	-.1714811673429 -.1057786223239	
ANI	1.2926025606191 .79641060879E-3	1.2926028059651 0.0353016	-.5809850915891 .08442732572258	.58708750148739 171.7317461	-.3754577889268 -.0547971632035	.01551022804823 0.0462540
CHEPE	1.3685310100644 .15587373193871	1.3773793035386 6.49779053	.58098509158911 -.0844278257226	.58708750148739 -8.2682537	.39096801697478 .1030512060202	
EPE	1.3685310100644 .15587373193871	1.3773793035386 6.49779053	-.97151063419 .1728184334125	.98676193849956 169.9133747	-.6513022876653 -.1939701867025	.04381646054721 0.1314454
LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.97151063419 -.1728184334125	.98676193849956 -10.0866253	.69511874821349 .32541956834410	
NOS	1.1585445991511 -.1120335102736	1.1639489231261 -5.5234387	.0973581085134 -.0557749203786	.11220268727644 -29.8077127	.0595211854585 .02685518106116	.69241736701E-3 0.0013219
VUNIO	1.1361224739351 -.1263434718197	1.1431259548501 -6.3455540	-.0973581085134 .05577492037857	.11220268727644 150.1922871	-.0588287560915 -.0255332895423	
NOS	1.1585445991511 -.1120335102736	1.1639489231261 -5.5234387	.03143047689324 -.0447857725909	.05471416913656 -54.9389746	.02071555828354 .02418252414306	.14968201522E-4 0.0000299
CHILE	1.1573345789303 -.1122142620855	1.1627519568094 -5.5380430	-.0314304768932 .04478577259094	.05471416913656 125.0610252	-.020700590082 -.024152587746	
Total network loss P-loss by summing injections = 1.611876433962E-01						

ution at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed
ult applying to the composite group. The entry "MVA" is $\text{SQRT}(P^2 + Q^2)$ in units of power, while "P.F." is the
associated power factor.

Node name	Source Rectangular	node voltage Polar	Injected Rectangular	source current Polar	Injected P and Q	source power MVA and P.F.
RECRE	1.5536161614004 .07922640365088	1.5556349186104 2.9192602	1.0494008279247 -.5904598614411	1.1972396542782 -28.9484975	.79218916938257 .49247603768196	.93278954098873 0.8492689
LARIO	1.3104809008116 -.087791193734	1.3134182445395 -3.3326086	-.909337569748 .21556810494384	.93453968541962 165.6636157	-.6052972494046 -.1013330267982	.61372073653819 -0.9862747
AIMOG	1.2896313717649 -.1088863494655	1.2942199628116 -4.8261593	-.0836026934855 .02491032696372	.08723493994648 163.4080053	-.055264528425 -.0115109735171	.0564506003667 -0.9789892
PATOU	1.251567026911 -.0696263697219	1.2535022354234 -3.1841597	-.2353720571541 .1598265561883	.28450752775976 145.8220077	-.1528560243414 -.0918227729382	.17831541192082 -0.8572227
CHAMI	1.2926025606191 .79641060879E-3	1.2926028059651 0.0353016	-.1262823556652 .05530710800892	.13786264740191 156.3483186	-.0815944245631 -.0357953410203	.08910032243474 -0.9157539
NONOG	1.1585445991511 -.1120335102736	1.1639489231261 -5.5234387	-.1470026580544 .10871489808942	.18283520049941 143.5154537	-.0912444236009 -.0547409171137	.10640541736542 -0.8575167

CHEPE	1.3685310100644 .15587373193871	1.3773793035386 6.4979053	-.3905255426009 .08837060768792	.40040367000255 167.2466924	-.2603342706713 -.0909189806823	.2757538640612 -0.7440820
LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.97151063419 -.1728184334125	.98676193849956 -10.0866253	.69511874821349 .32541956834418	.7675206637428 0.9056678
VUNIO	1.1361224739351 -.1263434718197	1.1431259548501 -6.3455540	-.0973581085134 .05577492037857	.11220268729644 150.1922871	-.0588287660915 -.0255332895423	.06413090202624 -0.9173232
CHILE	1.1573345789303 -.1122142620855	1.1627619568094 -5.5380430	-.0314304768932 .04478577259094	.05471416713656 125.0610252	-.020700590082 -.024152587746	.03180977718522 -0.6507619

ment card. KOMPAR = 1.

IC

ment card. KOMPAR = 1.

IC

ment card. KOMPAR = 1.

IC

uest for flushing of punch buffer.

: \$PUNCH

(Flush punched cards: R-L branches for equivalent impedance loads

isting of 80-column card images now being flushed from punch buffer follows.

=====

4567890123456789012345678901234567890123456789012345678901234567890123456789

=====

=====< End of LUNIT7 punched cards as flushed by \$PUNCH request >=====

nk card ending node names for voltage output. !BLANK card ending requests for output variables

ective branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be
mented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

From	To	Branch voltage Vkm = V _k - V _m				Branch current Ikm from K to M			
bus K	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
CRE	LARIO	2.9497395E-01	34.486451	2.4313526E-01	1.6701760E-01	1.1992397E+00	-28.948497	1.0494008E+00	-5.8045986E-01
RIO	AINOG	2.9659880E-02	45.335518	2.0849529E-02	2.1095156E-02	8.7234940E-02	-16.591995	8.3602693E-02	-2.4910327E-02
RIO	PATOU	6.1650672E-02	-17.136020	5.8713874E-02	-1.8164824E-02	3.4463773E-01	-80.570968	5.8460565E-02	-3.3998143E-01
TQU	CHAMI	8.1506337E-02	-120.229464	-4.1035534E-02	-7.0422780E-02	4.5563428E-01	176.335587	-4.5470274E-01	2.9120718E-02
TQU	NONOG	1.0223276E-01	24.507332	9.3022428E-02	4.2407141E-02	3.4620382E-01	-37.191912	2.7579124E-01	-2.0927589E-01
AMI	CHEPE	1.7266761E-01	-116.087143	-7.5928449E-02	-1.5507732E-01	5.8708750E-01	171.731746	-5.8098509E-01	8.4427826E-02
EPE	LUJAN	2.8083737E-01	-118.521574	-1.3409693E-01	-2.4675421E-01	9.8676194E-01	169.913375	-9.7151063E-01	1.7281843E-01
NGB	VUNIO	2.6599374E-02	32.546312	2.2422125E-02	1.4309962E-02	1.1220269E-01	-29.807713	9.7358109E-02	-5.5774920E-02
NGB	CHILE	1.2234460E-03	8.495974	1.2100202E-03	1.8075181E-04	5.4714169E-02	-54.938975	3.1430477E-02	-4.4785773E-02

tual List Sizes for the preceding solution follow. 04-May-94 15:56:25

Size 1-10: 11 9 9 2 -9999 0 -9999 -9999 0 0

Size 11-20: -9999 -9999 -9999 -9999 -9999 0 0 9 23 0

Size 21-29: 0 -9999 9 -9999 -9999 -9999 -9999 -9999 -9999

conds for overlays 1-5 : 21.539 0.000 21.539 --- (CP: 1/0; tot)

conds for overlays 6-11 : 16.047 0.000 16.047

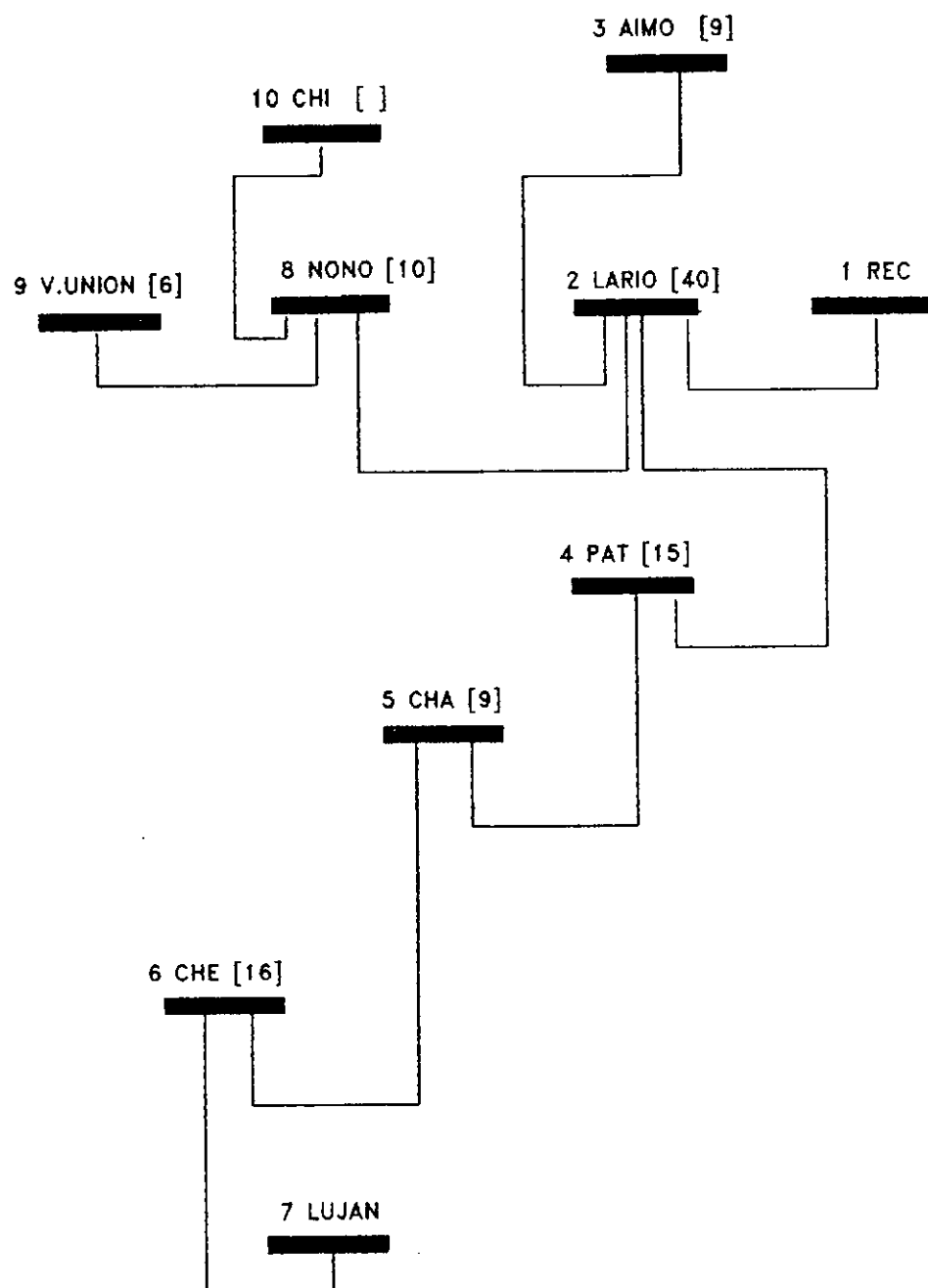
conds for overlays 12-15 : 0.000 0.000 0.000

conds for time-step loop : 0.000 0.000 0.000

conds after DELTAT-loop : 0.328 0.000 0.328

Totals : 37.914 0.000 37.914

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 290
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

Path: C:\RIV\ENIN

File: PROBE4 .DAT S:857-7a7-06-04-94 15:26:08** Page 1

CASO 290

A:C:\RIV\ENIN\PROBE3.DAT(-06-04-94 15:21; RED 132 KV LA RIOJA;
 ISO=110; LINEA=EN=240 MHZ (NO PATQUIA-NONOGASTA SI LARIO-NONOGASTA);
 SE

NEW DATA CASE

ED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
 SOURCE (An ENTP load flow will satisfy requested phasor power injections.
 FREQUENCY, 50.0,

ACELANEA CARD SIGUE II B-1, II B-2

67890123456789012345678901234567890123456789012345678901234567890

STAT TMAX XOPT COPT EPSILN TOLNAT

200 .000 50.50. (T-max = 0 means that no transient solution follows

IT IPLOT IDGURL KSSOUT MAXOUT IPUN MENSAV ICAT MERERG IPRSUP

8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72

1 1 1 0 1

RGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.

SE 100 MVA =1; UB=132 KV

RUE FORMATO RULE BOOK 4A-2

67890123456789012345678901234567890123456789012345678901234567890

S1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION

S A6 A6 A6 E6.2 E6.2 E6.2 11

S-B 9-14 15-20 21-26 27-32 33-38 39-44 80

S OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)

BO 1=CORRIENTE RAMA;2=VOLT RAMA;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG

CRE LARIO 0.11 0.22 4

RIO AIMOG .16 .30 4

RIO PATGU .08 .16 4

TQU CHAMI .08 .16 4

TQU NONOG .14 .26 4

AMI CHEPE .11 .35 4

EPE LUJAN .105 .34 4

NOG VUNIO .11 .21 4

NOG CHILE .01 .02 4

RIO NONOG .08 .16 4

K card ending branch cards.

K card ending switch cards.

URCE CARD SIGUE FORMATO RULE BOOK VII-4

557890123456789012345678901234567890123456789012345678901234567890

ME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP

A6 12 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6

2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

JAN 1.10 50. 15.0 -1.

CRE 1.10 50. 15.0 -1.

K card terminating all ENTP source cards.

Next come power constraints of the load flow. There will be one
 for each non-slack generator. So, 3 of them will apply to nodes
 that have no Type-14 source as required by the algorithm. The

program will define these internally. Yet, this is only possible for TMAX non-positive (no transient continuation). If data is modified to make TMAX > 0, a KILL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data. Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02

ORES DE POTENCIA EN PU 1=100 MVA									
RA RESTRICCIÓN DE POTENCIASIGUE RULE BOOK 10-4;10-6									
567890123456789012345678901234567890123456789012345678901234567890									
BUS1	BUS2	BUS3	PK or QK	QK or VK	VMIN	VMAX	THMIN	THMAX	
2	3-8	9-14	15-20	21-36	37-52	53-60	61-68	69-74	75-80
RIO			-0.4000	-0.200	.65	1.25			
AMI			-0.080	-.034	.65	1.25			
TOU			-0.150	-.080	.65	1.25			
MOG			-0.10	-.061	.65	1.25			
NIO			-.0600	-.02	.65	1.25			
JAN			1.0	1.20			-20.	40.	
CRE			0.8	1.10			-20.	15.	
EPE			-.16	-.09		1.5			
MOG			-0.090	-0.04	.65	1.15			
ILE			-.1000	-.04		1.15			

The following load-flow miscellaneous data card has two peculiarities. The use of VSCALE = 1.414 is the special flag requesting RMS rather than peak voltages. The use of KTAPER = 0 ensures constant acceleration factors (this works well for this problem whether RMS or peak values are used).

NNNOUT	NITERA	NFLOUT	NPRINT	RALCHK	CFITEV	CFITEA	VSCALE	KTAPER
10-16	17-24	25-32	33-40	41-48	50-56	57-64		
1	2500	20	1	.01	0.2	2.5	1.414	2

CH { Flush punched cards: R-L branches for equivalent impedance loads
K card ending requests for output variables
K card ending plot cards
N NEW DATA CASE

Path: C:\ATP

File: AP61528 .SAL 40.060 .a..06-04-94 15:27:14

Page 1

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
 e (dd-mm-yy) and time of day (hh.mm.ss) = 06-Apr-94 15.26.41 Name of disk plot file, if any, is C:\44061528.pl4
 information, consult the copyrighted ATP ENTP Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
 i length of "LARCQM" tables = 444863 INTEGER words. "VARDIM" List Sizes follow: 752 900 1500 150 7500
 20 2100 5250 225 480 150 150 15000 60 64800 120 12 15 4800 1980 300 450 12000 7 1200 252 4

riptive interpretation of input data cards. Input data card images are shown below, all 80 columns, character by character
 0 1 2 3 4 5 6 7 8
 0123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890

ment card. KOMPAR = 1. ;C data:C:\RIV\EMIN\PROBE4.DAT
 ment card. KOMPAR = 1. ;C DATA:C:\RIV\EMIN\PROBE3.DAT(-06-04-74 15:21; RED 132 KV LA RIOJA;
 ment card. KOMPAR = 1. ;C CASO 110; LINEA EN 240 MM2 (NO PATBUA-NONOGASTA SI LARIO-NONOGASTA)
 e all of 0 cards in the punch buffer. ;*ERASE
 er card preceding new ENTP data case. ;BEGIN NEW DATA CASE
 h of time-step loop numbers. W=13 S=2 ;PRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns
 aration of desired ENTP load flow usage. ;FIX SOURCE (An ENTP load flow will satisfy requested phasor power injections.
 power frequency STATFR = 5.00000000E+01 Hz. ;POWER FREQUENCY, 50.0,
 ment card. KOMPAR = 1. ;C MISCELANEA CARD SIGUE II 8-1,II 8-2
 ment card. KOMPAR = 1. ;C 34567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890
 ment card. KOMPAR = 1. ;C DELTAT TMAX XOPT COPT EPSILN TOLNAT
 t. data. 2.000E-04 0.000E+00 5.000E+01 ;.000200 .000 50.50.(T-max = 0 means that no transient solution follows
 ment card. KOMPAR = 1. ;C IOUT IPLOT IDOURL KSSOUT MAXOUT IPUN MENSAV ICAT NERERG IPRESUP
 ment card. KOMPAR = 1. ;C 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
 t. data. 1 1 0 1 0 1 0 0 0 0 ; 1 1 1 0 1
 ment card. KOMPAR = 1. ;C
 ment card. KOMPAR = 1. ;C CARGA DE VALORES PASIVOS DE LOS DISTINTOS RAMOS (R-L) VALORES EN P.U.
 ment card. KOMPAR = 1. ;C BASE 100 MVA =1; UB=132 KV
 ment card. KOMPAR = 1. ;C SIGUE FORMATO RULE BOOK 4A-2
 ment card. KOMPAR = 1. ;C 34567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890
 ment card. KOMPAR = 1. ;C BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
 ment card. KOMPAR = 1. ;C A6 A6 A6 A6 E6.2 E6.2 E6.2 11
 ment card. KOMPAR = 1. ;C 3-8 9-14 15-20 21-26 27-32 33-38 39-44 80
 ment card. KOMPAR = 1. ;C LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)
 ment card. KOMPAR = 1. ;C EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;;3=I y V DE RAMA; 4=CONSUMO POT Y ENERE
 ies R-L-C. 1.100E-01 7.003E-04 0.000E+00 ; RECRE LARIO 0.11 0.22 4
 ies R-L-C. 1.600E-01 9.549E-04 0.000E+00 ; LARIO AIMOG .16 .30 4
 ies R-L-C. 6.000E-02 5.093E-04 0.000E+00 ; LARIO PATQU .08 .15 4
 ies R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; PATQU CHAM .08 .16 4
 ment card. KOMPAR = 1. ;C PATQU NONOG .14 .26 4
 ies R-L-C. 1.100E-01 1.114E-03 0.000E+00 ; CHAM CHEPE .11 .33 4
 ies R-L-C. 1.050E-01 1.082E-03 0.000E+00 ; CHEPE LUJAN .105 .34 4
 ies R-L-C. 1.100E-01 6.685E-04 0.000E+00 ; NONOG VUNIO .11 .21 4
 ies R-L-C. 1.000E-02 6.366E-05 0.000E+00 ; NONOG CHILE .01 .02 4
 ies R-L-C. 8.000E-02 5.093E-04 0.000E+00 ; LARIO NONOG .06 .16 4
 ment card. KOMPAR = 1. ;C
 ment card. KOMPAR = 1. ;C
 nk card ending branches. IBR, NTOT = 9 11 ;BLANK card ending branch cards.
 nk card ending switches. KSWTCH = 0. ;BLANK card ending switch cards.
 ment card. KOMPAR = 1. ;C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
 ment card. KOMPAR = 1. ;C 34567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890
 ment card. KOMPAR = 1. ;C NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP

```

Comment card.  KOMPAT = 1.      IC 12 A6 12  E10.6  E10.6  E10.6  E10.6  E10.6  E10.6  E10.6
Comment card.  KOMPAT = 1.      IC 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
Comment card.  KOMPAT = 1.      IC
Source.  1.10E+00 5.00E+01 1.50E+01 -1.00E+00 14LUJAN 1.10 50. 15.0 -1.
Source.  1.10E+00 5.00E+01 1.50E+01 -1.00E+00 14RECRE 1.10 50. 15.0 -1.
Comment card.  KOMPAT = 1.      IC
Comment card.  KOMPAT = 1.      IC
Blank card ends electric network sources.  BLANK card terminating all EMTP source cards.
Comment card.  KOMPAT = 1.      IC      Next cone power constraints of the load flow. There will be one
Comment card.  KOMPAT = 1.      IC      for each non-slack generator. So, 3 of them will apply to nodes
Comment card.  KOMPAT = 1.      IC      that have no Type-14 source as required by the algorithm. The
Comment card.  KOMPAT = 1.      IC      program will define these internally. Yet, this is only possible
Comment card.  KOMPAT = 1.      IC      for TMA non-positive (no transient continuation). If data is
Comment card.  KOMPAT = 1.      IC      modified to make TMAX > 0, a KILL = 40 error termination will
Comment card.  KOMPAT = 1.      IC      will result. Yet, the transient simulation is possible as a
Comment card.  KOMPAT = 1.      IC      2nd simulation that replaces the power constraints at load nodes
Comment card.  KOMPAT = 1.      IC      by constant-impedance loads. Branch cards for these will be
Comment card.  KOMPAT = 1.      IC      punched by the present subcase, and the transient continuation
Comment card.  KOMPAT = 1.      IC      will be illustrated by the following (4th of 4) subcase.
Comment card.  KOMPAT = 1.      IC      The following 4 cards would be used if peak rather than RMS input data.
Comment card.  KOMPAT = 1.      IC      Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.828428 ) = 1.414212
Comment card.  KOMPAT = 1.      IC      (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02
Comment card.  KOMPAT = 1.      IC
Comment card.  KOMPAT = 1.      IC VALORES DE POTENCIA EN PU 1=100 MVA
Comment card.  KOMPAT = 1.      IC PARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4:10-6
Comment card.  KOMPAT = 1.      IC 34567890123456789012345678901234567890123456789012345678901234567890
Comment card.  KOMPAT = 1.      IC NKBUS1 BUS2 BUS3 PK or BK BK or VK VMIN VMAX THMIN THMAX
Comment card.  KOMPAT = 1.      IC 1-2 3-9 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
FIX.  -4.000E-01 -2.000E-01 6.500E-01 1.250E+00 LARIO -0.4000 -0.200 .65 1.25
FIX.  -8.000E-02 -3.400E-02 6.500E-01 1.250E+00 CHANT -0.080 -0.034 .65 1.25
FIX.  -1.500E-01 -8.000E-02 6.500E-01 1.250E+00 PATGU -0.150 -0.080 .65 1.25
FIX.  -1.000E-01 -6.100E-02 6.500E-01 1.250E+00 NONG -0.10 -0.061 .65 1.25
FIX.  -6.000E-02 -2.000E-02 6.500E-01 1.250E+00 VUNID -0.0600 -0.02 .65 1.25
Comment card.  KOMPAT = 1.      IC LUJAN 1.0 1.20 -20. 40.
FIX.  8.000E-01 1.100E+00 0.000E+00 1.000E+19 IRECRE 0.8 1.10 -20. 15.
FIX.  -1.600E-01 -9.000E-02 0.000E+00 1.500E+00 CHEPE -0.16 -0.09 1.5
FIX.  -9.000E-02 -4.000E-02 6.500E-01 1.150E+00 AIMBG -0.090 -0.04 .65 1.15
FIX.  -1.000E-01 -4.000E-02 0.000E+00 1.150E+00 CHILE -0.1000 -0.04 1.15
Comment card.  KOMPAT = 1.      IC      The following load-flow miscellaneous data card has two peculiarities. The
Comment card.  KOMPAT = 1.      IC      use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
Comment card.  KOMPAT = 1.      IC      voltages. The use of KTAPER = 0 ensures constant acceleration factors
Comment card.  KOMPAT = 1.      IC      (this works well for this problem whether RMS or peak values are used).
Comment card.  KOMPAT = 1.      IC      NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE KTAPER
Comment card.  KOMPAT = 1.      IC      10-16 17-24 25-32 33-40 41-48 50-56 57-64
<= LASTOV, NTOI, NEXT, IOFKOL, IOFKOR, NCURR = 9 11 19 0 0 0
Load flow iter. 1 2500 20 1 1.00E-02 1 2500 20 1 .01 0.2 2.5 1.414 2
Max del-V: .0232 .0227 .0223 .0218 .0213 .0207 .0204 .0149 .0152 .0149 .0137 .0136 .0134 .0133 .0131 .0129 .0127 .0125 .0124 .0126
Source No. 1 -4 -4 -4 -4 -4 -4 -9 -9 -9 -5 -5 -5 -5 -5 -5 -5 -5 7 7
Max del-V: .0128 .013 .0131 .0112 .0111 .0109 .0106 .0105 .0108 .0105 .0108 .0115 .0116 .0105 .0115 .0117 .0113 .0102 .0113 .0107
Source No. 7 7 7 -5 -5 4 -5 7 4 4 9 -5 -4 -4 -9 -4 -4 9 -9 -4
Max del-V: .0114 .0108 .0113 .0105 .0114 .0107 .0113 .0102 .0113 .0103 .011 .0117 .0117 .0124 .0102 .0111 .0118 .012 .0135 .0105
Source No. -4 4 -9 -4 -4 4 -9 -4 -4 9 -9 -4 4 -4 9 -9 -4 -9 -4 9

```


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[illegible]

Path: C:\ATP

File: AP61528.SAL 40.060 .a.. 06-04-94 15:27:14

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del-V: .0114 .0117 .0114 .0117 .0114 .0117 .0113 .0117 .0113 .0117 .0113 .0117 .0112 .0117 .0112 .0117 .0112 .0117
rce No. 9 4 9 4 9 4 9 4 9 4 9 4 4 4 4 4 4 4
del-V: .0112 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118
rce No. -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4
del-V: .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118 .0113 .0118
rce No. -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4
del-V: .0112 .0116 .0111 .0114 .0108 .0111 .0104 .0107 .01 .0102 .0095 .0096 .0089 .009 .0083 .0084 .0077 .0077 .007 .0071
rce No. -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4
del-V: .0063 .0064 .0057 .0057 .005 .0051 .0044 .0045 .0038 .0039 .0033 .0034 .0028 .0027 .0024 .0024 .002 .002 .0017 .0017
rce No. -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 9 4 9 4 9 4
del-V: .0014 .0014 .0012 .0012 .9E-3 .9E-3 .8E-3 .8E-3 .6E-3
rce No. 9 4 9 4 9 4 9 4 9
```

t the load flow iteration loop with counter NEKITE = 1209. If no warning on the preceding line, convergence was attained.

W	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	3	LARIO	8.89348959E-01	-3.80873	-4.04020805E-01	-2.03048523E-01
4	6	CHAM1	9.05428079E-01	0.16103	-8.18270015E-02	-3.56048400E-02
5	5	PATOU	8.82701351E-01	-2.45285	-1.52497678E-01	-8.17911190E-02
6	9	NOMOG	8.38623352E-01	-6.21261	-9.08492987E-02	-5.03486506E-02
7	10	VUNIO	8.24732158E-01	-7.03372	-6.01987321E-02	-2.43593172E-02
2	2	RECRE	1.10000000E+00	2.04657	7.92761431E-01	6.78039071E-01
8	7	CHEFE	9.70934254E-01	7.05285	-1.60428259E-01	-9.08059684E-02
9	4	AIMOG	8.57252277E-01	-5.40293	-9.32589514E-02	-4.23486528E-02
0	11	CHILE	8.36738430E-01	-6.33785	-1.09194030E-01	-5.54031841E-02

usoidal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage	Phasor branch current	Power flow	Power loss		
		Rectangular	Polar	P and Q	P and Q		
RECRE		1.5546456346292 .05547026888898	1.5556349156104 2.0434654	1.0496480231542 -1.3411526246414	1.3411526246414 -38.4964972	7.7276143126438 .67803907148634	.09692796574204 0.1978559
LARIO		1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	-1.049648023154 .8348229693006	1.3411526246414 141.5035028	-.6938374613223 -.4801831316023	
LARIO		1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	.14659910010062 -.084046811918	.16898272912901 -27.8261026	.09554336445337 .04663192719174	.00228441301951 0.0042833
AIMOG		1.2068533992447 -.1141540097252	1.2122401846189 -5.4034244	-.1465991001006 .08404681191799	.16898272912901 150.1738974	-.0932589514339 -.0423486527802	
LARIO		1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	-.1298428897114 -.1175239502998	.17513153600272 -137.8509909	-.0765966062631 .07220587479028	.00122684213611 0.0024537
PATOU		1.2471068979652 -.0534449912241	1.2482515700127 -2.4539194	.12984288971139 .11752395029979	.17513153600272 42.1490091	.0778234484592 -.0767521905981	
STOU		1.2471068979652 -.0534449912241	1.2482515700127 -2.4539194	-.3683458960794 .02386651846033	.36911828709613 176.2727727	-.2303211268575 -.0050389283986	.00544993237473 0.0108999
CHAM1		1.280393212628 .00358103066031	1.2803982203692 0.1602456	.3683458960794 -.02386651846033	.36911828709613 -3.7072273	.2357710592523 .01593879318811	

I	1.280393212628 .00358103066031	1.2803982203692 0.1602456	-.4963158669284 .07912409706717	.50258338703058 170.9419692	-.3175980607765 -.0515436331864	.01387245315095 0.0442033
CHEPE	1.3626813884637 .16858793450787	1.3730704490764 7.0526702	.49631586692843 -.0791240870672	.50258338703058 -9.0580308	.33145051412705 .09574669384728	
E	1.3626813884637 .16858793450787	1.3730704490764 7.0526702	-.7444658766525 .18169893720791	.76631843595364 166.2641848	-.4919187729672 -.1865528622466	.03093030712733 0.0998315
LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.74446587665248 -.1816989372079	.76631843595364 -13.7158152	.52274908009457 .28638433294455	
06	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	.09734877138892 -.0541045352449	.11137362356051 -29.0644457	.06088095671741 .02566174603322	.68222462137E-3 0.0013024
VUNIO	1.1573965688744 -.1428037440376	1.166173111915 -7.0338096	-.0973487713889 .0541045352449	.11137362356051 150.9355543	-.060198732096 -.0243593172106	
06	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	.17317298983299 -.113512317528	.20706021017633 -33.2442449	.10940839983566 .05583192343033	.21436965319E-3 0.0004287
CHILE	1.17544549098797 -.1306403375443	1.1827022669092 -6.3417867	-.173172989833 .11351231752795	.20706021017633 146.7557551	-.1091940301825 -.0554031841239	
10	1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	.41359218837384 -.2685564852355	.49313394128363 -32.9967432	.270865899862674 .15129650679071	.00972724336184 0.0194545
NONOG	1.1794668861286 -.1283120009229	1.1864257688768 -6.2086848	-.4135921883738 .26855648523554	.49313394128363 147.0032568	-.2611386552649 -.131842320067	
Total network loss F-loss by summing injections = 1.632357556567E-01						

tion at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed
it applying to the composite group. The entry "MVA" is $\sqrt{P^2 + Q^2}$ in units of power, while "P.F." is the
ciated power factor.

Node name	Source Rectangular	node voltage Polar	Injected Rectangular	source current Polar	Injected F and Q	source power MVA and P.F.
RECRE	1.5546456346292 .05547026886898	1.5556349186104 2.0434654	1.0496480231542 -.8348229693001	1.3411526246414 -38.4964972	.79276143126438 .67803907148634	1.0431719270391 0.7599528
LARIO	1.2555232988362 -.0836217696019	1.2583049528123 -3.8104500	-.6192996243911 .36469572184674	.71870359019806 149.5068440	-.4040208045053 -.2030485226295	.45217420649034 -0.8935070
AINOG	1.2063533992447 -.1141540097252	1.2122401846189 -5.4034244	-.1465991001006 .08404681191799	.16898272912901 150.1738974	-.0932589514339 -.0423486527802	.10242382737838 -0.9105201
PATBU	1.2471066979652 -.0534449912241	1.2482515700127 -2.4539194	-.238503096368 .14139046890312	.27726332022687 149.3394914	-.1524976783983 -.0817911189967	.17304718739007 -0.8812491
CHANI	1.280393212628 .00358103066031	1.2803982203692 0.1602456	-.127969970849 .05525756846384	.13939050274654 156.6452622	-.0818270015242 -.0356049399993	.08923767595443 -0.9169558

CHEPE	1.3626813884637	1.3730704490764	-.2481500097241	.26851448230485	-.1604282588402	.18434465040093
	.16858793450787	7.0526702	.10257485014074	.157.5418424	-.0908059683974	-0.8702626
LUJAN	1.5026279441629	1.5556349186104	.74446587665248	.76631843595364	.52274908009457	.5960558588722
	.40262794416288	15.0000000	-.1816989372079	-13.7158152	.28638433294465	0.8770136
NONOG	1.1794668861286	1.1864257688768	-.1430704271519	.17509413618719	-.0908492987115	.10386809757585
	-.1283120009229	-6.2036848	.10093963246268	144.7961099	-.0503486506035	-0.8746603
VUNIO	1.1573965688744	1.166173111915	-.0973487713887	.11137362356051	-.060198732096	.0649404625864
	-.1428037440376	-7.0338096	.0541045352449	150.9355543	-.0243593172106	-0.9269834
CHILE	1.1754649098797	1.1827022669092	-.173172989833	.20706021017532	-.1091940301825	.12244523978112
	-.1306403375443	-6.3417867	.11351231752795	146.7557551	-.0534031541239	-0.8917781

ent card. KOMPAT = 1. IC
ent card. KOMPAT = 1. IC
ent card. KOMPAT = 1. IC
est for flushing of punch buffer. ;PUNCH (Flush punched cards: R-L branches for equivalent impedance loads

esting of 80-column card images now being flushed from punch buffer follows.

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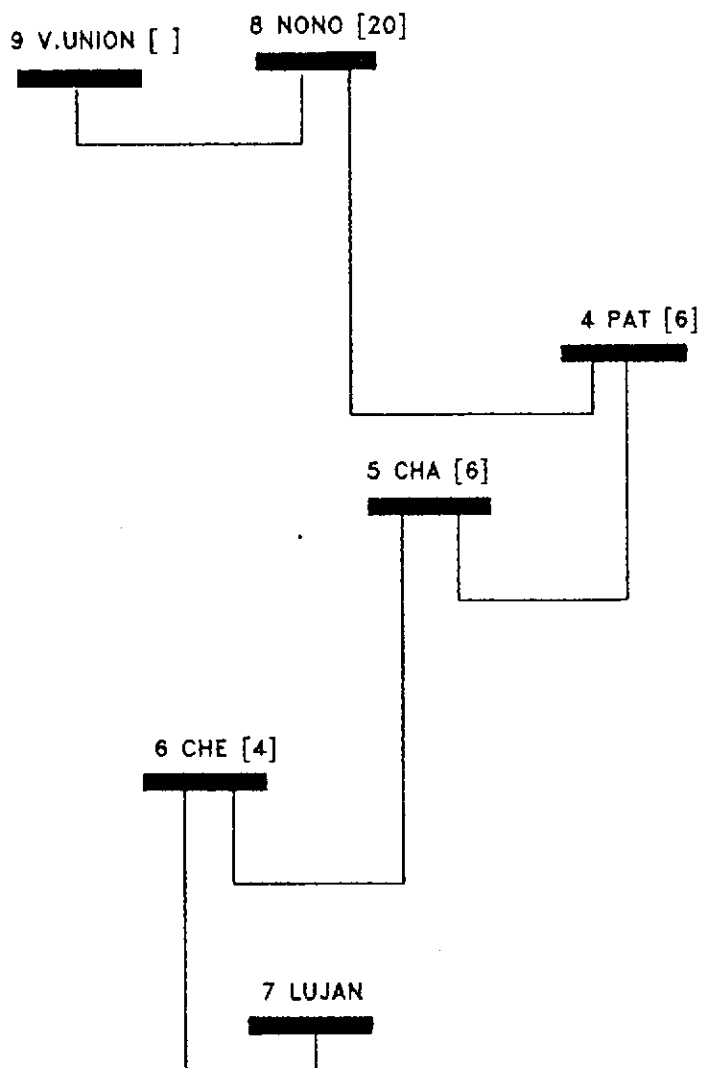
=====

Path: C:\ATF

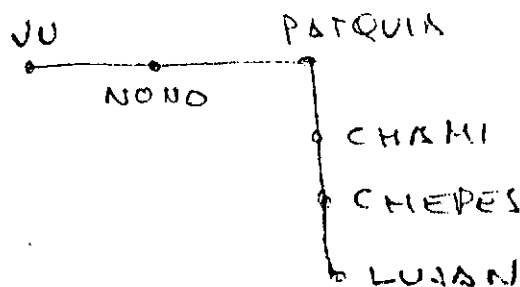
File: AP6152B .SAL 40.060 .a.. 06-04-94 15:27:14

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CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 300
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993



```
ent card. KOMPAT = 1.          :C      The following 2 cards would be used if peak rather than rms input data:
ce. 1.02E+00 5.00E+01 0.00E+00 -1.00E+00 :14V.UNI      1.02      50.      0.0      -1.
ce. 1.10E+00 5.00E+01 0.00E+00 -1.00E+00 :14LUJAN     1.1       50.      0.0      -1.
ent card. KOMPAT = 1.          :C      -----+-----
ent card. KOMPAT = 1.          :C      From bus name : Names of all adjacent busses.
ent card. KOMPAT = 1.          :C      -----+-----
ent card. KOMPAT = 1.          :C      |
ent card. KOMPAT = 1.          :C      |
ent card. KOMPAT = 1.          :C      -----+-----
x card ends electric network sources. :BLANK card terminating all EMTP source cards.
```

of input elements that are connected to each node. Only the physical connections of multi-phase lines are shown (capacitive and inductive coupling are ignored). Repeated entries indicate parallel connections. Switches are included, although sources (including rotating machinery) are omitted -- except that U.M. usage produces extra, internally-defined nodes "UMXXXX".

bus name : Names of all adjacent busses.

```

4.UNI :NONOG $
NONOG :4.UNI $PATQU $
PATQU :NONOG $CHAMI $
CHAMI :PATQU $CHEPE $
CHEPE :CHAMI $LUJAN $
LUJAN :CHEPE $

```

```
ent card. KOMPAT = 1.      :C Next come power constraints of the load flow. There will be one
ent card. KOMPAT = 1.      :C for each non-slack generator. So, 3 of them will apply to nodes
ent card. KOMPAT = 1.      :C that have no Type-14 source as required by the algorithm. The
ent card. KOMPAT = 1.      :C program will define these internally. Yet, this is only possible
ent card. KOMPAT = 1.      :C for TMAX non-positive (no transient continuation). If data is
ent card. KOMPAT = 1.      :C modified to make TMAX > 0, a KILL = 40 error termination will
ent card. KOMPAT = 1.      :C will result. Yet, the transient simulation is possible as a
ent card. KOMPAT = 1.      :C 2nd simulation that replaces the power constraints at load nodes
ent card. KOMPAT = 1.      :C by constant-impedance loads.
ent card. KOMPAT = 1.      :C The following 4 cards would be used if peak rather than RMS input data.
ent card. KOMPAT = 1.      :C Note that average of Vmin & Vmax = 0.5 ( 1.0 + 1.828428 ) = 1.414212
ent card. KOMPAT = 1.      :C (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02
ent card. KOMPAT = 1.      :C 34567890123456789012345678901234567890123456789012345678901234567890
ent card. KOMPAT = 1.      :C NKBUS1 BUS2 BUS3 PK D TITAK          BK O VK          VMIN    VMAX    THMIN THMAX
ent card. KOMPAT = 1.      :C I2 A6 A6 A6 E16.0                      E16.0          EB.0    EB.0    E6.0 E6.0
ent card. KOMPAT = 1.      :C I2 3-B 9-14 15-20 21-36                37-52          53-60    61-68    69-74 75-80
        6.00E-02 1.10E+00 8.50E-01 1.15E+00 : IV.UNI                                0.06         1.1       .85     1.15 -20.   20.
ent card. KOMPAT = 1.      :C IGREEN                               1.0           1.02              -20.   20.
ent card. KOMPAT = 1.      :C BLUE                                 -0.4          -0.08          -0.1       1.15
        -2.00E-01 -1.00E-01 8.50E-01 1.15E+00 : NONOG                    -0.2          -0.1 = -0.06-.89 1.15
ent card. KOMPAT = 1.      :C PATOU                               -0.06         0.1          .85     1.15
        -6.00E-02 1.00E-01 8.50E-01 1.15E+00 : CHAM1                     -0.06         0.1          .85     1.15
        -4.00E-02 -3.00E-02 8.50E-01 1.15E+00 : CHEPE                     -0.04         -0.03        .85     1.15
ent card. KOMPAT = 1.      :C The following load-flow miscellaneous data card has two peculiarities. The
ent card. KOMPAT = 1.      :C use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
ent card. KOMPAT = 1.      :C voltages. The use of KTAPER = 0 ensures constant acceleration factors
ent card. KOMPAT = 1.      :C (this works well for this problem whether RMS or peak values are used).
ent card. KOMPAT = 1.      :C NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE KTAPER
LASTOV, NTOT, NEXT, IOFKOL, IOFKOR, NCURR = 9 7 11 0 0 1
flow iter. 1 1500 20 1 1.00E-05 : 1 1500 20 1 .00001 0.0 0.0 1.414 0
del-V: .1131 .0143 .0144 .0146 .0147 .0149 .015 .0152 .0152 .0116 .0066 .0044 .0036 .0034 .0033 .0031 .0029 .0028 .0026 .0024
ce No. 1 4 4 4 4 4 4 4 3 3 3 3 -3 -3 -3 -3 -3 -3 -3 -3
```

[illegible]

```

ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .3E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .2E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-5      .1E-6      .1E-6      .1E-6      .1E-6      .1E-6      .9E-6      .9E-6      .9E-6      .9E-6      .9E-6
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .9E-6      .9E-6      .9E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .8E-6      .7E-6      .7E-6      .7E-6      .7E-6      .7E-6
ce No.      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1      -1
del-V:      .7E-6      .7E-6      .7E-6      .7E-6
ce No.      -1      -1      -1      -1

```

the load flow iteration loop with counter NEKITE = 724. If no warning on the preceding line, convergence was attained.

Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	VUNI	1.10000000E+00	-9.07134	6.00154633E-02	1.24217047E-01
4	NONOG	1.07170724E+00	-9.07090	-1.99986348E-01	-9.9997926E-02
5	CHAMI	1.08944622E+00	-6.29796	-5.99915993E-02	1.00000316E-01
6	CHEPE	1.08757873E+00	-3.31250	-3.99956362E-02	-2.99997674E-02

nodal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

s K	Bus M	Phasor node voltage		Phasor branch current		Power flow P and Q	Power loss P and Q
		Rectangular	Polar	Rectangular	Polar		
NI		1.5361783750873	1.5556349186104	.05101495002466	.17736235734376	.06001546329388	.0015445586249
		-.2452672010563	-9.0713166	-.1698672442719	-73.2838068	.12421704664077	0.0031945
NONOG		1.4966686696833	1.5156229591696	-.0510149500247	.17736235734376	-.058470904669	
		-.2389473740188	-9.0708805	.16986724427187	106.7161932	-.1210225470815	
OG		1.4966686696833	1.5156229591696	-.1887804963899	.18879158991759	-.1415154430616	.00199240258128
		-.2389473740188	-9.0708805	.00204660851049	179.3788689	.02102275452079	0.0041220
PATQU		1.5182477097282	1.5307843608201	.1887804963899	.18879158991759	.1435078456429	
		-.1955112560353	-7.3378399	-.0020466085105	-0.6211311	-.0169007266402	
QU		1.5182477097282	1.5307843608201	-.1887804963899	.18879158991759	-.1435078456429	.00121540121685
		-.1955112560353	-7.3378399	.00204660851049	179.3788689	.0169007266402	0.0025146
CHAMI		1.5314113160428	1.5407096804915	.1887804963899	.18879158991759	.14472324685975	
		-.1690139066951	-6.2979494	-.0020466085105	-0.6211311	-.0143861648851	
MI		1.5314113160428	1.5407096804915	-.2804258623633	.30441122301208	-.2047148461395	.00531903946073
		-.1690139066951	-6.2979494	-.1184378673125	-157.1032344	.11438648039331	0.0109948
CHEPE		1.5354988991289	1.5380686376194	.28042586236328	.30441122301208	.21003388560027	
		-.0888721823888	-3.3124911	.11843786731245	22.8967656	-.10339163663	
EPE		1.5354988991289	1.5380686376194	-.3300925358352	.33883851853219	-.2500295217959	.00672221576309
		-.0888721823888	-3.3124911	-.076488296013	-166.9537962	.07339186918709	0.0138979

LUJAN 1.5556349186104 1.5556349186104 .3300925358352 .33883851853219 .25675173755894
 0.0 0.0 .07648829601303 13.0462038 .0594939320714
 Total network loss P-loss by summing injections = 1.679361764685E-02

tion at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed
 It applying to the composite group. The entry "MVA" is $\sqrt{P^2 + Q^2}$ in units of power, while "P.F." is the
 iated power factor.

Node name	Source node Rectangular	voltage Polar	Injected Rectangular	source current Polar	Injected P and Q	source power MVA and P.F.
V.UNI	1.5361783750873 -2.452672010563	1.5556349186104 -9.0713166	.05101495002466 -1.1698672442719	.17736235734376 -73.2838068	.06001546329388 .12421704664077	.13795553816551 0.4350348
NONOG	1.4966686696833 -2.389473740188	1.5156229591696 -9.0708805	-.2397954464146 .17191385278235	.2950529255907 144.3625514	-.1999863477306 -.0999997925607	.22359449409771 -0.8944154
CHAMI	1.5314113160428 -1.1690139066951	1.5407096804915 -6.2979494	-.0916453659734 -1.1204844758229	.1513782745929 -127.2580867	-.0599915992798 .1000003155082	.1166149865407 -0.5144416
CHEPE	1.5354988991289 -1.0888721823888	1.5380686376194 -3.3124911	-.0496666734719 .04194957129942	.0650118834212 139.8148239	-.0399956361956 -.0299997674429	.04999636948136 -0.7999708
LUJAN	1.5556349186104 0.0	1.5556349186104 0.0	.3300925358352 .07648829601303	.33883851853219 13.0462038	.25675173755894 -.0594939320714	.26355451559944 0.9741883

ent card. KOMPAR = 1. :C \$UNITS. 0.0, 0.0 ----- 1st of punched cards that are produced
 ent card. KOMPAR = 1. :C \$VINTAGE, 1,
 ent card. KOMPAR = 1. :C Polar V, P, Q = 9.41780959E-01 -3.81708 -5.99988408E-01 -2.99999500E-01
 ent card. KOMPAR = 1. :C RED 1.18261633E+00 1.56852131E+00
 ent card. KOMPAR = 1. :C Polar V, P, Q = 9.15105791E-01 -8.02053 -3.99985812E-01 -9.99988825E-02
 ent card. KOMPAR = 1. :C BLUE 1.97046099E+00 1.30673427E+00
 ent card. KOMPAR = 1. :C Polar V, P, Q = 9.82613423E-01 -1.92907 -5.99992780E-01 -1.99999933E-01
 ent card. KOMPAR = 1. :C YELLOW 1.44830775E+00 1.28060019E+00
 XOPT, COPT = -1.00000000E+00 -1.00000000E+00:\$UNITS, -1, -1
 MOLDAT = 0 (data vintage). :\$VINTAGE, 0, (----- last of punched cards that are produced
 est for flushing of punch buffer. :\$PUNCH (Flush punched cards: R-L branches for equivalent impedance loads

esting of 80-column card images now being flushed from punch buffer follows.

=====

56789012345678901234567890123456789012345678901234567890123456789

=====

=====< End of LUNIT7 punched cards as flushed by \$PUNCH request >=====

nk card ending node names for voltage output. ;BLANK card ending requests for output variables

ective branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be
 mented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

From To (===== Branch voltage $V_{km} = V_k - V_m$ =====) (===== Branch current I_{km} from K to M =====)
 K bus M Magnitude Degrees Real part Imag part Magnitude Degrees Real part Imag part

al List Sizes for the preceding solution follow. 05-Apr-93 10.38.02

Size 1-10: 7 5 5 2 -9999 0 -9999 -9999 0 0

Size 11-20: -9999 -9999 -9999 -9999 -9999 0 0 0 23 0

Size 21-29: 0 -9999 6 -9999 -9999 -9999 -9999 -9999 -9999

nds for overlays 1-5 : 9.836 0.000 9.836 --- (CP: I/O; tot)

nds for overlays 6-11 : 9.176 0.000 9.176

ds for overlays 12-15 :	0.000	0.000	0.000
ds for time-step loop :	0.000	0.000	0.000
ds after DELTA1-loop :	0.000	0.000	0.000
	<hr/>		
Totals :	19.012	0.000	19.012

EN, NOMBRE ORIGEN; 6 CHAMICAL
INO, NOMBRE DESTINO; 7 LUJAN
132.000 132.000
CONSUMIDA 25.000000
MM2); DIST [KM], COSENO FI; 240.000 258.000 .900
SHUNT; CAPACITIVA [MVAR];
MVAR]; 10.000000 -10.000000
DE CARGA [AMP]; 98.41198 -3.92445
10000066282 .0000009935
10137589000
138.96840 .00000
10272920900 1820847000
0001037833 .0007057545
ADOB]; 4.47.4291, NCCNY, 7.85244
ADO]; 19.53
P]; 99.001070
96.800450 20.757750
GRADOS]; 2.283617
135.818600 17.709820
RADOS]; 47.429063
ORRIENTE DE CARGA [AMP]; 98.490
571.924100 -85.723820
DE LINEA [KVA] NL [CMPLX]; 931.1749000000 3036.4770000000
S CIRCUITO PARAMETROS DISTRIBUIDOS
9838346000 .0049426690
30.8815300000 101.3015000000
0000005256 .0003166548
PLX]; 30.8815300000 101.3015000000
PLX]; .0000000912 .0000000137
X]; 121000 394570
X]; .0000000000 .0000012340
CAPACITIVA DE LA LINEA;
NCIA ATENDIDA [BRAZOS PARALELOS DEL CIRC PI]
S CONCENTRADOS BYT [MVAR] .000000 5.760040
REACTIVA IND. DE LA LINEA;
O ATENDIDO [BRAZO SERIE DEL CIRC PI]
S CONCENTRADOS, NLD [MVAR] 3036.477000 .000000
RESISTIVAS [SERIE CIRC PI];
S CONCENTRADOS, PERD [KW] 882.887900
RESISTIVAS [SERIE CIRC PI];
S CONCENTRADOS, PERD [KW] -295.966900

CONSTANTES DEL CUADRIPOLO
PI CON ADMITANCIAS DISTRIBUIDAS

12[MM] VALU2[KV] CPF SEC [MM2]DIST[KM]
25.00 132.00 1 240.0 258.00

NI [MW] DPU [MW] DU[KV],

135.82 17.71 22.14 7.85 -3.36 6.96 3.82 17.71

DELTAU, DEPO(MW) ANGUZ1, I1 (AMP) VALI1(AMP) COR(AMP),

3.63 4.12 -7.43 96.80 20.76 99.00 98.412 -3.924

VALCOR(AMP) VALU1(KV) VALU2 (KV) COR120(AMP)

98.490 136.968 132.000 .000 12.132

A	B	C			
.9838346	.0049427	30.8815300	101.3015000	-.0000003	.0003167

Z2U Y2U WW

.12100000 .39457000 .00000000 .00000123 1

CONCLUSION: POSSIBLE

(DELTAU < 10% DEPO < 5%, O ANGUZ1 < 20)

CASO 320

DO BRISEN, NOMBRE ORIGEN; 7 LUJAN
DO DESTINO, NOMBRE DESTINO; 5 CHAMICAL
[KV]; 132.000 .000
TENCIA CONSUMIDA
A) , N2 30.000000
CCION [MM2], DIST [KM], COSENO FI; 150.000 231.000 .900
TENCIA SHUNT CAPACITIVA [HVAR];
SHUNT [HVAR] .000000 .000000
RRIENTE DE CARGA [AMP]; 118.09440 -57.19572
RD .0000106509 .0000024352
SIH .0293120600
COM [KV]; 146.95970 .00000
M .0577120900 .2524163000
MOD []; .0002498359 .0010927110
GU1 [GRADOS]; 6.380
[MW]; 29.24959 2.12568
GN1 [GRADO]; 4.16
LI1 [AMP]; 115.213800
[AMP]; 115.127100 -4.469234
G I1 [GRADOS]; -25.841930
[KV]; 146.049700 16.329730
GU21 [GRADOS]; -6.379712
L.ARS.CORRIENTE DE CARGA [AMP]; 131.216
[OHM?]; 386.253600 -88.312450
RDIDAS DE LINEA [KVA] ML [CMPLX]; 2766.7670000000 5734.2320000000
NSTANTES CIRCUITO PARAMETROS DISTRIBUIDOS
[]; .9699248000 .0144212700
[]; 43.6893900000 91.6874300000
[]; -.0000031541 .0006469372
RIM [CMPLX]; 43.6893900000 91.6874300000
RIM [CMPLX]; .0000003122 .0000000714
U [CMPLX]; .193000 .400000
U [CMPLX]; .0000000000 .0000028290
TENCIA CAPACITIVA DE LA LINEA;
LA POTENCIA ATENDIDA [BRAZOS PARALELOS DEL CIRC P1]
PARAMETROS CONCENTRADOS BYT [HVAR] .000000 12.750140
TENCIA REACTIVA IND. DE LA LINEA;
CONSUMO ATENDIDO [BRAZO SERIE DEL CIRC P1]
PARAMETROS CONCENTRADOS. NLQ [HVAR] 5734.232000 .000000
RDIDAS RESISTIVAS (SERIE CIRC P1);
PARAMETROS CONCENTRADOS, PERD [KW] 963.835900
RDIDAS RESISTIVAS (SERIE CIRC P1);
PARAMETROS CONCENTRADOS, PERD [KW] -2593.458000

CONSTANTES DEL CUADRIPOLO
P1 CON ADMITANCIAS DISTRIBUIDAS

MM, N2[MM] VALU2[KV] CPF SEC [MM2]DIST[KM]
1 30.00 132.00 1 150.0 231.00

UI[KV] N1 [MW] DPU [MW] DU[KV],

05 16.33 29.25 2.13 2.25 -10.95 14.05 16.33

TAU, DEPO(MW) ANGU21, 11 (AMP) VALI1(AMP) COR(AMP),

18 -2.30 -6.38 115.13 -4.47 115.21 118.094 -57.196

VALCOR(AMP) VALU1(KV) VALU2 (KV) COR120(AMP)
131.216 146.960 132.000 .000 24.902

A.	B.	C			
.9699248	.0144213	43.6873900	91.6874300	-.0000032	.0006469

Z2U	Y2U	WH
-----	-----	----

.19300000	.40000000	.00000000	.00000283	1
-----------	-----------	-----------	-----------	---

CONCLUSION: DUDOSA A COMPENSAR

TAU >10%<20% O DEPO >5%<10% , O ANGU21 >20<25 }

CASO 325

ORIGEN, NOMBRE ORIGEN; 7 LUJAN
DESTINO, NOMBRE DESTINO; 6 CHAMICAL
[KV]; 132.000 .000
ENCIA CONSUMIDA
], N2 30.000000
CION [MM2], DIST [KM], COSENO FI; 150.000 231.000 .900
ENCIA SHUNT CAPACITIVA [HVAR];
SHUNT [HVAR] .000000 -10.000000
RIENTE DE CARGA [AMP]; 118.09440 -13.45706
O .0000105509 .0000024352
IH .0293120600
OM [KV]; 140.48320 .00000
 .0577120900 .2524163000
MOD []; .0002498359 .0010927110
GU1 [GRADOS]; 8.036
[MW]; 26.29506 13.03921
GU1 [GRADO]; 26.38
I1 [AMP]; 120.623000
[AMP]; 114.496400 37.953970
S I1 [GRADOS]; -6.500915
[KV]; 139.103600 19.639530
GU21 [GRADOS]; -8.036264
ABS. CORRIENTE DE CARGA [AMP]; 118.859
[OHM?]; 386.253600 -88.312450
RDIDAS DE LINEA [KVA] NL [CMPLX]; 2062.0980000000 4273.7790000000
CONSTANTES CIRCUITO PARAMETROS DISTRIBUIDOS
[]: .9699248000 .0144212700
[]: 43.6893900000 71.6874300000
[]: -.0000031541 .0006463372
ZIM [CMPLX]; 43.6893900000 71.6874300000
ZIM [CMPLX]; .0000003122 .0000000714
U [CMPLX]; .193000 .400000
U [CMPLX]; .0000000000 .0000028290
TENCIA CAPACITIVA DE LA LINEA;
LA POTENCIA ATENDIDA (BRAIOS PARALELOS DEL CIRC P1)
PARAMETROS CONCENTRADOS QYT [HVAR] .000000 12.141860
TENCIA REACTIVA IND. DE LA LINEA;
CONSUMO ATENDIDO (BRAIO SERIE DEL CIRC P1)
PARAMETROS CONCENTRADOS, NLO [HVAR] 4273.779000 .000000
RDIDAS RESISTIVAS (SERIE CIRC P1);
PARAMETROS CONCENTRADOS, PERD [KW] 1668.504000
RDIDAS RESISTIVAS (SERIE CIRC P1);
PARAMETROS CONCENTRADOS, PERD [KW] -1211.752000

CONSTANTES DEL CUADRIPOLO
P1 CON ADMITANCIAS DISTRIBUIDAS

NW, N2[NW] VALU2[KV] CPF SEC [MM2]DIST[KM]
1 30.00 132.00 1 150.0 231.00

U1[KV] N1 [MW] DFU [MW] DU[KV],

10 19.64 26.30 13.04 -1.70 9.96 7.10 19.64

ELTAU, DEPO{MN} ANGUZ1, I1 {AMP} VALI1{AMP} CDR{AMP},

0.04 7.41 -8.04 114.50 37.95 120.62 118.094 -13.457

VALCOR{AMP} VALU1{KV} VALU2 {KV} CDR120{ AMP}
118.859 140.483 132.000 .000 24.902

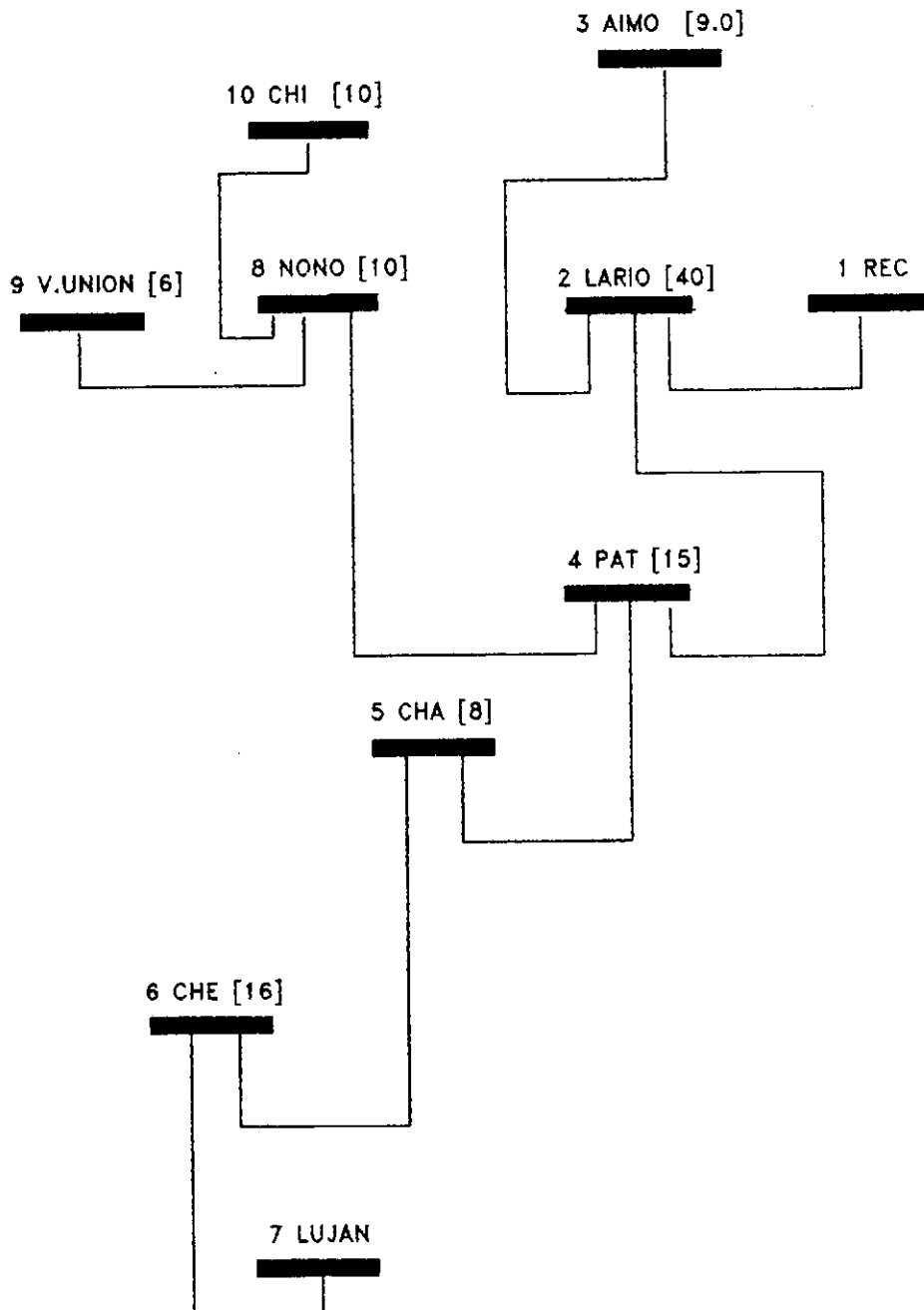
A,	B,	C			
.9599248	.0144213	43.6893900	91.6874300	-.0000032	.0006469

ZZU	YZU	WW
-----	-----	----

.19300000	.40000000	.00000000	.00000283	1
-----------	-----------	-----------	-----------	---

CONCLUSION: DUDOSA A COMPENSAR
TAU >10%<20% O DEPO >5%<10% , O ANGUZ1 >20<25]

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 330
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

DATA: C:\ARIV\BIN\PROBE3.DAT (-06-04-94 16:21; RED 132 KV LA RIOJA;
CASO: 125; LINEA EN 150 MHZ (CON AUTOTRANSFORMADOR, NO CONSIDERADO)

CASO 330

ASE

IN NEW DATA CASE

NTED NUMBER WIDTH, 13, 2, { Request maximum precision for 8 output columns
SOURCE { An EMTP load flow will satisfy requested phasor power injections.
ER FREQUENCY, 50.0,

ISCELANEA CARD SIGUE 11 B-1, 11 B-2

4567890123456789012345678901234567890123456789012345678901234567890

ELTAT TMAX XOPT COPT EPSILN TOLNAT

00200 .000 50.50, { T-max = 0 means that no transient solution follows

OUT IPLOT IDOURL KSSOUT MAXOUT IPUN MENSAB ICAT NERERG IFRSUP

1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72

1 1 1 0 1

ARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.

ASE 100 MVA =1; UR=132 KV

IGUE FORMATO RULE BOOK 4A-2

4567890123456789012345678901234567890123456789012345678901234567890

US1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION

A6 A6 A6 A6 E6.2 E6.2 E6.2 11

3-8 9-14 15-20 21-26 27-32 33-38 39-44 80

AS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)

N 80 1=CORRIENTE RAMA; 2=VOLT RAMA; 3=I y V DE RAMA; 4=CONSUMO POT Y ENERG

ECRE LARIO	0.11	0.22	4
ARIO AIMGG	.16	.30	4
ARIO PATOU	.08	.16	4
ATOU CHAMI	.08	.16	4
ATOU NONOG	.14	.26	4
HAMI CHEPE	0.1218	.25	4
HEPE LUJAN	.134	.28	4
ONOG VUNIO	.11	.21	4
ONOG CHILE	.01	.02	4
ARIO NONOG	.08	.16	4

NK card ending branch cards.

NK card ending switch cards.

SOURCE CARD SIGUE FORMATO RULE BOOK VII-4

4567890123456789012345678901234567890123456789012345678901234567890

AME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 TSTART TSTOP

2 A6 I2 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6

1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

UJAN 1.10 50. 15.0 -1.

ECRE 1.10 50. 15.0 -1.

NK card terminating all EMTP source cards.

Next come power constraints of the load flow. There will be one
for each non-slack generator. So, 3 of them will apply to nodes
that have no type-14 source as required by the algorithm. The

program will define these internally. Yet, this is only possible for TMAX non-positive (no transient continuation). If data is modified to make TMAX > 0, a KILL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data. Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02

ALORES DE POTENCIA EN PU I=100 MVA

ARA RESTRICCIONE DE POTENCIASIGUE RULE BOOK 10-4:10-6

KBUS1	BUS2	BUS3	PX or QX	QX or VX	VMIN	VMAX	TMIN	TMAX
-2	3-8	9-14	15-20	21-36	37-52	53-60	61-68	69-74
ARIO			-0.4000		-0.200	.65	1.25	
HAMI			-0.080		-.034	.65	1.25	
AIQU			-0.150		-.080	.65	1.25	
ONGG			-0.10		-.051	.65	1.25	
UNIO			-.0600		-.02	.65	1.25	
UJAN				1.0	1.20			-20. 40.
ECRE			0.8		1.10			-20. 15.
HEPE			-.16		-.09		1.5	
IMOG			-0.090		-0.04	.65	1.15	
HILE			-.1000		-.04		1.15	

The following load-flow miscellaneous data card has two peculiarities. The use of VSCALE = 1.414 is the special flag requesting RMS rather than peak voltages. The use of KTAPER = 0 ensures constant acceleration factors (this works well for this problem whether RMS or peak values are used).

NNOUT	NITERA	NFLOUT	NPRINT	RALCHK	CFITEV	CFITEA	VSCALE	KTAPER
10-16	17-24	25-32	33-40	41-48	50-56	57-64		
1	2500	20	1	.01	0.2	2.5	1.414	2

UNCH (Flush punched cards; R-L branches for equivalent impedance loads
 NK card ending requests for output variables
 NK card ending plot cards
 IN. NEW DATA CASE

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Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
 Date (dd-mth-yy) and time of day (hh:mm:ss) = 19-Apr-94 10:50:55 Name of disk plot file, if any, is C:\44191030.pl4
 For more information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
 Total length of "LARCORN" tables = 444863 INTEGER words. "VARDIM" List Sizes follow: 752 700 1500 150 7500
 120 2100 5250 225 480 150 150 15000 .. 60 64800 120 12 15 4800 1980 300 450 12000 9 1200 252 4

Descriptive interpretation of input data cards.

Input data card images are shown below, all 80 columns, character by character
 0 1 2 3 4 5 6 7 8
 01234567890123456789012345678901234567890123456789012345678901234567890

```

:ent card.  KOMPAT = 1.      :C data:C:\RIV\EMIN\PROBE4.DAT
:ent card.  KOMPAT = 1.      :C DATA:C:\RIV\EMIN\PROBE3.DAT(-06-04-94 15:21; RED 132 KV LA RIOJA;
:ent card.  KOMPAT = 1.      :C CASO 125; LINEA EN 150 MM2 (CON AUTOTRANSFORMADOR, NO CONSIDERADO)
:se all of 0 cards in the punch buffer.      :ERASE
:er card preceding new EMTP data case.        :BEGIN NEW DATA CASE
:h of time-step loop numbers. M=13 S=2       :PRINTED NUMBER WIDTH, 13, 2, ( Request maximum precision for 2 output columns
:aration of desired EMTP load flow usage.     :FIX SOURCE ( An EMTP load flow will satisfy requested phasor power injections.
:power frequency STATFR = 5.00000000E+01 Hz. :POWER FREQUENCY, 50.0.
:ent card.  KOMPAT = 1.      :C MISCELANEA CARD SIGUE II B-1,11 B-2
:ent card.  KOMPAT = 1.      :C 34567890123456789012345678901234567890123456789012345678901234567890
:ent card.  KOMPAT = 1.      :C DELTAT TMAX XOPT COPT EPSILN TOLMAT
:ent card.  2.000E-04 0.000E+00 5.000E+01 : .000200 .000 50.50.( T-max = 0 means that no transient solution follows
:ent card.  KOMPAT = 1.      :C IOUT IFLOT IDOUEL KSSQUT MAXOUT IPUN MENSAY ICAT NERERG IPASUF
:ent card.  KOMPAT = 1.      :C 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
:ent card.  1 1 0 1 0 1 0 0 0 0 : 1 1 1 0 1
:ent card.  KOMPAT = 1.      :C
:ent card.  KOMPAT = 1.      :C CARGA DE VALORES PASIVOS DE LOS DISTINTOS RAMOS (R-L) VALORES EN P.U.
:ent card.  KOMPAT = 1.      :C BASE 100 MVA =1; UR=132 KV
:ent card.  KOMPAT = 1.      :C SIGUE FORMATO RULE BOOK 4A-2
:ent card.  KOMPAT = 1.      :C 34567890123456789012345678901234567890123456789012345678901234567890
:ent card.  KOMPAT = 1.      :C BUS1 BUS2 BUS3 BUS4 RES13 XL XC OUTPUT OPTION
:ent card.  KOMPAT = 1.      :C A6 A5 A5 A6 E6.2 E6.2 E6.2 11
:ent card.  KOMPAT = 1.      :C 3-8 9-14 15-20 21-26 27-32 33-38 39-44 80
:ent card.  KOMPAT = 1.      :C LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)
:ent card.  KOMPAT = 1.      :C EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG
:es R-L-C. 1.100E-01 7.003E-04 0.000E+00 : RECRE LARIO 0.11 0.22 4
:es R-L-C. 1.600E-01 9.549E-04 0.000E+00 : LARIO AIMOG .16 .30 4
:es R-L-C. 8.000E-02 5.093E-04 0.000E+00 : LARIO PATQU .08 .16 4
:es R-L-C. 8.000E-02 5.093E-04 0.000E+00 : PATQU CHAMI .08 .16 4
:es R-L-C. 1.400E-01 8.276E-04 0.000E+00 : PATQU NONOG .14 .26 4
:es R-L-C. 1.218E-01 7.958E-04 0.000E+00 : CHAMI CHEPE 0.1218 .25 4
:es R-L-C. 1.340E-01 8.913E-04 0.000E+00 : CHEPE LUJAN .134 .28 4
:es R-L-C. 1.100E-01 6.685E-04 0.000E+00 : NONOG VUNIO .11 .21 4
:es R-L-C. 1.000E-02 6.366E-05 0.000E+00 : NONOG CHILE .01 .02 4
:ent card.  KOMPAT = 1.      :C LARIO NONOG .08 .16 4
:ent card.  KOMPAT = 1.      :C
:ent card.  KOMPAT = 1.      :C
:k card ending branches. IBR, NTOT = 9 11 :BLANK card ending branch cards.
:k card ending switches. KSWTCH = 0. :BLANK card ending switch cards.
:ent card.  KOMPAT = 1.      :C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
:ent card.  KOMPAT = 1.      :C 34567890123456789012345678901234567890123456789012345678901234567890
:ent card.  KOMPAT = 1.      :C NAME IV AMPLITUDE FREQUENCY PHASE AI TIME-1 TSTART TSTOP

```

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ent card. KOMPAT = 1. IC 12 A6 12 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6
ent card. KOMPAT = 1. IC 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80
ent card. KOMPAT = 1. IC
ce, 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 14LUJAN 1.10 50. 15.0 -1.
ce, 1.10E+00 5.00E+01 1.50E+01 -1.00E+00 14RECRE 1.10 50. 15.0 -1.
ent card. KOMPAT = 1. IC
ent card. KOMPAT = 1. IC
k card ends electric network sources. BLANK card terminating all ENTP source cards.
ent card. KOMPAT = 1. IC Next come power constraints of the load flow. There will be one
ent card. KOMPAT = 1. IC for each non-slack generator. So, 3 of them will apply to nodes
ent card. KOMPAT = 1. IC that have no Type-14 source as required by the algorithm. The
ent card. KOMPAT = 1. IC program will define these internally. Yet, this is only possible
ent card. KOMPAT = 1. IC for THAX non-positive (no transient continuation). If data is
ent card. KOMPAT = 1. IC modified to make THAX > 0, a KILL = 40 error termination will
ent card. KOMPAT = 1. IC will result. Yet, the transient simulation is possible as a
ent card. KOMPAT = 1. IC 2nd simulation that replaces the power constraints at load nodes
ent card. KOMPAT = 1. IC by constant-impedance loads. Branch cards for these will be
ent card. KOMPAT = 1. IC punched by the present subcase, and the transient continuation
ent card. KOMPAT = 1. IC will be illustrated by the following (4th of 4) subcase.
ent card. KOMPAT = 1. IC The following 4 cards would be used if peak rather than RMS input data.
ent card. KOMPAT = 1. IC Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212
ent card. KOMPAT = 1. IC (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 + 1.02
ent card. KOMPAT = 1. IC
ent card. KOMPAT = 1. IC VALORES DE POTENCIA EN PU 1=100 MVA
ent card. KOMPAT = 1. IC PARA RESTRICCIONE DE POTENCIASIGUE RULE 800X 10-4;10-6
ent card. KOMPAT = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
ent card. KOMPAT = 1. IC KXBUS1 BUS2 BUS3 PK or QX QX or VX VMIN VMAX THMIN THMAX
ent card. KOMPAT = 1. IC 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
-4.000E-01 -2.000E-01 6.500E-01 1.250E+00 LARIO -0.4000 -0.200 .65 1.25
-8.000E-02 -3.400E-02 6.500E-01 1.250E+00 CHAMI -0.080 -0.034 .65 1.25
-1.500E-01 -8.000E-02 6.500E-01 1.250E+00 PATQU -0.150 -0.080 .65 1.25
-1.000E-01 -6.100E-02 6.500E-01 1.250E+00 NONDG -0.10 -0.061 .65 1.25
-6.000E-02 -2.000E-02 6.500E-01 1.250E+00 VUNIO -0.0600 -0.02 .65 1.25
ent card. KOMPAT = 1. IC LUJAN 1.0 1.20 -20. 40.
8.000E-01 1.100E+00 0.000E+00 1.000E+19 IRECRE 0.8 1.10 -20. 15.
-1.600E-01 -9.000E-02 0.000E+00 1.500E+00 CHEPE -0.16 -0.09 1.5
-9.000E-02 -4.000E-02 6.500E-01 1.150E+00 AIMDG -0.090 -0.04 .65 1.15
-1.000E-01 -4.000E-02 0.000E+00 1.150E+00 CHILE -0.1000 -0.04 1.15
ent card. KOMPAT = 1. IC The following load-flow miscellaneous data card has two peculiarities. The
ent card. KOMPAT = 1. IC use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
ent card. KOMPAT = 1. IC voltages. The use of KTAPE2 = 0 ensures constant acceleration factors
ent card. KOMPAT = 1. IC (this works well for this problem whether RMS or peak values are used).
ent card. KOMPAT = 1. IC NNNOUT NITERA NFLOUT NPRINT RALCHK CFITEV CFITEA VSCALE KTAPE2
ent card. KOMPAT = 1. IC 10-16 17-24 25-32 33-40 41-48 50-56 57-64
LASTOV, NIOT, NEXT, IOFKOL, IOFKOR, NCURF = 9 11 19 0 0 0
d flow iter. 1 2500 20 1 1.00E-02 1 2500 20 1 .01 0.2 2.5 1.414 2
del-V: .0232 .0227 .0223 .0218 .0213 .0209 .0204 .0189 .0152 .0155 .0158 .0151 .0136 .0135 .0133 .0132 .013 .0127 .0125 .0127
rce No. 1 -4 -4 -4 -4 -4 -4 -4 -9 -9 -9 -9 -5 -5 -5 -5 -5 -5 7 7
del-V: .0129 .0131 .0117 .0115 .0113 .0111 .0108 .0106 .0113 .0095 .0105 .0113 .0117 .0116 .0117 .0116 .0117 .0116 .0117 .0116
rce No. 7 7 -5 -5 -5 4 -5 -5 -5 -5 -4 -9 -4 -9 -4 4 -4 4 -4 4
del-V: .0117 .0116 .0117 .0116 .0117 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0116 .0115 .0116 .0115
rce No. -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4

[illegible]

del-V:	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0105	.0104	.0105
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105	.0104	.0105
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0105	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104	.0104
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0104
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0104	.0103	.0104	.0103	.0104	.0103	.0104	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103	.0103
ce No.	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4	-9	-4
del-V:	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102	.0102
ce No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9
del-V:	.0101	.0102	.0101	.0102	.0101	.0102	.01	.0102	.01	.0102	.01	.0102	.0099	.0102	.0099	.0103	.0099	.0103	.0099
ce No.	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9	4	9
del-V:	.0099	.0103	.0099	.0103	.0099	.0103	.0099	.0103	.0099	.0103	.0099	.0103	.0099	.0103	.0099	.0103	.0099	.0103	.0099
ce No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4
del-V:	.0098	.0103	.0098	.0103	.0098	.0103	.0098	.0103	.0098	.0103	.0098	.0103	.0098	.0103	.0098	.0103	.0098	.0103	.0098
ce No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4
del-V:	.0097	.0101	.0095	.0099	.0093	.0096	.009	.0093	.0087	.0083	.0083	.0085	.0078	.008	.0074	.0075	.0069	.007	.0066
ce No.	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4	4	-4
del-V:	.0058	.006	.0053	.0055	.0048	.005	.0043	.0045	.0039	.004	.0035	.0036	.0031	.0032	.0027	.0028	.0024	.0024	.0021
ce No.	-4	4	-4	4	-4	4	-4	4	9	4	9	4	9	4	9	4	9	4	9
del-V:	.0018	.0018	.0015	.0015	.0013	.0013	.0011	.0011	.9E-3	.9E-3	.8E-3	.8E-3	.7E-3						
ce No.	9	4	9	4	9	4	9	4	9	4	9	4	9						

t the load flow iteration loop with counter NEKITE = 1013. If no warning on the preceding line, convergence was attained.

w	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
3	3	LARIO	8.94035941E-01	2.66405	-4.01991738E-01	-2.00845588E-01
4	6	CHANI	8.72401752E-01	4.16587	-8.03964213E-02	-3.51836953E-02
5	5	FATOU	8.37248967E-01	1.49566	-1.51426441E-01	-8.22549298E-02
6	7	NONOG	7.37211215E-01	-3.12345	-9.20615844E-02	-5.24217800E-02
7	10	VUNID	7.21038652E-01	-4.21627	-6.13102487E-02	-2.44235159E-02
2	2	RECRE	1.10000000E+00	8.68003	7.96576835E-01	6.56314773E-01

8 8 CREPE 9.52496096E-01 8.94420 -1.59991038E-01 -9.06375138E-02
 9 4 AIMOG 8.62404631E-01 1.10328 -7.18567171E-02 -4.09956888E-02
 0 11 CHILE 7.35020471E-01 -3.28589 -1.06309446E-01 -5.43081631E-02

usoidal steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P"
 printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage		Phasor branch current		Power flow	
		Rectangular	Polar	Rectangular	Polar	P and Q	P and Q
CRE		1.5378254999571	1.5556349126104	1.1397068834456	1.3269512280458	.77657687493801	.09684377583858
		.23471840933694	8.6780842	-.6796085501514	-30.8976734	.65631477260225	0.1936880
LARIO		1.2629438617448	1.2643091260419	-1.1397068834456	1.3269512280458	-.6997328590993	
		.05873983549556	2.6629220	.67960855015144	149.1923266	-.4526268205249	
RIO		1.2629438617448	1.2643091260419	.15190336548417	.16495953570083	.09403364879853	.00217697187347
		.05873983549556	2.6629220	-.0643196390963	-22.9490000	.04507743684176	0.0040817
AIMOG		1.219343431539	1.2195690936314	-.1519033654842	.16495953570083	-.0918566717125	
		.02345976810539	1.1022254	.06431963909428	157.0510000	-.040995688779	
RIO		1.2629438617448	1.2643091260419	.33782143720916	.47048229811195	.20370727221168	.00885414371347
		.05873983549556	2.6629220	-.3274603325575	-44.1077471	.21670379630844	0.0177083
PATOU		1.1835244935588	1.1839274151816	-.3378214372092	.47048229811195	-.1948531284987	
		.03088523214669	1.4948503	.32746033255746	135.8922529	-.1989955058815	
TOU		1.1835244935588	1.1839274151816	-.4109336399075	.42019509425698	-.2418201534142	.00706255658951
		.03088523214669	1.4948503	.08773517441724	167.5481792	-.0582642543874	0.0141251
CHAMI		1.2304368126582	1.2336759680804	.41093363990748	.42019509425698	.24858271010375	
		.08961580057851	4.1656401	-.0877351744172	-11.0518208	.07233936774645	
TOU		1.1835244935588	1.1839274151816	.48941367216477	.56532543589208	.28524684043621	.02237157853829
		.03088523214669	1.4948503	-.2829633131952	-30.0351260	.17500483341517	0.0415472
NONOE		1.041436118024	1.0429810458496	-.4894136721648	.56532543589208	-.2628752618979	
		-.0567474587683	-3.1189409	.28296331319515	149.9648740	-.1334576161298	
AMI		1.2304368126582	1.2336759680804	-.5450668150947	.56157338943481	-.3292791314003	.01920576850783
		.08961580057851	4.1656401	.13515486970084	166.0738070	-.1075730630466	0.0394206
CHEPE		1.3306146681619	1.346993838181	.54506681509473	.56157338943481	.34848483990813	
		.20942064122265	8.9442068	-.1351548697006	-13.9261930	.14699364701175	
EPE		1.3306146681619	1.346993838181	-.800654072475	.83335662252474	-.5084758782673	.04653037844049
		.20942064122265	8.9442068	.23116296531907	163.8956375	-.2376311608223	0.0972277
LUJAN		1.5026279441629	1.5556349126104	.80065407247496	.83335662252474	.55500625670784	
		.40262794416288	15.0000000	-.2311629653191	-16.1043625	.33485881726511	
NOG		1.041436118024	1.0429810458496	.11642656572465	.12946744438888	.06223214873085	.92150005361E-3

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	-0.0567474587683	-3.1189409	-0.0566275017121	-25.9373413	.02618350690922	0.0017600
VUNIO	1.0167374204348	1.0194975159326	-0.1164265657247	.12946744438888	-0.0613102486772	
	-0.0749680123821	-4.2170100	.05662750171208	154.0626587	-0.0244235158978	
NOG	1.041436118024	1.0429810458496	.20218245813133	.23327368512418	.10858152875101	.27208306086E-3
	-0.0567474587683	-3.1189409	-0.11635663193556	-29.9205604	.05485232918143	0.0005442
CHILE	1.037087160804	1.0387998954674	-0.2021824581313	.23327368512418	-0.1083094456902	
	-0.0596275416115	-3.2906100	.11635663193558	150.0794396	-0.0543081630597	
Total network loss P-loss by summing injections = 2.042392567662E-01						

ation at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed
ult applying to the composite group. The entry "MVA" is $\text{SQRT}(P^2 + Q^2)$ in units of power, while "P.F." is the
ociated power factor.

Node name	Source node voltage Rectangular	Polar	Injected source current Rectangular	Polar	Injected source power P and Q	MVA and P.F.
RECRE	1.5378254999571	1.5556349186104	1.1397068834456	1.3269512280458	.79557683498801	1.0321258328205
	.23471840933694	8.6780842	-0.6796085501514	-30.8076734	.65631477260224	0.7717827
LARIO	1.2629438617448	1.2643091260419	-0.6499820807523	.71086003960011	-0.4019919378891	.44737341770246
	.05873983549556	2.6629220	.28782857849971	156.1150204	-0.2008458884747	-0.8945610
AIMUG	1.2193434315539	1.2195690936314	-0.1519033654842	.16495953570083	-0.091856717125	.1005877572026
	.02345996810539	1.1022254	.06431963909428	157.0510000	-0.040995688779	-0.9131814
PATBU	1.1835244933588	1.1839274151816	-0.2593414049519	.2911070548666	-0.1514264414782	.17232481150466
	.03088523214669	1.4948503	.13223219377654	152.9840156	-0.0822549298338	-0.8787269
CHANI	1.2304368126582	1.2336759600804	-0.1341331751872	.14226853547634	-0.0803964212966	.08775805930093
	.03961580057851	4.1656401	.0474196952834	160.5301249	-0.0351835953001	-0.9161144
NONOG	1.041436118024	1.0429810458496	-0.1708046483088	.20314932394352	-0.0220615844161	.10594044717513
	-0.0567474587683	-3.1189409	.1099791795515	147.2229734	-0.0524217800391	-0.8689937
CHEPE	1.3306146681619	1.346993838181	-0.2555872573802	.273024542046	-0.1599910383892	.18388118790408
	.20942064122265	8.9442068	.09600809561843	159.4119510	-0.0906375138105	-0.8700783
LUJAN	1.5026277441629	1.5556349186104	.80065407247496	.83335662252474	.55500625670784	.64819933082735
	.40262774416288	15.0000000	-0.2311629653191	-16.1043625	.33485881726511	0.8562278
VUNIO	1.0167374204348	1.0194975159326	-0.1164265657247	.12946744438888	-0.0613102486772	.06599586897431
	-0.0749680123821	-4.2170100	.05662750171208	154.0626587	-0.0244235158978	-0.9290013
CHILE	1.037087160804	1.0387998954674	-0.2021824581313	.23327368512418	-0.1083094456902	.12116233986115
	-0.0596275416115	-3.2906100	.11635663193558	150.0794396	-0.0543081630597	-0.8939201

ment card. KOMPAT = 1. IC
ment card. KOMPAT = 1. IC
ment card. KOMPAT = 1. IC
quest for flushing of punch buffer. %PUNCH { Flush punched cards: R-L branches for equivalent impedance loads

sting of 80-column card images now being flushed from punch buffer follows.

=====

56789012345678901234567890123456789012345678901234567890123456789

=====

=====(End of LUN117 punched cards as flushed by \$PUNCH request)=====

nk card ending node names for voltage output. (ELANK card ending requests for output variables

active branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be
sented to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

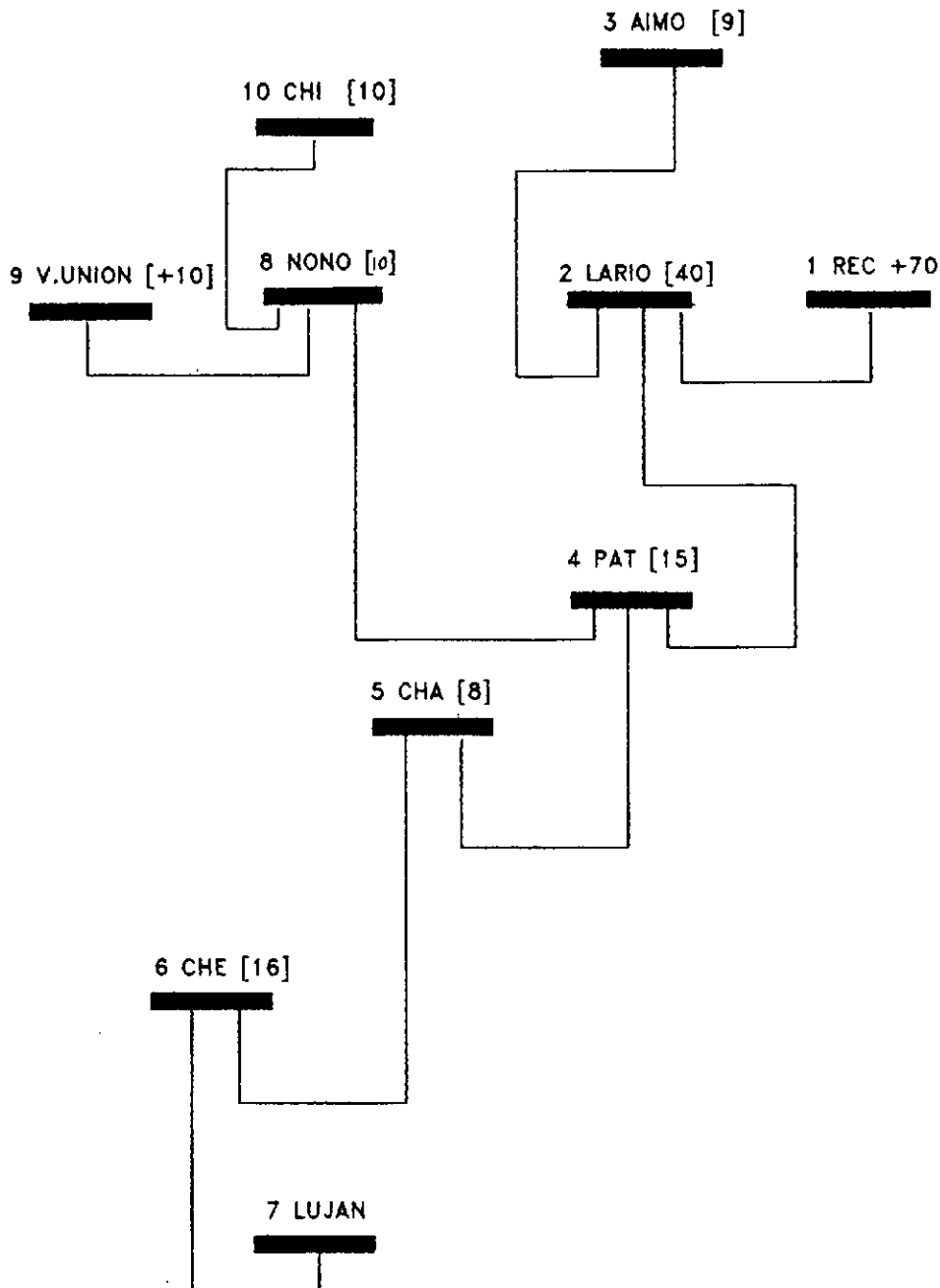
From To		Branch voltage $V_{km} = V_k - V_m$				Branch current I_{km} from K to M			
K	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
DE	LARIO	3.2638685E-01	32.627275	2.7458164E-01	1.7597857E-01	1.3269512E+00	-30.807673	1.1397067E+00	-6.7960855E-01
DO	AIMOG	5.6086242E-02	38.978513	4.3600430E-02	3.5279867E-02	1.6495954E-01	-22.949000	1.5190337E-01	-6.4319619E-02
DO	PATOU	8.4162432E-02	19.327202	7.9419368E-02	2.7854603E-02	4.7048230E-01	-44.107747	3.3762144E-01	-3.2746033E-01
DU	CHAMI	7.5166784E-02	-128.616872	-4.6712319E-02	-5.8730568E-02	4.2019509E-01	167.748179	-4.1093364E-01	3.7735174E-02
DU	NONDS	1.6693890E-01	31.664118	1.4208838E-01	8.7632691E-02	5.6532644E-01	-30.035126	4.9941367E-01	-2.8296331E-01
MI	CHEPE	1.5616915E-01	-129.901537	-1.0017786E-01	-1.1930484E-01	5.6157339E-01	166.073807	-5.4506582E-01	1.3515487E-01
PE	LUJAN	2.5868442E-01	-131.678807	-1.7201328E-01	-1.9320730E-01	8.3335662E-01	163.895637	-8.0065407E-01	2.3116297E-01
OG	VUNIO	3.0692290E-02	36.416683	2.4698698E-02	1.8220554E-02	1.2946744E-01	-25.937341	1.1642657E-01	-5.6627502E-02
OS	CHILE	5.2161582E-03	33.514388	4.3489572E-03	2.8600828E-03	2.3327369E-01	-27.920560	2.0218246E-01	-1.1635663E-01

ual List Sizes for the preceding solution follow. 17-Apr-94 10:51:47

Size 1-10: 11 9 9 2 -9999 0 -9999 -9999 0 0
 Size 11-20: -9999 -9999 -9999 -9999 -9999 0 0 9 23 0
 Size 21-29: 0 -9999 9 -9999 -9999 -9999 -9999 -9999 -9999
 onds for overlays 1-5 : 40.328 0.000 40.328 --- (CF: I/O; tot)
 onds for overlays 6-11 : 11.539 0.000 11.539
 onds for overlays 12-15 : 0.000 0.000 0.000
 onds for time-step loop : 0.000 0.000 0.000
 onds after DELIAT-loop : 0.441 0.000 0.441

Totals : 52.309 0.000 52.309

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
CASO 340
CARGA MW [] AÑO 1993



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

C DATA:C:\RIVENIN\PROBE5.DAT(-20-04-94 12:00; RED 132 KV LA RIOJA;

C CASO 130; LINEA EN 150 MM2 (ALIMENTACION VILLA UNION)

*ERASE

BEGIN NEW DATA CASE

PRINTED NUMBER WIDTH, 13, 2, (Request maximum precision for 8 output columns

FIX SOURCE (An EMTP load flow will satisfy requested phasor power injections.

POWER FREQUENCY, 50.0,

C MISCELANEA CARD SIGUE II B-1,II B-2

C 34567890123456789012345678901234567890123456789012345678901234567890

C DELTAT TMAX XOPT COPT EPSILN TOLMAI

.000200 .000 50.50.(T-max = 0 means that no transient solution follows

C IOUT IFLOT IDOUBL KSSOUT MAXOUT IPUN MENSAR ICAT NERERG IPRSUP

C 1-8 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72

1 1 1 0 1

C

C CARGA DE VALORES PASIVOS DE LOS DISTINTOS TRAMOS (R-L) VALORES EN P.U.

C BASE 100 MVA =1; UB=132 KV

C SIGUE FORMATO RULE BOOK 4A-2

C 34567890123456789012345678901234567890123456789012345678901234567890

C BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION

C A6 A6 A6 A6 E6.2 E6.2 E6.2 11

C 3-8 9-14 15-20 21-26 27-32 33-38 39-44 80

C LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)

C EN 80 1=CORRIENTE RAMA;2=VOLT RAMA;;3=I y V DE RAMA; 4=CONSUMO POT Y ENERG

RECRE LARIO 0.11 0.22 4

LARIO ALMOG .15 .30 4

LARIO PATOU .08 .16 4

PATOU CHAMI .08 .16 4

PATOU NONOG .14 .26 4

CHAMI CHEPE 0.1218 .25 4

CHEPE LUJAN .134 .28 4

NONOG VUNIO .11 .21 4

NONOG CHILE .01 .02 4

C LARIO NONOG .08 .16 4

C

C

BLANK card ending branch cards.

BLANK card ending switch cards.

C SOURCE CARD SIGUE FORMATO RULE BOOK VII-4

C 34567890123456789012345678901234567890123456789012345678901234567890

C NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 ISTART ISTOP

C I2 A6 I2 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6 E10.6

C 1-2 9-10 10-20 21-30 31-40 41-50 51-60 61-70 71-80

C

14LUJAN 1.10 50. 15.0 -1.

14RECRE 1.10 50. 15.0 -1.

14VUNIO 1.1 50. 15.0 -1.

C

C

BLANK card terminating all EMTP source cards.

C Next come power constraints of the load flow. There will be one

C for each non-slack generator. So, 3 of them will apply to nodes

caso 340

that have no Type-14 source as required by the algorithm. The program will define these internally. Yet, this is only possible for TMAX non-positive (no transient continuation). If data is modified to make TMAX > 0, a FILL = 40 error termination will result. Yet, the transient simulation is possible as a 2nd simulation that replaces the power constraints at load nodes by constant-impedance loads. Branch cards for these will be punched by the present subcase, and the transient continuation will be illustrated by the following (4th of 4) subcase.

The following 4 cards would be used if peak rather than RMS input data. Note that average of Vmin & Vmax = 0.5 (1.0 + 1.828428) = 1.414212 (power constraints RED, BLUE, and YELLOW), and 1.4708 = 1.414 * 1.02

C VALORES DE POTENCIA EN PU 1=100 MVA
C PARA RESTRICCIONE DE POTENCIASIGUE RULE 800K 10-4;10-6
C 34567890123456789012345678901234567890123456789012345678901234567890
C NKBUS1 BUS2 BUS3 PK or GK GK or VK VMIN VMAX THMIN THMAX
C 1-2 3-8 9-14 15-20 21-36 37-52 53-60 61-68 69-74 75-80
C LARIO -0.4000 -0.200 .65 1.25
C CHAM1 -0.080 -0.034 .65 1.25
C PATQU -0.150 -0.080 .65 1.25
C NONOB -0.10 -0.061 .65 1.25
C VUNIO -0.0600 -0.02 .65 1.25
C 1VUNIO 0.1 1.1 -20. 15.
C LUJAN 1.0 1.20 -20. 40.
C 1RECRE 0.7 1.10 -20. 15.
C CHEPE -.16 -.07 1.5
C AIMOB -0.090 -0.04 .65 1.15
C CHILE -.1000 -.04 1.15

C The following load-flow miscellaneous data card has two peculiarities. The
C use of VSCALE = 1.414 is the special flag requesting RMS rather than peak
C voltages. The use of KTAPER = 0 ensures constant acceleration factors
C (this works well for this problem whether RMS or peak values are used).
C HNNOUT NITERA NFLOUT NPRINT RALCHX CFITEV CFITEA VSCALE KTAPER
C 10-16 17-24 25-32 33-40 41-48 50-56 57-64
C 1 2500 20 1 .01 0.2 2.5 1.414 2

C \$PUNCH { Flush punched cards: R-L branches for equivalent impedance loads
C BLANK card ending requests for output variables
C BLANK card ending plot cards
C BEGIN NEW DATA CASE

Alternative Transients Program (ATP), Salford 386 translation. Copyright 1987. Use licensed only by LEC (K.U. Leuven, Belgium).
Date (dd-mth-yy) and time of day (hh.mm.ss) = 20-Apr-94 12.03.58 Name of disk plot file, if any, is 0:44201203.pl4
For more information, consult the copyrighted ATP EMTP Rule Book published by LEC in July, 1987. Last major program update: Oct, 1990
Total length of "LABCOM" tables = 444863 INTEGER words. "VARDIM" List Sizes follow: 752 900 1500 150 7500
120 2100 5250 225 480 150 150 15000 60 64800 120 12 15 4800 1980 300 450 12000 9 1200 252 4

Descriptive interpretation of input data cards. Input data card images are shown below, all 80 columns, character by character
0 1 2 3 4 5 6 7 8
012345678901234567890123456789012345678901234567890123456789012345678901234567890

Blank card. KOMPAN = 1. IC DATA: C:\RIV\EMIN\PROBES.DAT
Blank card. KOMPAN = 1. IC DATA: C:\RIV\EMIN\PROBES.DAT (-20-04-94 12:00; RED 132 KV LA RIOJA;
Blank card. KOMPAN = 1. IC CASO 130; LINEA EN 150 MM2 (ALIMENTACION VILLA UNION)
Delete all of 0 cards in the punch buffer. IERASE
Blank card preceding new EMTP data case. IBEGIN NEW DATA CASE
Number of time-step loop numbers. N=13 S=2 IPRINTED NUMBER WIDTH, 13, 2. (Request maximum precision for 8 output columns
Duration of desired EMTP load flow usage. IFIX SOURCE (An EMTP load flow will satisfy requested phasor power injections.
Power frequency STATFR = 5.00000000E+01 Hz. IPOWER FREQUENCY, 50.0,
Blank card. KOMPAN = 1. IC MISCELANEA CARD SIGUE II R-1, II R-2
Blank card. KOMPAN = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
Blank card. KOMPAN = 1. IC DELTAT TMAX KOPT COPT EPSILN TOLMAT
IC DATA. 2.000E-04 0.000E+00 5.000E+01 1.000200 .000 50.50. (T-max = 0 means that no transient solution follows
Blank card. KOMPAN = 1. IC ICUT IPLOT IDOURL KSGOUT MAXOUT IPUN MEMSAV ICAT NEREAG IPRSUP
Blank card. KOMPAN = 1. IC 1-6 8-16 17-24 25-32 33-40 41-48 49-56 57-64 65-72
IC DATA. 1 1 0 1 0 1 0 0 0 0 1 1 1 0 1
Blank card. KOMPAN = 1. IC
Blank card. KOMPAN = 1. IC CARGA DE VALORES PASIVOS DE LOS DISTINTOS RAMOS (R-L) VALORES EN P.U.
Blank card. KOMPAN = 1. IC BASE 100 MVA =1; UB=132 KV
Blank card. KOMPAN = 1. IC SIGUE FORMATO RULE BOOK 4A-2
Blank card. KOMPAN = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
Blank card. KOMPAN = 1. IC BUS1 BUS2 BUS3 BUS4 RESIS XL XC OUTPUT OPTION
Blank card. KOMPAN = 1. IC A6 A6 A6 A6 E6.2 E6.2 E6.2 11
Blank card. KOMPAN = 1. IC 3-8 9-14 15-20 21-26 27-32 33-39 39-44 80
Blank card. KOMPAN = 1. IC LAS OPCIONES DE SALIDA SON: (IV-A.2 RULE BOOK ACTUALIZ)
Blank card. KOMPAN = 1. IC EN 60 1=CORRIENTE RAMA; 2=VOLT RAMA; 3=I y V DE RAMA; 4=CONSUMO POT Y ENERS
IC R-L-C. 1.100E-01 7.003E-04 0.000E+00 1 RECRE LARIO 0.11 0.22 4
IC R-L-C. 1.600E-01 9.547E-04 0.000E+00 1 LARIO AINOG .16 .30 4
IC R-L-C. 8.000E-02 5.093E-04 0.000E+00 1 LARIO PATOU .06 .16 4
IC R-L-C. 8.000E-02 5.093E-04 0.000E+00 1 PATOU CHAMI .08 .16 4
IC R-L-C. 1.400E-01 8.276E-04 0.000E+00 1 PATOU NONOG .14 .26 4
IC R-L-C. 1.218E-01 7.958E-04 0.000E+00 1 CHAMI CHEPE 0.1218 .25 4
IC R-L-C. 1.340E-01 8.913E-04 0.000E+00 1 CHEPE LUJAN .134 .23 4
IC R-L-C. 1.100E-01 6.685E-04 0.000E+00 1 NONOG YUNIO .11 .21 4
IC R-L-C. 1.000E-02 6.366E-05 0.000E+00 1 NONOG CHILE .01 .02 4
Blank card. KOMPAN = 1. IC LARIO NONOG .06 .16 4
Blank card. KOMPAN = 1. IC
Blank card. KOMPAN = 1. IC
Blank card ending branches. IRR, NTOT = 9 11 IBLANK card ending branch cards.
Blank card ending switches. KSWTCH = 0. IBLANK card ending switch cards.
Blank card. KOMPAN = 1. IC SOURCE CARD SIGUE FORMATO RULE BOOK VII-4
Blank card. KOMPAN = 1. IC 34567890123456789012345678901234567890123456789012345678901234567890
Blank card. KOMPAN = 1. IC NAME IV AMPLITUDE FREQUENCY PHASE A1 TIME-1 ISTART ISTOP

d flow iter.	1	2500	20	1	1.00E-02	1	2500	20	1	.01	0.2	2.5	1.414	2						
del-V:	.0263	.0264	.0265	.0266	.0267	.0268	.0269	.027	.027	.0271	.0271	.0271	.0271	.0271	.0256	.023				
rce No.	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5	-5				
del-V:	.0208	.0189	.0171	.0156	.0132	.0111	.0109	.011	.0111	.0108	.0113	.0114	.0112	.0116	.0116	.0115	.0119	.0119	.0118	.0122
rce No.	-5	-5	-5	-5	-5	-5	4	4	4	9	4	4	7	4	4	9	4	4	4	4

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del-V:	.012	.0124	.0123	.0123	.0128	.0128	.013	.013	.0133	.0133	.0131	.0134	.0136	.0137	.0137	.0139	.0143	.0199	.0258	.0144
rce No.	9	4	9	9	4	9	4	9	4	9	9	4	4	4	9	9	4	-4	-9	-9
del-V:	.018	.014	.0149	.0238	.0258	.0145	.0211	.0136	.0145	.022	.0258	.0146	.0221	.0135	.0144	.0201	.0258	.0144	.0187	.0138
rce No.	-4	-4	-9	-4	-9	-7	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4
del-V:	.0148	.0239	.0257	.0146	.0223	.0136	.0144	.0203	.0257	.0144	.0182	.0139	.0148	.0239	.0257	.0145	.0208	.0137	.0146	.0233
rce No.	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4
del-V:	.0256	.0146	.0218	.0137	.0145	.0215	.0256	.0144	.0189	.0139	.0147	.0239	.0256	.0145	.0212	.0137	.0145	.0224	.0256	.0145
rce No.	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9
del-V:	.0195	.0139	.0146	.0239	.0255	.0145	.0212	.0138	.0145	.0223	.0255	.0144	.0188	.0139	.0146	.024	.0255	.0145	.0204	.0139
rce No.	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4
del-V:	.0145	.0233	.0255	.0145	.0194	.0139	.0146	.024	.0255	.0145	.02	.0139	.0145	.0237	.0254	.0144	.0193	.0139	.0146	.024
rce No.	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4
del-V:	.0254	.0144	.0193	.014	.0145	.024	.0254	.0144	.019	.014	.0145	.024	.0254	.0144	.0187	.014	.0145	.0241	.0253	.0144
rce No.	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9
del-V:	.0184	.014	.0145	.0241	.0253	.0144	.0181	.014	.0145	.0241	.0253	.0144	.0178	.0141	.0145	.0241	.0253	.0144	.0175	.0141
rce No.	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4
del-V:	.0145	.0241	.0253	.0143	.0172	.0141	.0145	.0241	.0253	.0143	.0169	.0141	.0145	.0241	.0252	.0143	.0166	.0141	.0145	.0241
rce No.	4	-4	-9	-9	-4	-4	4	-4	-9	-9	-4	-4	-9	-4	-9	-9	-4	-4	-9	-9
del-V:	.0252	.0143	.0163	.0141	.0145	.0242	.0252	.0143	.016	.0141	.0145	.0242	.0252	.0143	.0158	.0142	.0145	.0242	.0252	.0143
rce No.	-9	-9	-4	-4	-9	-4	-9	-9	-4	-4	-9	-4	-9	-9	-4	-4	4	-4	-9	-9
del-V:	.0155	.0142	.0145	.0242	.0251	.0143	.015	.0142	.0145	.0242	.0252	.0141	.0138	.0144	.0185	.0142	.0138	.0144	.0173	.0142
rce No.	-4	-4	-9	-4	-9	-9	-4	-4	4	-4	-9	-9	4	-4	4	-9	4	-4	4	-9
del-V:	.0138	.0143	.0165	.0142	.0138	.0143	.0163	.0142	.014	.0143	.0159	.0143	.0143	.0143	.0155	.0143	.0144	.0143	.0155	.0143
rce No.	4	-4	4	-9	4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9
del-V:	.0145	.0143	.0154	.0143	.0145	.0143	.0153	.0143	.0145	.0143	.0153	.0143	.0145	.0143	.0152	.0143	.0144	.0143	.0152	.0143
rce No.	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9
del-V:	.0145	.0143	.0152	.0143	.0145	.0143	.0151	.0143	.0145	.0143	.0151	.0143	.0144	.0143	.015	.0142	.0144	.0143	.015	.0142
rce No.	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9
del-V:	.0144	.0143	.015	.0142	.0144	.0143	.0149	.0142	.0143	.0143	.0149	.0142	.0143	.0143	.0147	.0142	.0143	.0143	.0149	.0142
rce No.	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9
del-V:	.0143	.0143	.0148	.0142	.0143	.0143	.0148	.0142	.0142	.0143	.0147	.0142	.0142	.0143	.0147	.0142	.0142	.0143	.0146	.0142
rce No.	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9
del-V:	.0142	.0143	.0146	.0142	.0141	.0143	.0145	.0142	.0141	.0142	.0145	.0142	.0141	.0142	.0145	.0142	.014	.0142	.0145	.0142
rce No.	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	-4	-4	4	-9	4	-4	4	-9
del-V:	.014	.0142	.0144	.0142	.014	.0142	.0144	.0142	.014	.0142	.0143	.0142	.014	.0142	.0143	.0142	.014	.0142	.0142	.0142
rce No.	4	-4	4	-9	4	-4	4	-9	4	-4	4	-9	4	-4	4	-9	4	-4	4	-9
del-V:	.014	.0142	.0142	.0142	.014	.0142	.0142	.0142	.0141	.0142	.0141	.0142	.0141	.0142	.0141	.0142	.0141	.0142	.014	.0142
rce No.	4	-4	4	-9	4	-4	4	-9	4	-4	4	-9	4	-4	4	-9	4	-4	-4	-9
del-V:	.0141	.0142	.014	.0142	.0141	.0142	.014	.0142	.0141	.0142	.014	.0142	.0141	.0142	.014	.0142	.0141	.0142	.014	.0141
rce No.	4	-4	9	-9	4	-4	-4	-9	4	-4	9	-9	4	-4	-4	-9	4	-4	-4	-9
del-V:	.0141	.0142	.0141	.0141	.0141	.0142	.014	.0141	.0141	.0142	.0141	.0141	.0141	.0142	.014	.0141	.0141	.0142	.0141	.0141
rce No.	4	-4	-4	-9	4	-4	9	-9	4	-4	-4	-9	4	-4	9	-9	4	-4	-4	-9
del-V:	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.014	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141
rce No.	4	-4	-4	-9	4	-4	9	-9	4	-4	9	-9	4	-4	-4	-9	4	-4	-4	-9
del-V:	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.0141
rce No.	4	-4	-4	-9	4	-4	9	-9	4	-4	-4	-9	4	-4	9	-9	4	-4	9	-9
del-V:	.0141	.0141	.0141	.0141	.0141	.0141	.0141	.014	.0141	.0141	.014	.0141	.0141	.0141	.0141	.014	.0141	.0141	.0141	.014
rce No.	4	-4	9	-9	4	-4	9	-9	4	-4	-4	-9	4	-4	9	-9	4	-4	-4	-9
del-V:	.0141	.0141	.0141	.014	.0141	.0141	.0141	.014	.0141	.0141	.0141	.0141	.0141	.0141	.014	.0141	.0141	.0141	.0141	.014
rce No.	4	-4	-4	-9	4	-4	-4	-9	4	-4	9	-9	4	-4	-4	-9	4	-4	-4	-9

[illegible]

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del-V: .0139 .0139 .0139 .014 .0139 .0139 .0139 .014 .0139 .0139 .0139 .014 .0139 .0139 .0139 .014 .0139 .0139 .0139 .014
rce No. -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4
del-V: .0139 .0139 .0139 .014 .0139 .0139 .0139 .014 .0139 .0139 .0139 .014 .0139 .0139 .0139 .014 .0139 .0139 .0139 .014
rce No. -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4 -9 -4
del-V: .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138 .0138
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138 .0139 .0138
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139 .0139
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .014 .0139 .014 .0139 .014 .0139 .014 .0139 .014 .0139 .014 .0139 .014 .0139 .014 .0139 .014 .0139 .014 .014
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014 .014
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .014 .014 .0141 .014 .0141 .014 .0141 .014 .0141 .014 .0141 .014 .0141 .014 .0141 .014 .0141 .0141 .0141 .0141
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141 .0141
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0142 .0141 .0142 .0141 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0142
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0142 .0142 .0142 .0142 .0142 .0142 .0142 .0141 .0142 .014 .0142 .014 .0142 .0139 .0142 .0138 .0142 .0138 .0142 .0138
rce No. 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9 4 9
del-V: .0142 .0138 .0143 .0138 .0143 .0138 .0143 .0139 .0143 .0139 .0143 .0139 .0143 .0139 .0143 .0139 .0143 .0139 .0143 .0139
rce No. 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4
del-V: .0141 .0137 .0138 .0134 .0134 .0128 .0128 .0122 .012 .0114 .0112 .0105 .0103 .0096 .0093 .0086 .0083 .0076 .0073 .0066
rce No. 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4
del-V: .0063 .0057 .0054 .0048 .0046 .004 .0038 .0033 .0031 .0027 .0025 .0021 .002 .0017 .0016 .0013 .0012 1.E-3 .7E-3 .7E-3
rce No. 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4 -4 4
del-V: .7E-3 .5E-3 .5E-3
rce No. 4 -4 4

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At the load flow iteration loop with counter NEKITE = 1443. If no warning on the preceding line, convergence was attained.

W	Node	Name	Voltage magnit	Degrees	Real power P	Reactive power
4	3	LARIO	9.84131935E-01	7.40470	-4.02451874E-01	-2.00752871E-01
5	6	CHAMI	9.90567338E-01	7.08011	-8.02959822E-02	-3.49401326E-02
6	5	FATOU	9.85846721E-01	5.61556	-1.50582043E-01	-8.02383390E-02
7	7	NONOG	1.02435925E+00	2.03351	-1.11764035E-01	-7.52374662E-02
3	10	VUNIO	1.10000000E+00	1.06563	9.29445117E-02	3.50169746E-01
2	2	RECRE	1.10000000E+00	13.98075	6.95472923E-01	2.64054969E-01
9	8	CHEPE	1.01816078E+00	10.18702	-1.59939836E-01	-9.05338393E-02
9	4	AIMOG	9.55469302E-01	6.11408	-9.25553934E-02	-4.11532710E-02
0	11	CHILE	1.02227222E+00	1.94247	-9.14793632E-02	-2.72257733E-02

Harmonic steady-state phasor solution, branch by branch. All flows are away from a bus, and the real part, magnitude, or "P" printed above the imaginary part, the angle, or "Q". The first solution frequency = 5.00000000E+01 Hertz.

Bus K	Bus M	Phasor node voltage		Phasor branch current		Power flow P and Q	Power loss P and Q
		Rectangular	Polar	Rectangular	Polar		
CRE		1.5095608070938 .37580069671061	1.5556349186104 13.9774481	.94966174314211 -.113427953047	.95641169321592 -8.8111622	.89547272278074 .26405496864384	.05030778256061 0.1000196
	LARI0	1.3801438676778 .17935218805452	1.3917486493073 7.4041767	-.7496617431421 .11342795304699	.95641169321592 173.1668378	-.8451631398001 -.1634354016826	
R10		1.3801438676778 .17935218805452	1.3917486493073 7.4041767	.14270509033718 -.0459775206376	.14972891832303 -17.8582133	.09435363781323 .04452507308307	.00175929445836 0.0033718
	AIMOG	1.3435177790326 .14389707385538	1.351201831867 6.1133423	-.1427050903372 .04597752063761	.14972891832303 162.1417867	-.0925553733549 -.0411532709717	
R10		1.3801438676778 .17935218805452	1.3917486493073 7.4041767	.19626171551641 .14410460123523	.24348485934894 36.2878428	.14835757770817 -.0818425416159	.00237137906929 0.0047425
	FATOU	1.3874996512741 .13642191315307	1.3941901666108 5.6153940	-.1962617155164 -.1441046052352	.24348485934894 -143.7121572	-.1459681826387 .08658533175852	
TOU		1.3874996512741 .13642191315307	1.3941901666108 5.6153940	-.1878551733759 -.0772878406819	.20313290349281 -157.6366326	-.1355963713152 .04080464492305	.00165051905925 0.0033010
	CHANI	1.3901620106351 .17266176814776	1.4008434966094 7.0800285	.18785517337586 .07728784068185	.20313290349261 22.3633674	.13724669037842 -.0375036068046	
TOU		1.3874996512741 .13642191315307	1.3941901666108 5.6153940	.15787712512962 .31480694817857	.35217694595297 63.3660256	.13100051110307 -.2076283156816	.00868200208825 0.0181277
	NONOG	1.4472466602824 .05130098787432	1.4481556120787 2.0301268	-.1578771251296 -.3148069481786	.35217694595297 -116.6339744	-.1223185090148 .22373203384546	
ANI		1.3901620106351 .17266176814776	1.4008434966094 7.0800285	-.3077690516479 -.0419137457674	.31060996641529 -172.1448427	-.217542872552 .00256347423529	.0058755437707 0.0109798
	CHEFE	1.417169844684 .25470912529421	1.4398774625605 10.1890352	.30776905164791 .04191374576741	.31060996641529 7.7551375	.22341641632231 .00949634467927	
EFE		1.417169844684 .25470912529421	1.4398774625605 10.1890352	-.5486804621757 .04262470552636	.55033363779916 175.5578509	-.3833582519511 -.1000801839496	.02029205671134 0.0428019
	LUNAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.54868046217574 -.0426247055264	.55033363779916 -4.4421491	.40565034866142 .14246158006189	
NNOG		1.4472466602824 .05130098787432	1.4481556120787 2.0301268	-.1278300663421 .44789961979376	.46578385586623 105.9136913	-.0810120086641 -.5275895123073	.01193250303121 0.0127802
	VUN10	1.5556366899367 .02887624782884	1.5556349186104 1.0636057	.12783006634206 -.4478996197936	.46578385586623 -74.6713097	.09294451170519 .35016974594782	
NNOG		1.4472466602824	1.4481556120787	.12772060454661	.13199922466181	.09156648294789	.37113768654E-4

.05130088787432 2.0301268 -0.0333376794667 -14.6289836 .02740001284272 0.0001742

CHILE 1.4453027006471 1.4461357918352 -.1277206045966 .13199982466181 -.0714753631791
.04907985257706 1.9449132 .03333767946674 165.3710364 -.0272257733056

Total network loss P-loss by summing injections = 1.029792569272E-01

ution at nodes with known voltage. Nodes that are shorted together by switches are shown as a group of names, with the printed
ult applying to the composite group. The entry "MVA" is $\text{SERF}(P_{112} + Q_{112})$ in units of power, while "P.F." is the
ociated power factor.

Node name	Source node Rectangular	voltage Polar	Injected source Rectangular	current Polar	Injected source P and Q	power MVA and P.F.
RECRE	1.5095608090936 .37580065671081	1.5556349186104 13.3794481	.94956174319211 -.113427953047	.75641169321592 -6.2111612	.69547252278074 .26405456884384	.74391371026679 0.9348537
LAGJO	1.3801438676778 .17935218805452	1.3917486493073 7.4041967	-.61064747372895 .21155497764461	.64627770771194 150.8930499	-.4024518742787 -.2007528712195	.44974351139794 -0.3948475
AINOG	1.3435177790326 .14389707385538	1.331201831867 6.1133423	-.1427050903372 .04597758063781	.14991811892303 161.1417867	-.0925553933547 -.0411532707737	.10121211474511 -0.3137473
PATQU	1.3874996512741 .13642191315307	1.3941301666106 5.6153940	-.2262357637605 .07341450226149	.24476660828087 157.5642650	-.150582042855 -.080238339	.17061577866394 -0.8828287
CHAMI	1.3901620106351 .17266176814776	1.4002434966094 7.0800285	-.111913878272 .03537409491444	.12502253711785 163.5641601	-.0302959821736 -.0349401325793	.08756563907745 -0.3169496
NONOG	1.4472466602824 .05130088787432	1.4481556126787 2.0301268	-.1379858068753 .09975499214845	.186848390099721 147.7311026	-.11117640747512 -.0762374662191	.13529707663307 -0.8261077
CHEPE	1.417169844684 .25470912527421	1.4398774625605 10.1890352	-.2409114105272 .08453845129377	.25531364526664 160.6634695	-.159936836288 -.0705838392494	.18381016168615 -0.6701355
LUJAN	1.5026279441629 .40262794416288	1.5556349186104 15.0000000	.54868046217574 -.0426247055264	.55033363979916 -4.4421491	.40365034866242 .14248158006189	.42805911347877 0.7427781
VUNIO	1.5553662899367 .02827624782884	1.5556349186104 1.0636057	.12783008634206 -.4478976177936	.4653836596623 -74.0713087	.09294411170527 .35016974574782	.76227481535525 0.2015439
CHILE	1.4453027006471 .04907985257706	1.4461357918352 1.9449132	-.1277206045966 .03333767946674	.13199982466182 165.3710364	-.0714753631791 -.0272257733056	.07544483547971 -0.5694527

ment card. KOMPAR = 1.

IC

ment card. KOMPAR = 1.

IC

ment card. KOMPAR = 1.

IC

uest for flushing of punch buffer.

!#PUNCH

(Flush punched cards; R-L branches for equivalent impedance loads

isting of 80-column card images now being flushed from punch buffer follows.

=====

4567890123456789012345678901234567890123456789012345678901234567890123456789

=====

=====(End of LUNIT7 punched cards as flushed by !#PUNCH request)=====

card ending node names for voltage output. (BLANK card ending requests for output variables)

Active branch outputs follow (for column-80 keyed branches only). Any request for branch current output automatically will be added to include branch voltage. But the converse is not true (a request for voltage only will not produce current output).

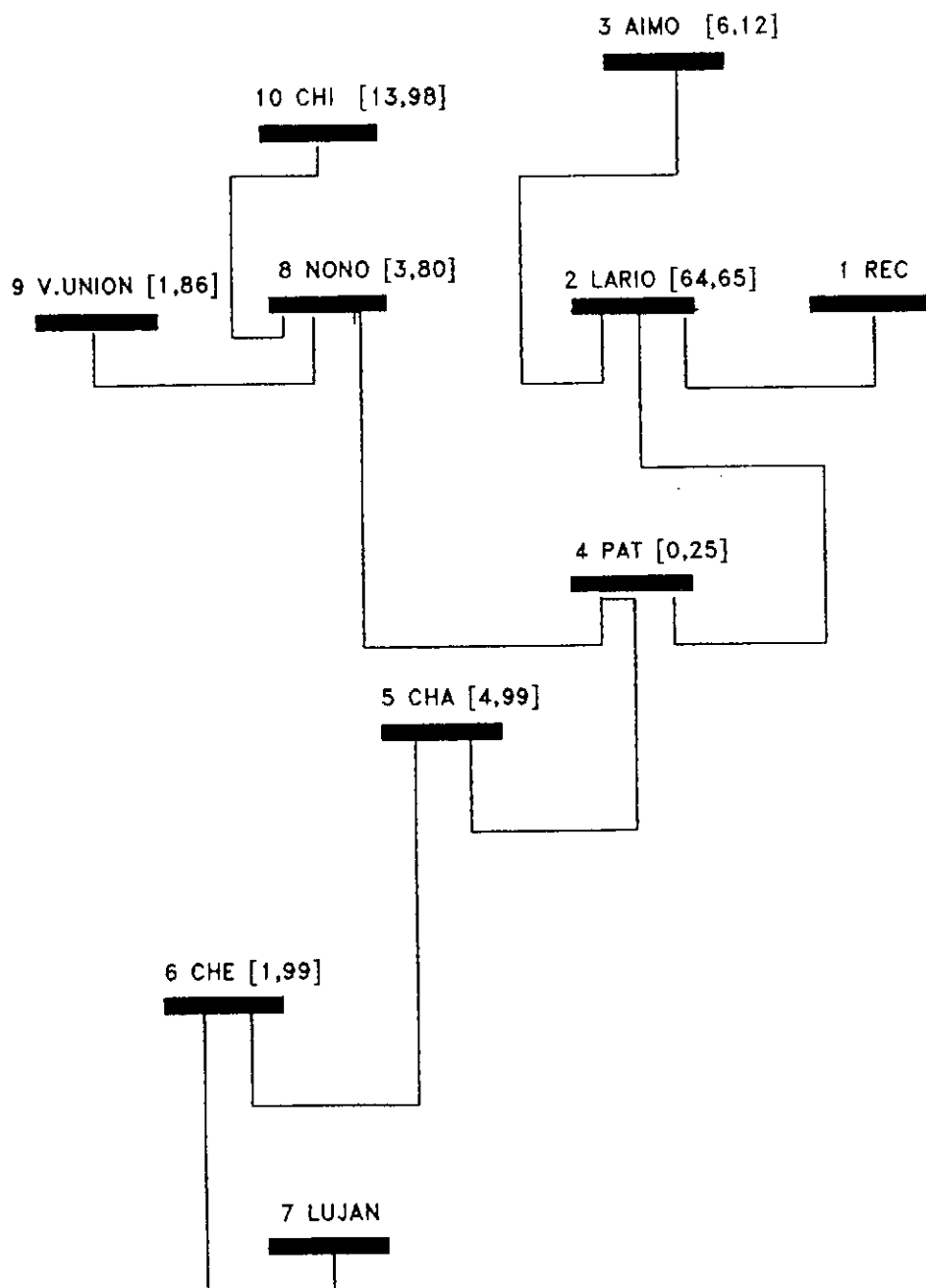
K	To	bus M	Magnitude	Degrees	Real part	Imag part	Magnitude	Degrees	Real part	Imag part
LARIO	2.3524617E-01	56.623787	1.2941694E-01	1.4644851E-01	9.5641169E-01	-6.811162	9.4966174E-01	-1.1342755E-01		
AINOG	5.0975832E-02	44.069300	3.6626089E-02	3.5455114E-02	1.4992892E-01	-17.858213	1.4270509E-01	-4.5977581E-02		
PAIGU	4.3555896E-02	99.722792	-7.3557836E-03	4.2930275E-02	2.4348486E-01	36.287843	1.9626192E-01	1.4410481E-01		
CHAMI	3.6337518E-02	-94.201684	-2.6623594E-03	-3.6239655E-02	2.0313290E-01	-157.635633	-1.8785517E-01	-7.7257941E-02		
MONOG	1.0399661E-01	125.065270	-5.9747009E-02	8.5121025E-02	3.5217695E-01	63.366026	1.5787713E-01	3.1480695E-01		
CHEPE	8.6378191E-02	-108.220187	-2.7007834E-02	-8.2047357E-02	3.1060997E-01	-172.244843	-3.0776905E-01	-4.1513746E-02		
LUJAN	1.7083051E-01	-120.016594	-8.5458099E-02	-1.4791882E-01	5.5033364E-01	175.557851	-5.4668046E-01	6.2654706E-02		
VUNIO	1.1042123E-01	168.282716	-1.0812023E-01	2.2424640E-02	4.6578386E-01	105.928591	-1.2783005E-01	4.6789582E-01		
CHILE	2.9516058E-03	48.805985	1.9439596E-03	2.2210353E-03	1.3199982E-01	-14.628964	1.2772050E-01	-3.3197679E-02		

al List Sizes for the preceding solution follow. 20-Apr-94 12:04:37

size 1-10:	11	9	9	3	-9999	0	-9999	-9999	0	0
size 11-20:	-9999	-9999	-9999	-9999	-9999	0	0	9	23	0
size 21-29:	0	-9999	9	-9999	-9999	-9999	-9999	-9999	-9999	-9999
nds for overlays 1-5 :	26.594	0.000	26.594	---	(CP: 1/0; tot)					
nds for overlays 6-11 :	12.359	0.000	12.359							
nds for overlays 12-15 :	0.000	0.000	0.000							
nds for time-step loop :	0.000	0.000	0.000							
nds after DELTAI-loop :	0.332	0.000	0.332							

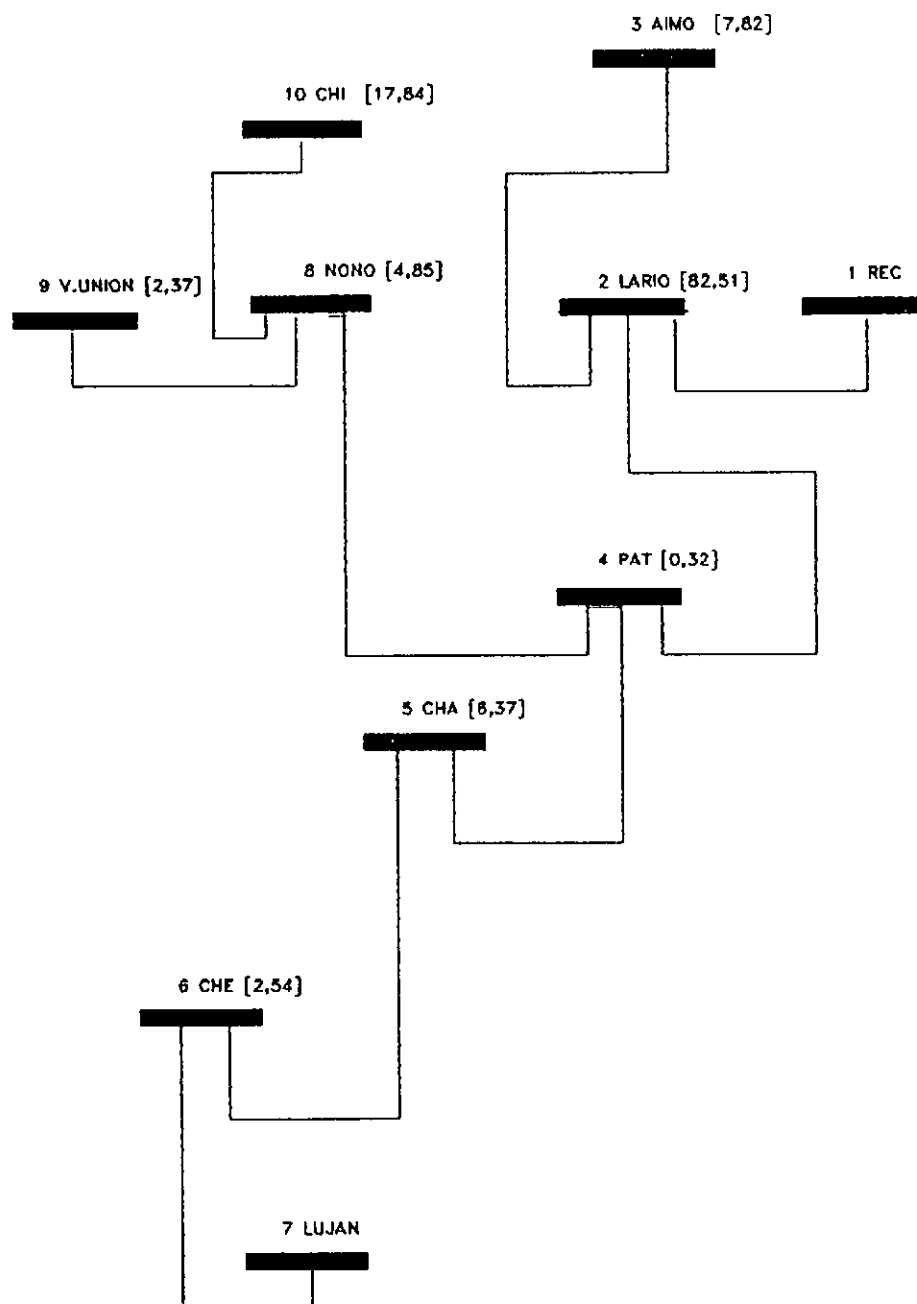
Totals : 39.285 0.000 39.285

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
GRAFICO N° LAR-G-300-1
CARGA MW [] AÑO 1995
ALTERNATIVA N° 3-7



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
GRAFICO N° LAR-G-300-2
CARGA MW [] AÑO 2000
ALTERNATIVA N° 1-7



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

CIRCUITO PARA FLUJO

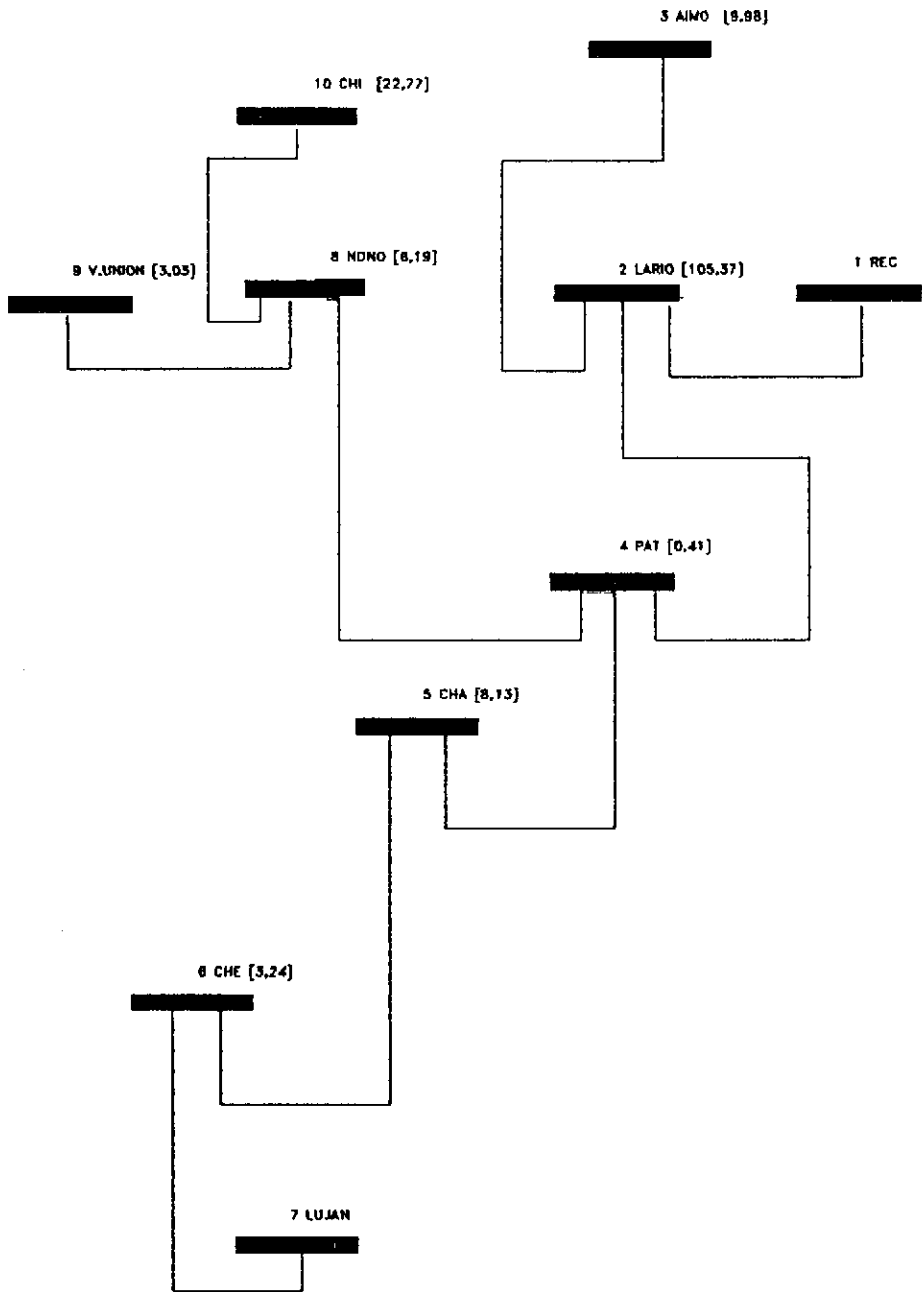
DE CARGAS 132 kV - LA RIOJA

GRAFICO N° LAR-G-300-3

CARGA MW []

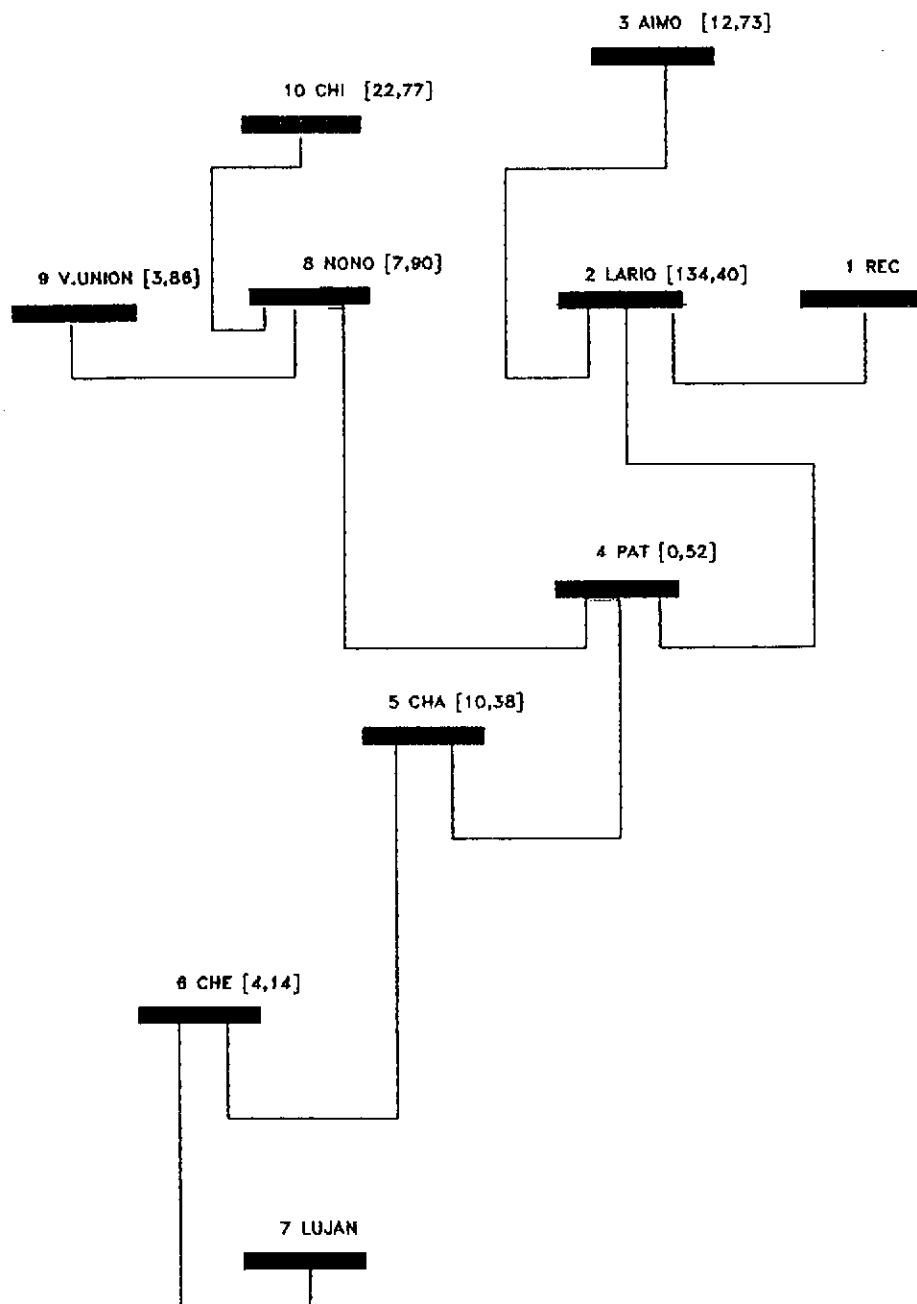
AÑO 2005

ALTERNATIVA N° 5-7



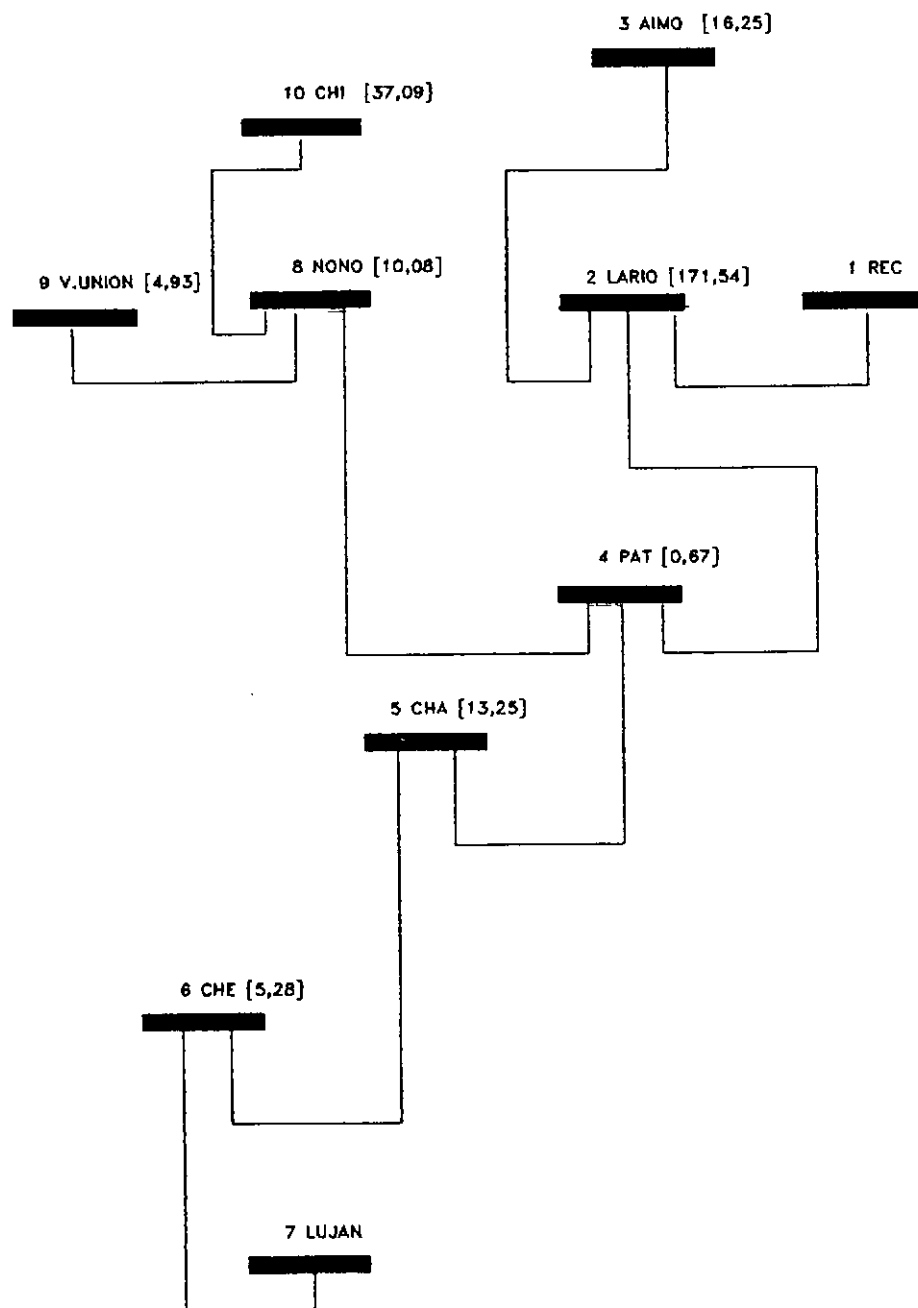
ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

CIRCUITO PARA FLUJO
 DE CARGAS 132 kV - LA RIOJA
 GRAFICO N° LAR-G-300-4
 CARGA MW [] AÑO 2010
 ALTERNATIVA N° 6-7



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993

CIRCUITO PARA FLUJO
DE CARGAS 132 kV - LA RIOJA
GRAFICO N° LAR-G-300-5
CARGA MW [] AÑO 2013
ALTERNATIVA N° 7-7



ESTUDIO DE ELECTRIFICACION DE LA RIOJA-CFI AÑO 1993